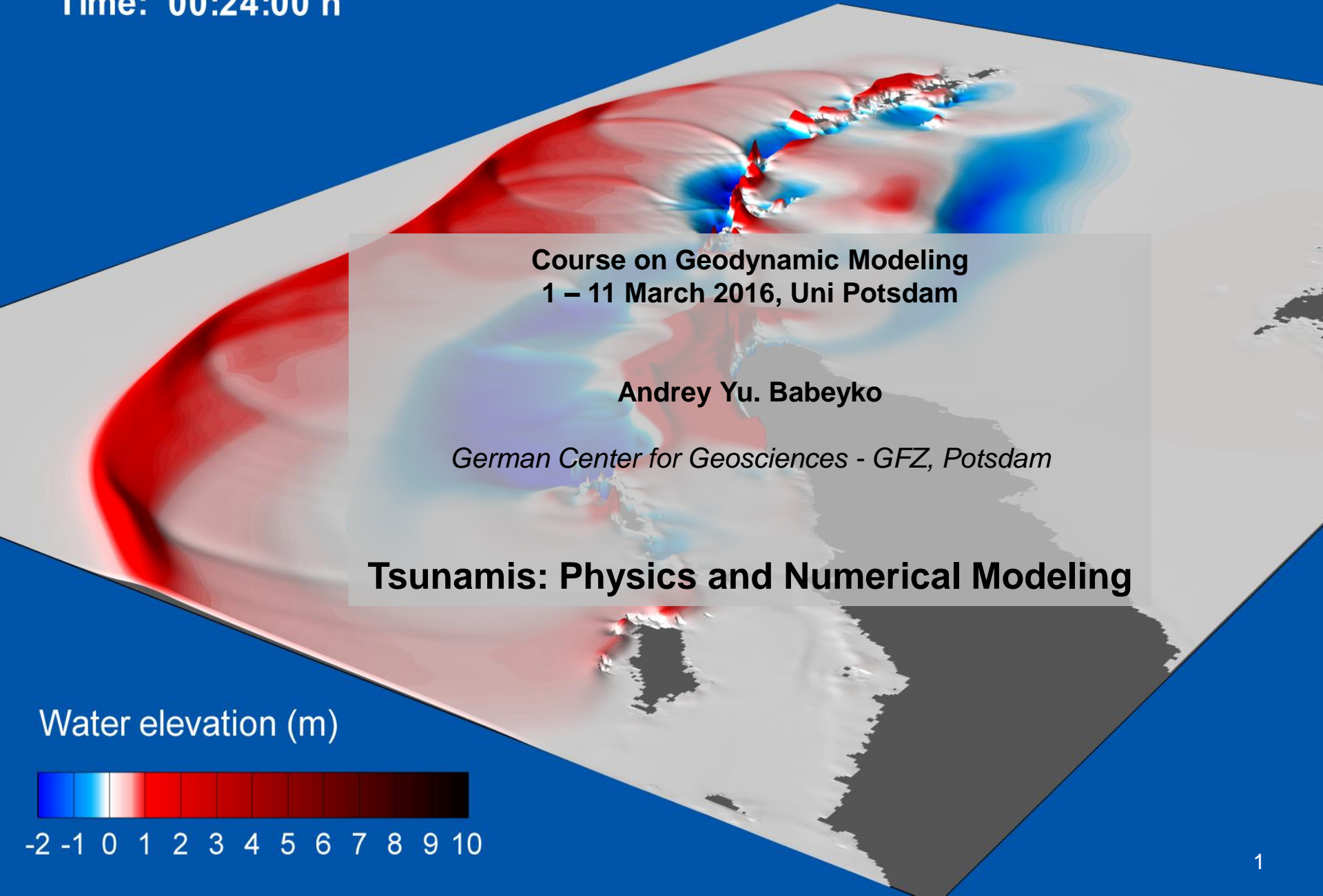


Time: 00:24:00 h



**Course on Geodynamic Modeling
1 – 11 March 2016, Uni Potsdam**

Andrey Yu. Babeyko

German Center for Geosciences - GFZ, Potsdam

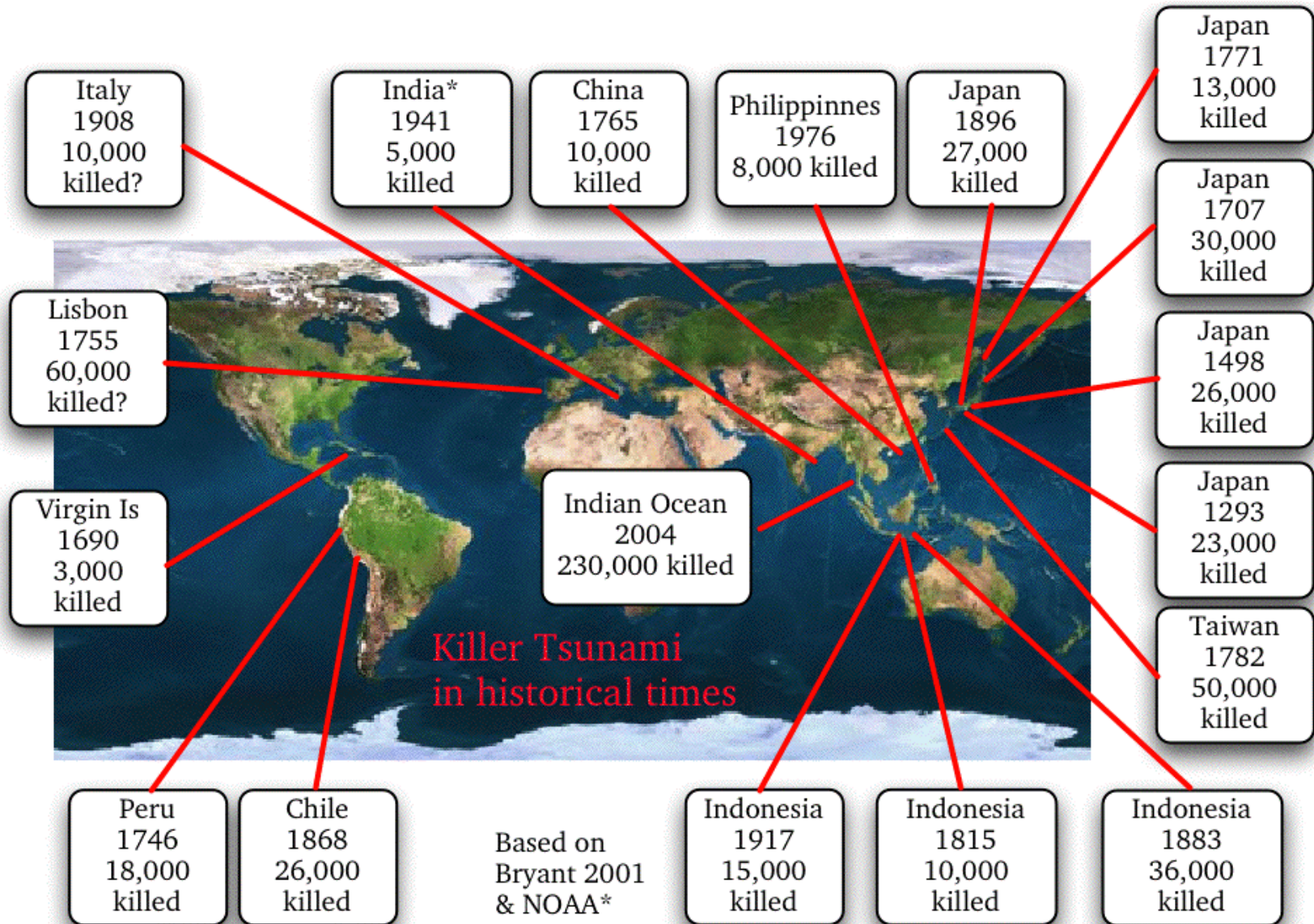
Tsunamis: Physics and Numerical Modeling

Water elevation (m)



Outline:

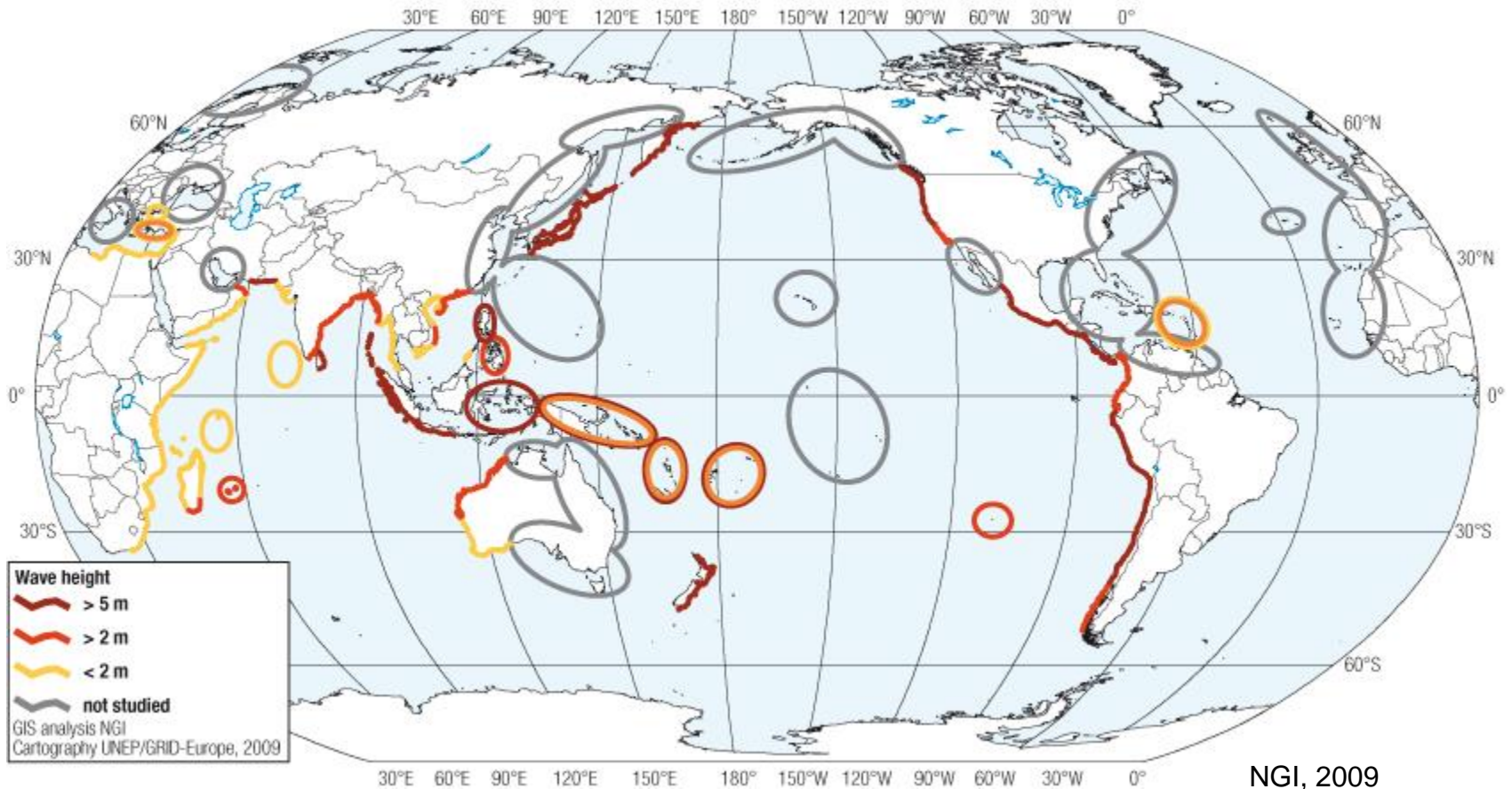
1. Tsunami as global natural hazard
2. Tsunamigenic sources
3. Tsunami modeling: background
4. Tsunami modeling: applications



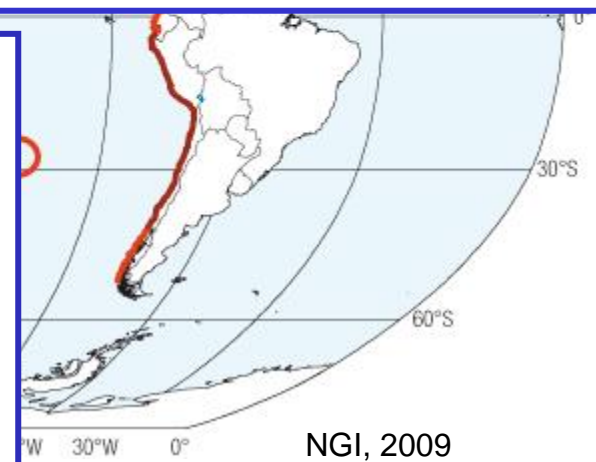
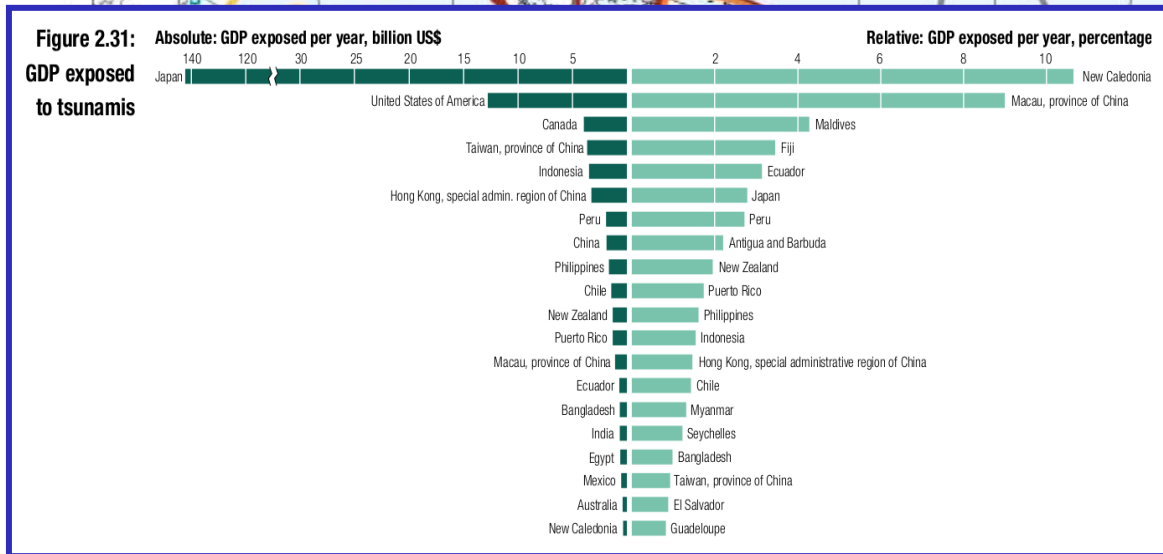
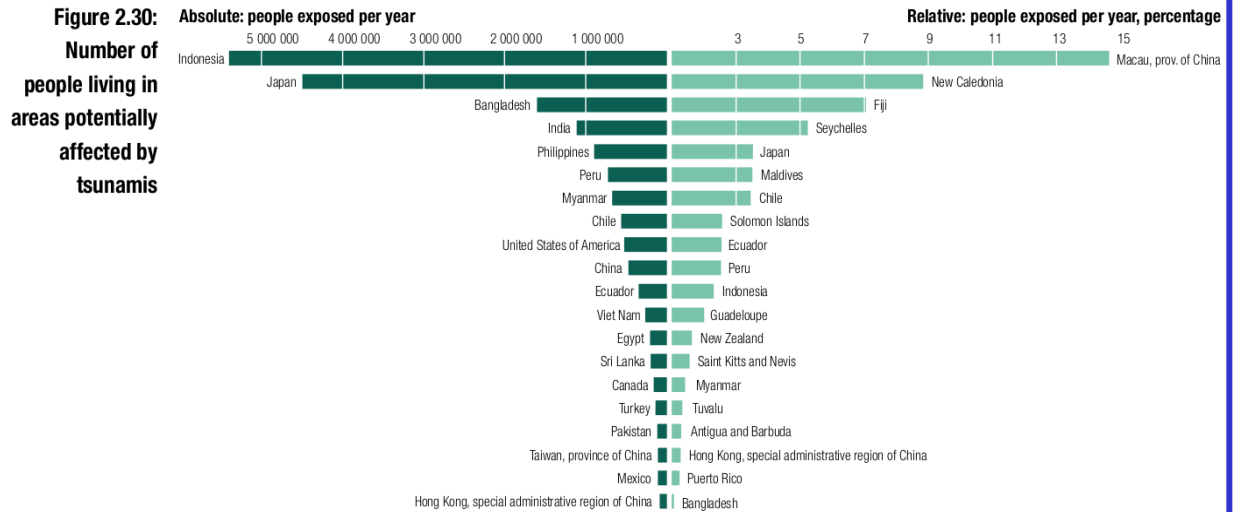
Michael Paine, Australian Spaceguard Survey - updated 24 Jan 05

Global Assessment Report on Disaster Risk Reduction -- **GAR**

Sketch of global tsunami hazard



Global Assessment Report on Disaster Risk Reduction -- GAR



What controls Tsunami distribution worldwide?

Lithospheric Plates and Distribution of Earthquakes

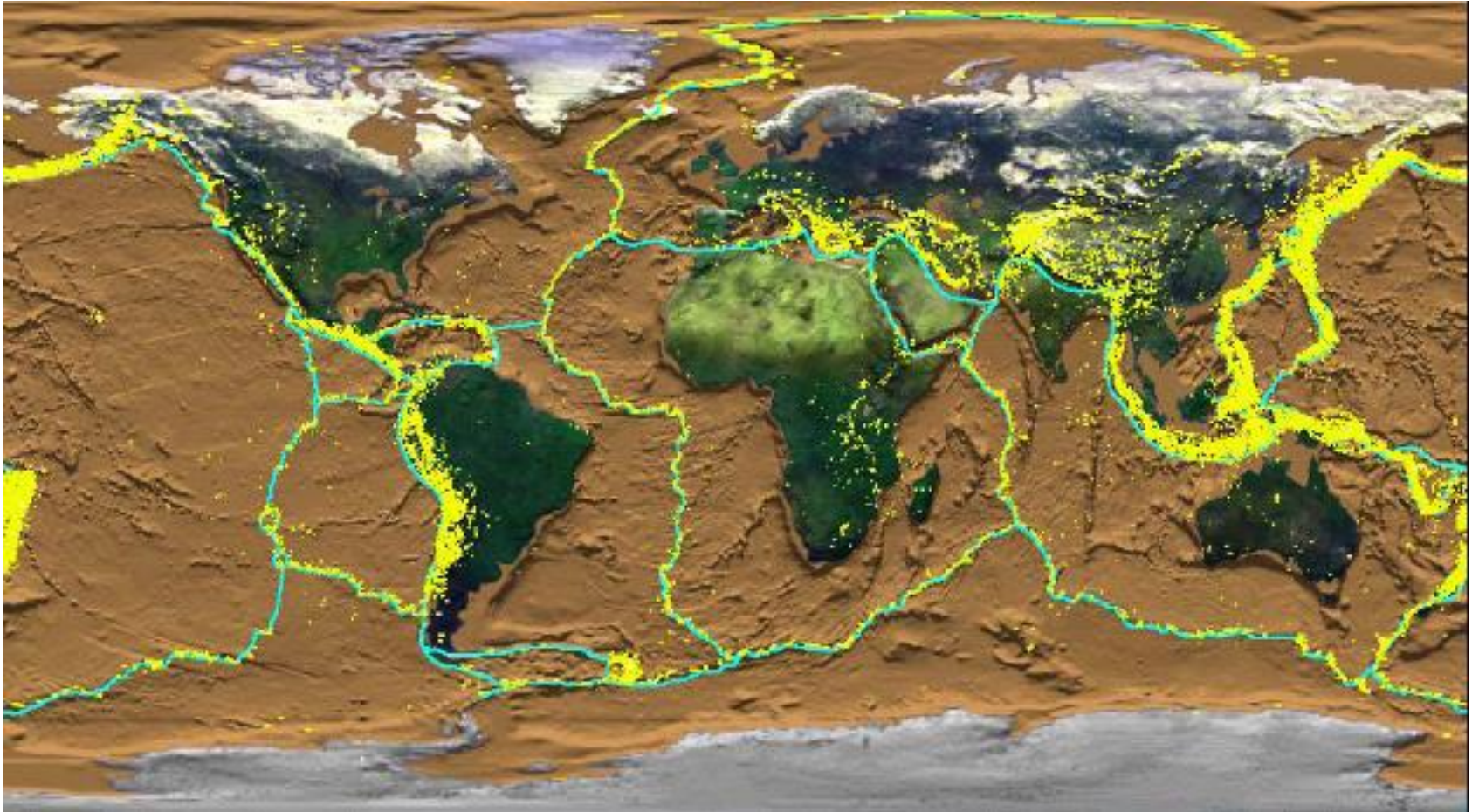
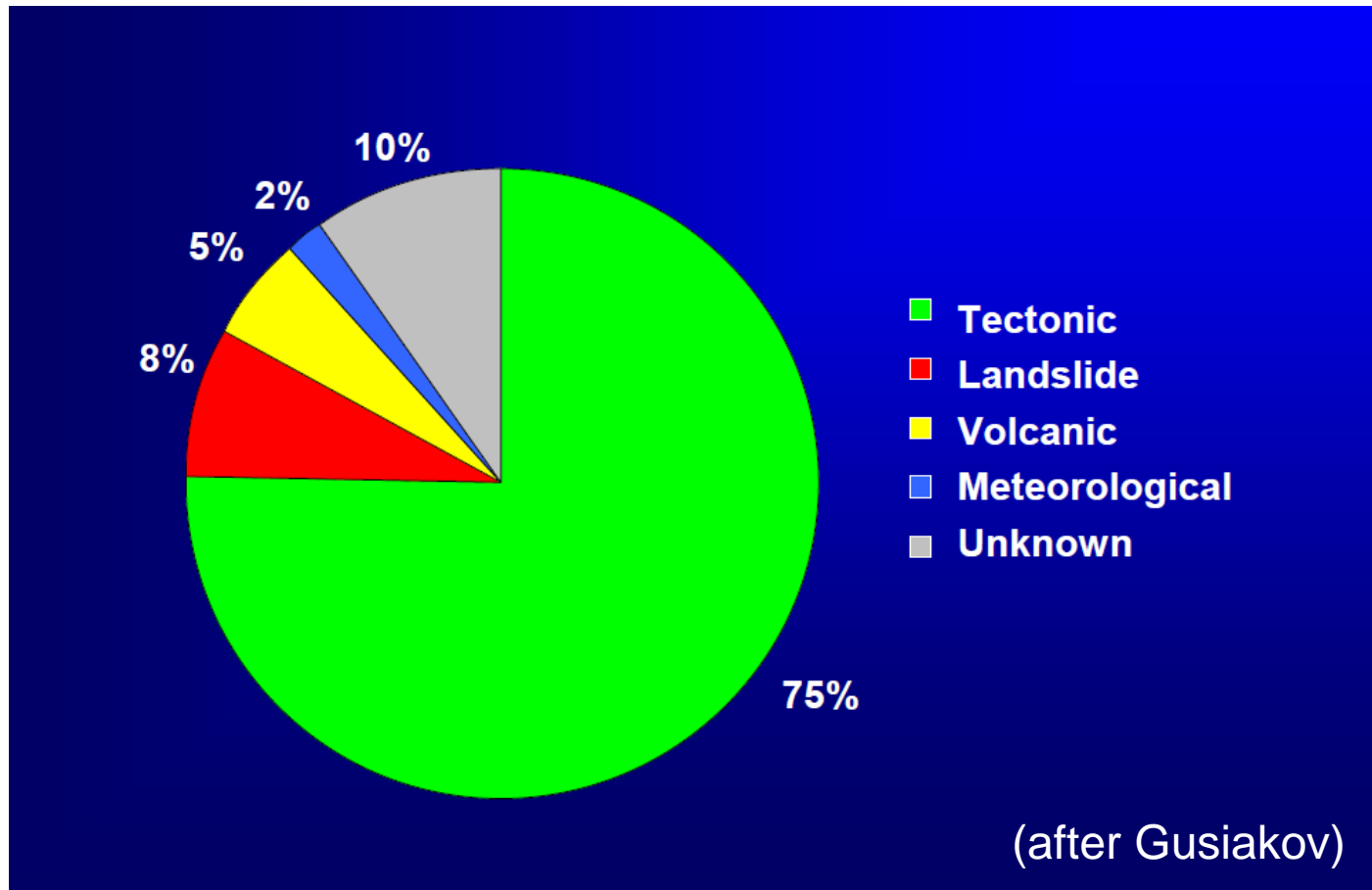
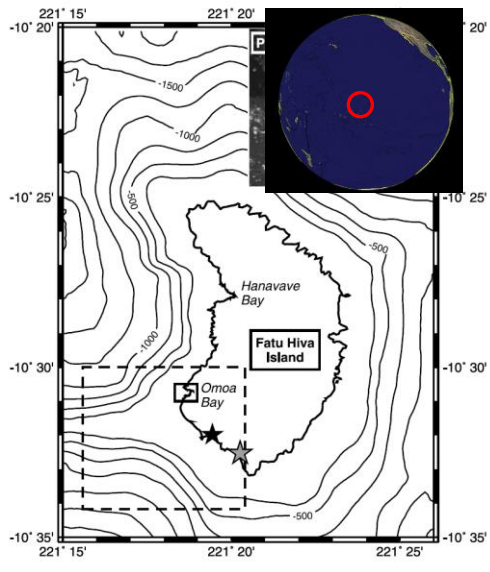


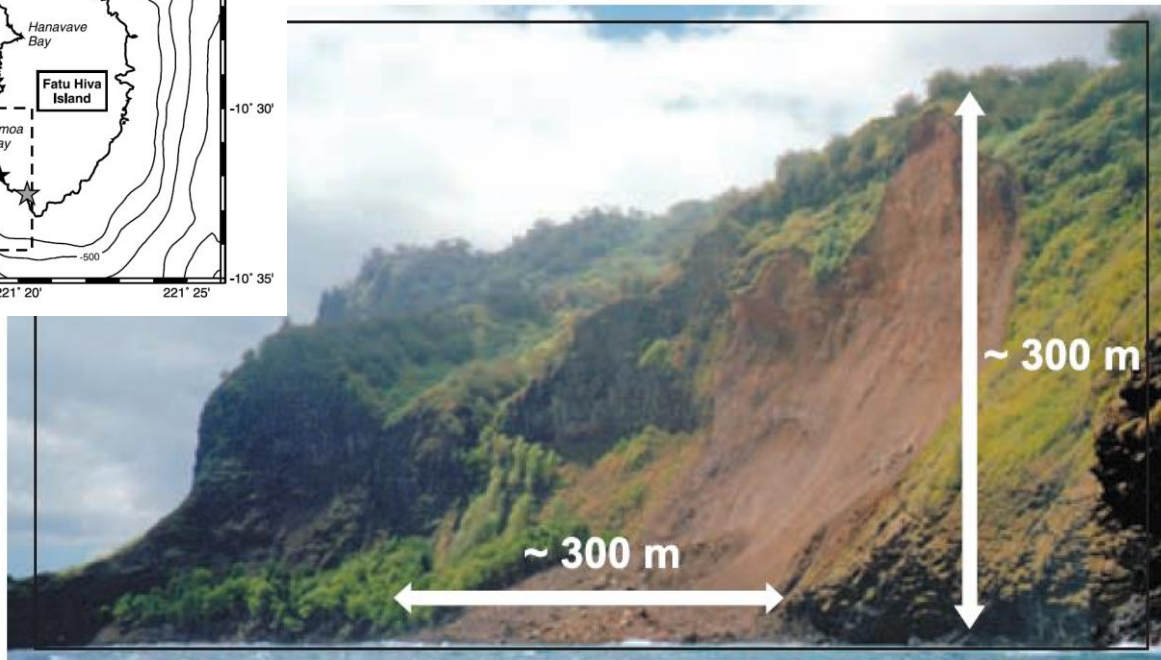
Image from Humboldt University Berlin

Tsunamigenic Sources





Fatu Hiva (French Polynesia) 1999



Hebert et al. (2002)

Lituya Bay (Alaska, USA) 1958



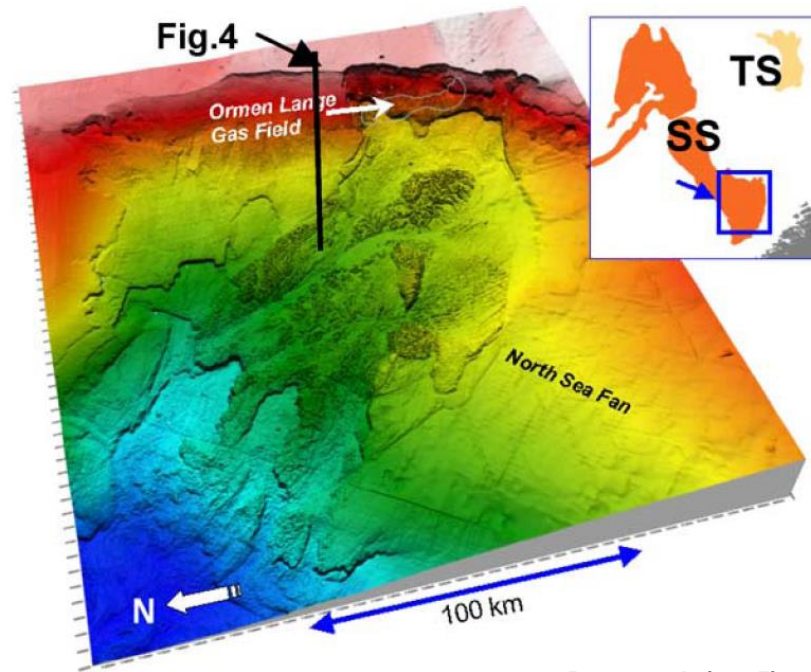
About 500 m run-up

after G. Pararas-Carayannis

Storegga Slide (Norway) 8200 B.C.



Fig. 1. Location map showing the Storegga and Trænadjupet submarine slides on the Mid-Norway margin.

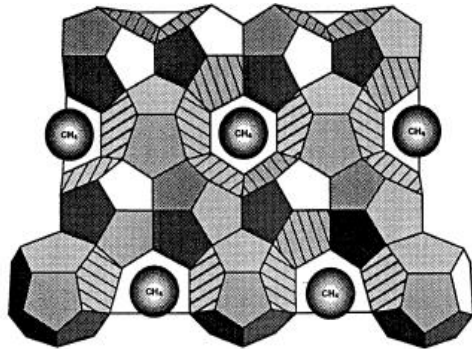


Bryn et al. (2005)

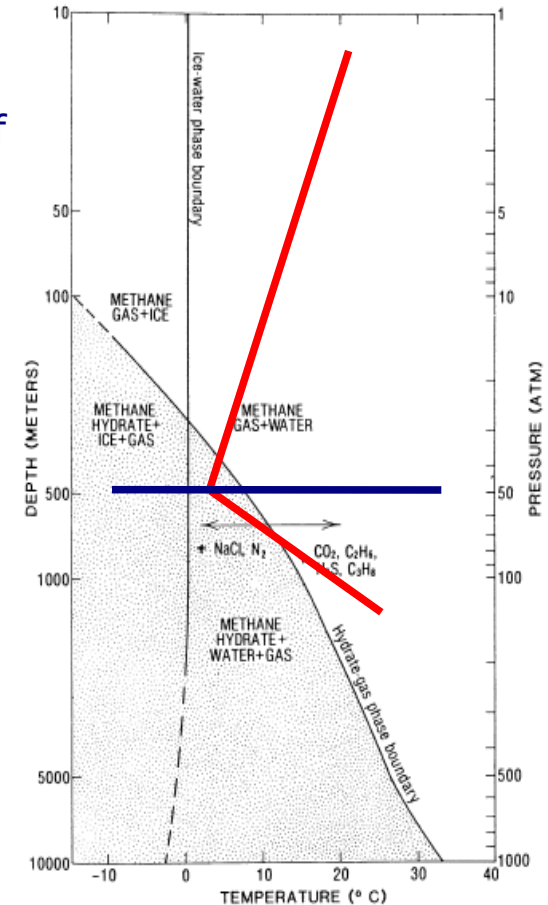
One of the biggest historic slides (2400 km^3).

Slides of this size are extremely rare but re-occur in geological time scales.

Gas hydrates can destabilize submarine slopes



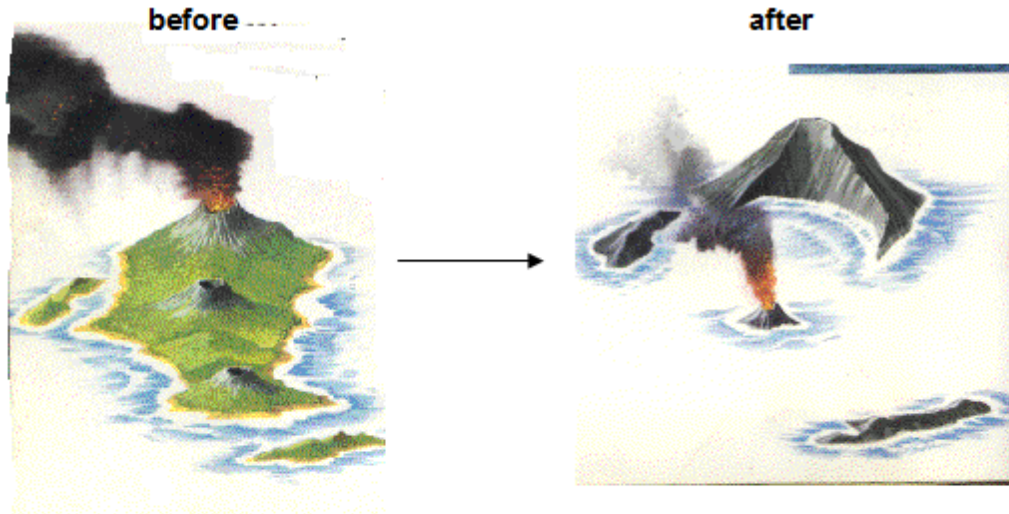
Natural gas hydrates are solid crystalline compounds composed of molecules of natural gas trapped in cages of water molecules. Looks like ice and has similar density.



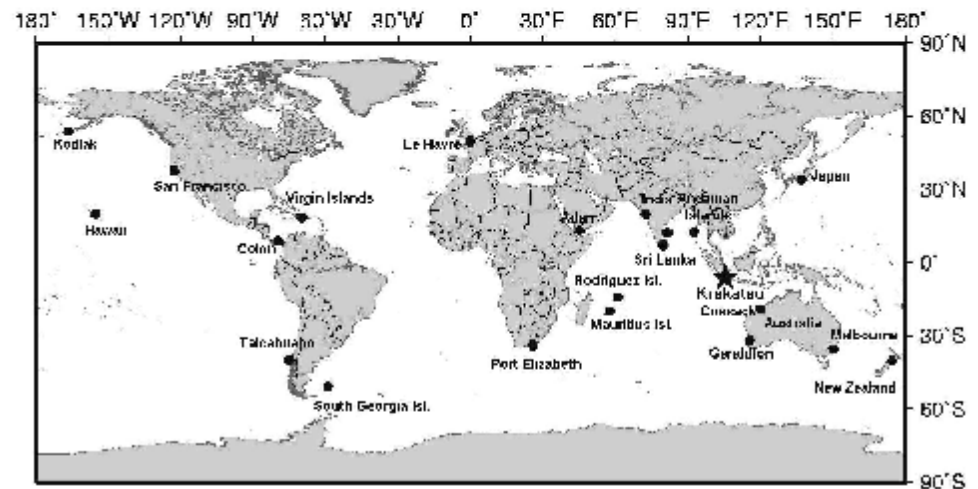
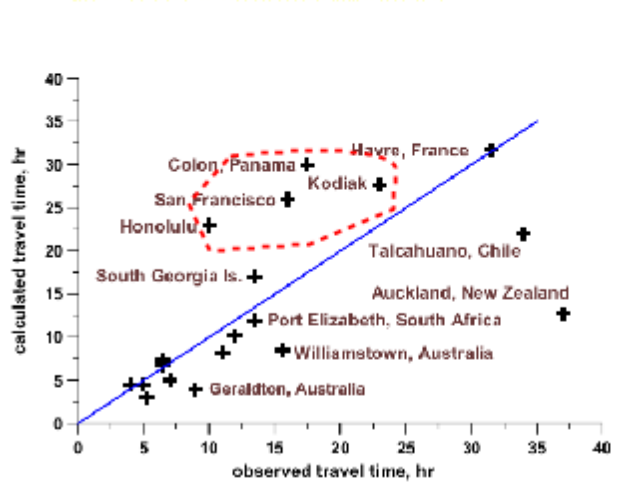
That's why they are important for us!

1 m^3
Gas Hydrate
 164 m^3
Gas
 0.8 m^3
Water

Krakatau, August 26, 1883



after G. Pararas-Carayannis
(www.drgeorgepc.com)



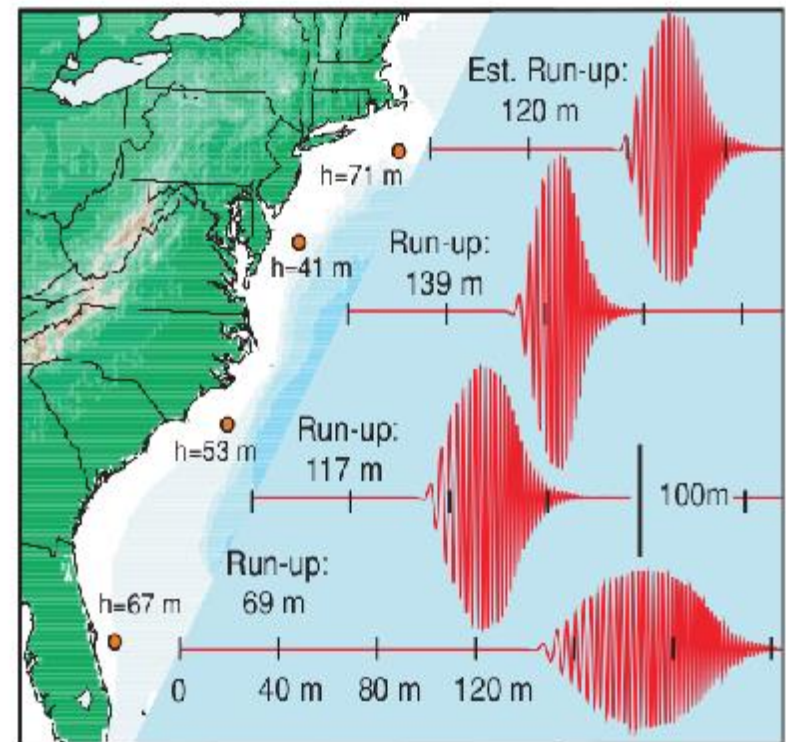
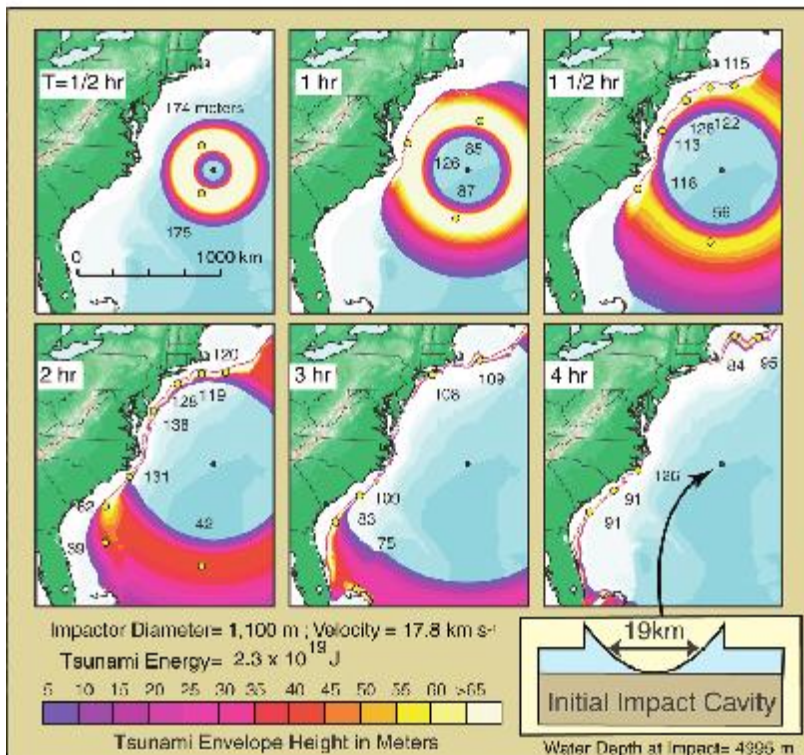
Sea-level change recordings and analysis (Choi et al., 2003)

Asteroid impact tsunami of 2880 March 16

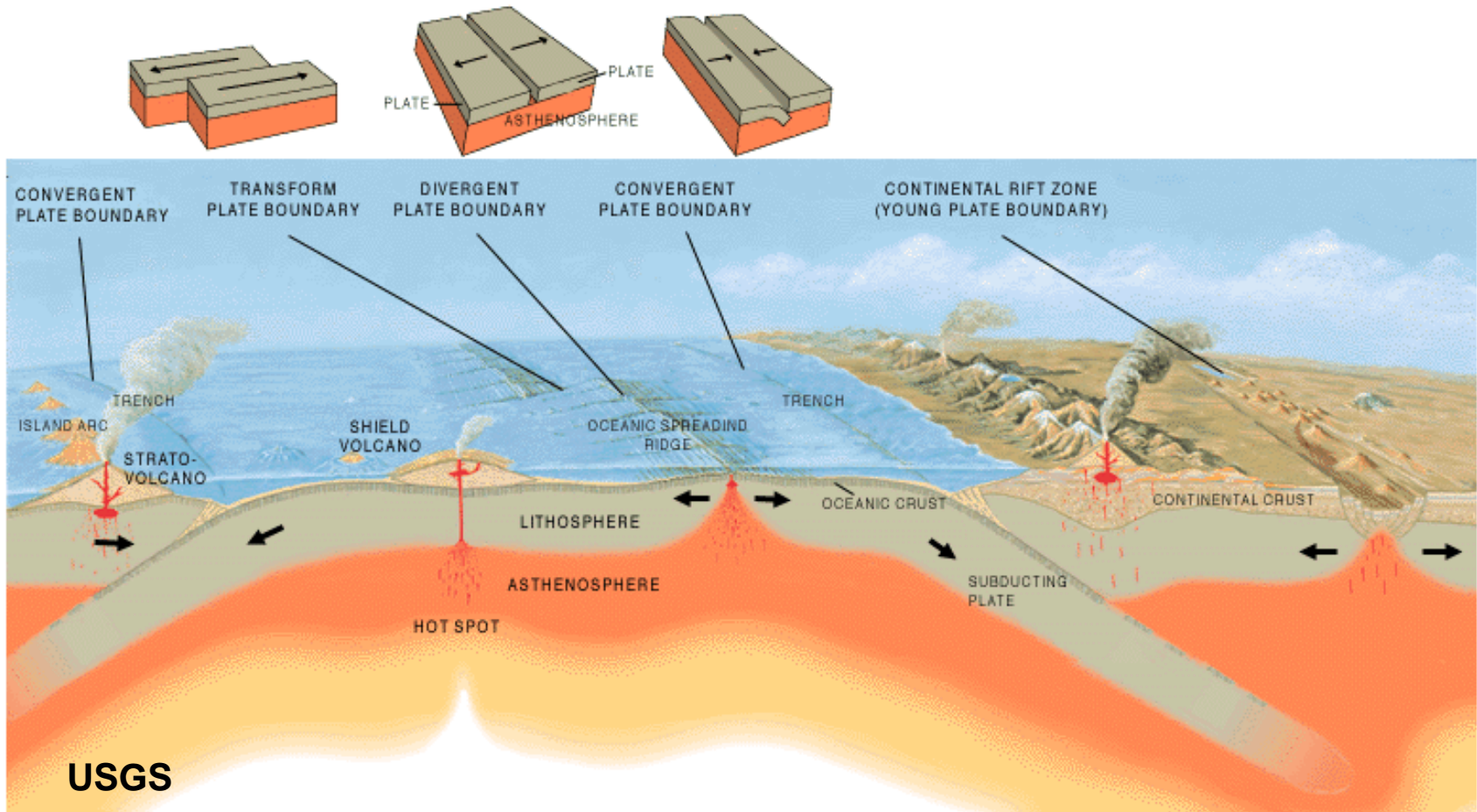
A scenario according to Ward & Asphaug (2003)



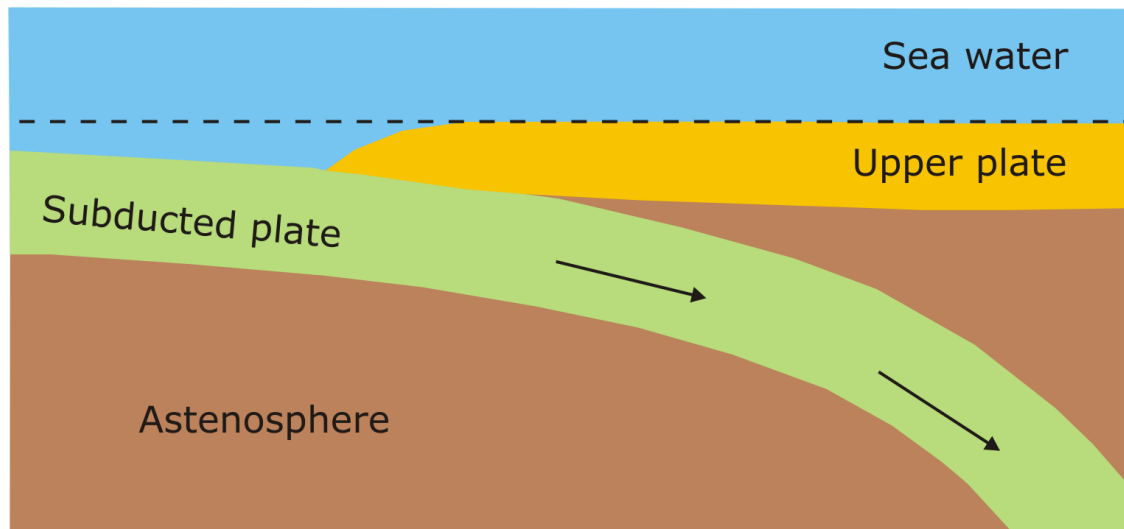
A 1.1-km diameter asteroid named „DA 1950“ has a 0.0-0.3% probability to collide with the Earth in the year 2880



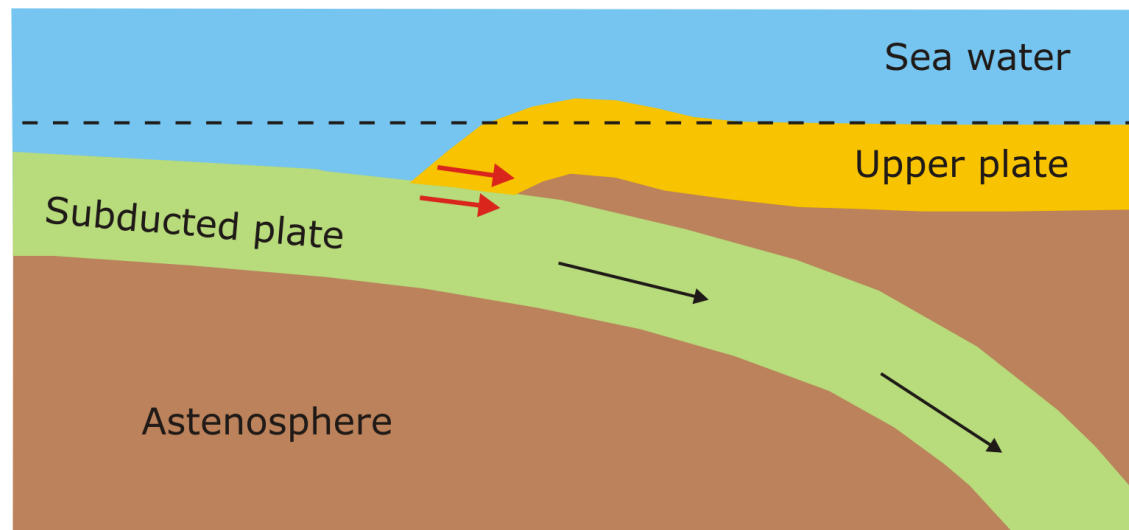
Elements of plate tectonics



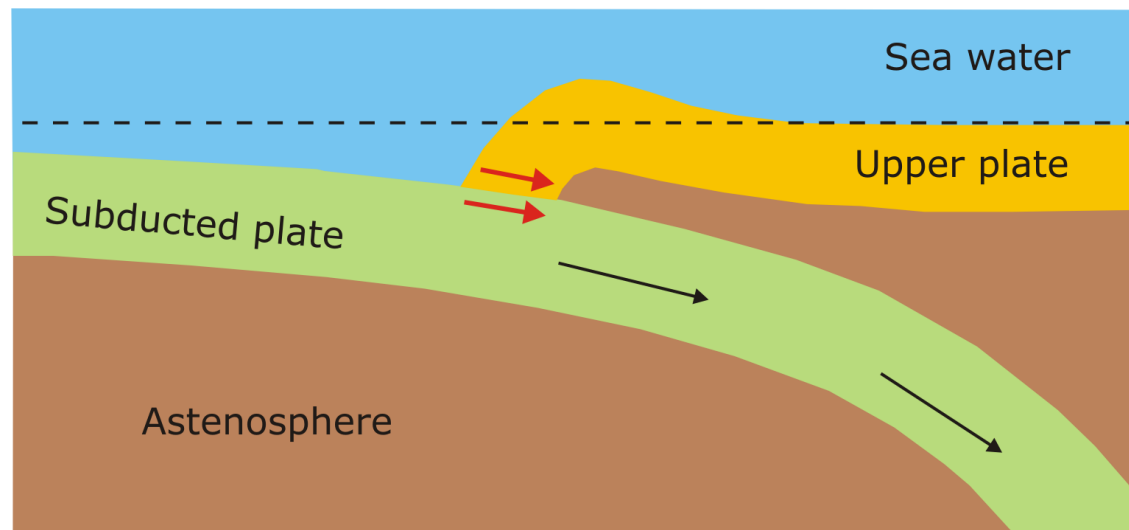
Mechanism of interplate subduction earthquake



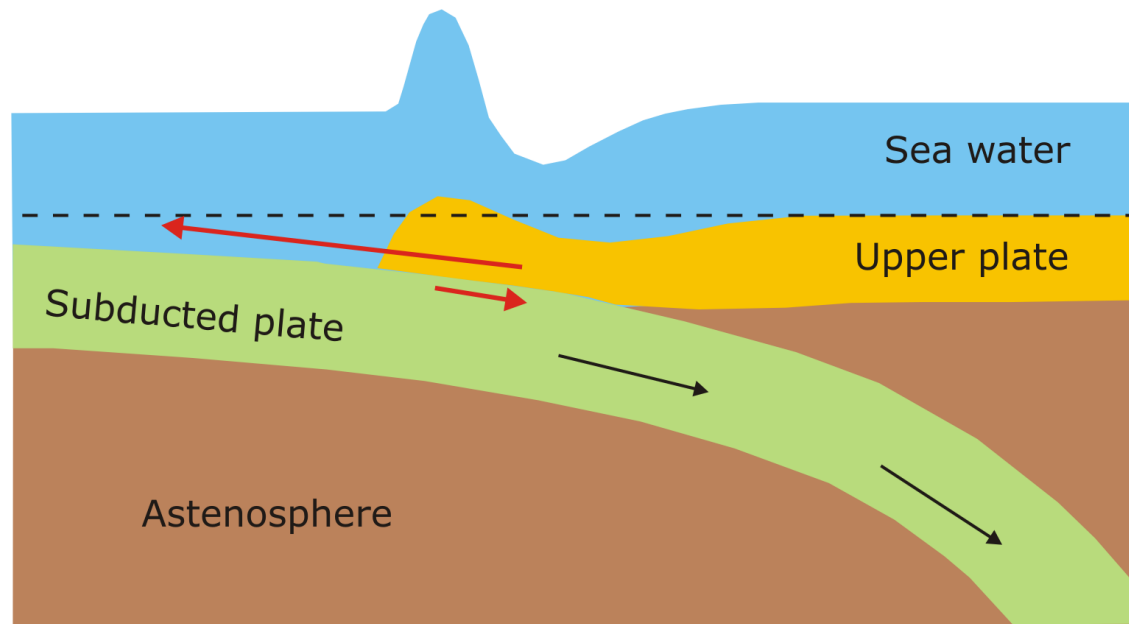
Mechanism of interplate subduction earthquake



Mechanism of interplate subduction earthquake

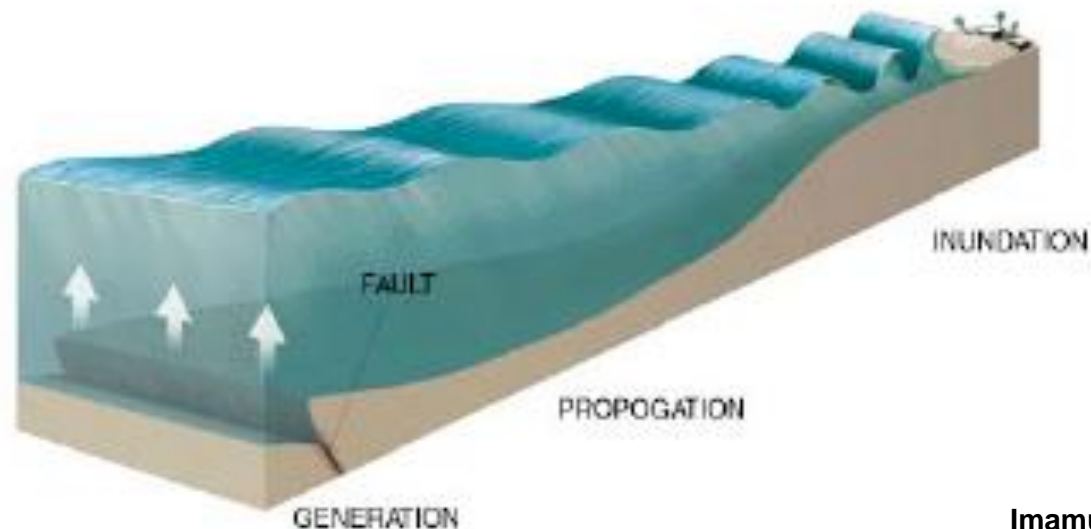


Mechanism of interplate subduction earthquake



3 steps in Tsunami modelling

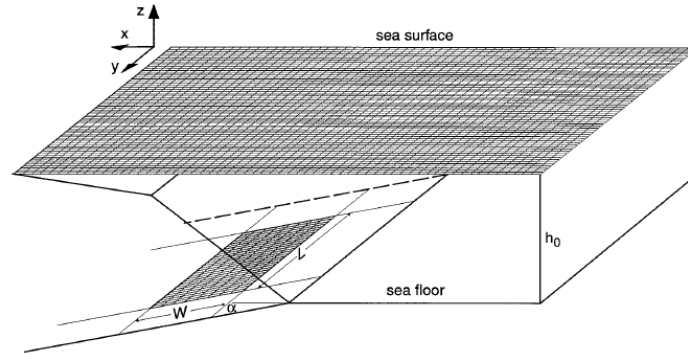
- Tsunami generation
- Tsunami propagation in deep ocean
- Wave run-up and coastal inundation



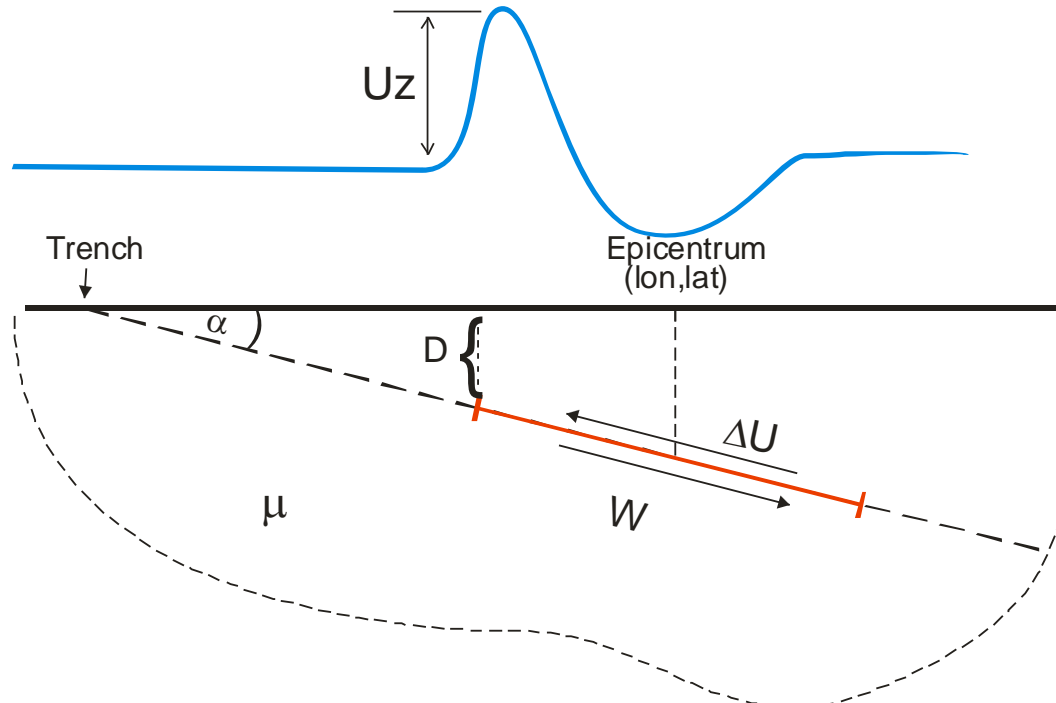
Imamura (2005)

Modeling sea surface displacement Rectangular fault

$$M_0 = \mu L W \Delta U$$



- Model fault parameters:**
- Length – L
 - Width – W
 - Dip angle – α
 - Depth – D
 - Slip – ΔU
 - Rake angle – β
 - Shear modulus (rigidity) – μ



Analytical solution for the homogeneous elastic half-space (Okada, 1985)

1144

YOSHIMITSU OKADA

(1) Displacements

For strike-slip

$$\begin{cases} u_x = -\frac{U_1}{2\pi} \left[\frac{\xi q}{R(R+\eta)} + \tan^{-1} \frac{\xi \eta}{qR} + I_1 \sin \delta \right] \\ u_y = -\frac{U_1}{2\pi} \left[\frac{\hat{y} q}{R(R+\eta)} + \frac{q \cos \delta}{R+\eta} + I_2 \sin \delta \right] \\ u_z = -\frac{U_1}{2\pi} \left[\frac{dq}{R(R+\eta)} + \frac{q \sin \delta}{R+\eta} + I_4 \sin \delta \right] \end{cases}$$

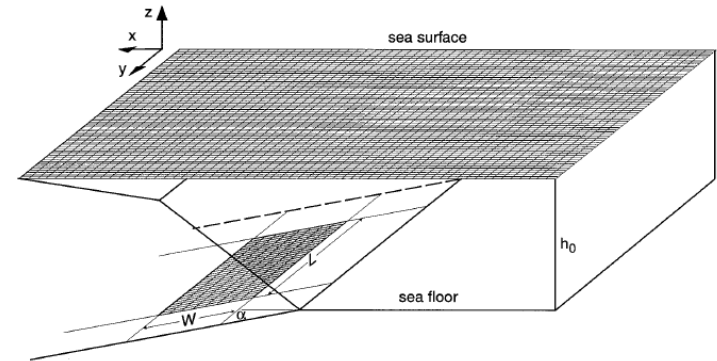
For dip-slip

$$\begin{cases} u_x = -\frac{U_2}{2\pi} \left[\frac{q}{R} - I_5 \sin \delta \cos \delta \right] \\ u_y = -\frac{U_2}{2\pi} \left[\frac{\hat{y} q}{R(R+\xi)} + \cos \delta \tan^{-1} \frac{\xi \eta}{qR} - I_1 \sin \delta \cos \delta \right] \\ u_z = -\frac{U_2}{2\pi} \left[\frac{dq}{R(R+\xi)} + \sin \delta \tan^{-1} \frac{\xi \eta}{qR} - I_5 \sin \delta \cos \delta \right] \end{cases}$$

where

$$\begin{cases} I_1 = \frac{\mu}{\lambda + \mu} \left[\frac{-1}{\cos \delta} \frac{\xi}{R+d} \right] - \frac{\sin \delta}{\cos \delta} I_5 \\ I_2 = \frac{\mu}{\lambda + \mu} [-\ln(R+\eta)] - I_3 \\ I_3 = \frac{\mu}{\lambda + \mu} \left[\frac{1}{\cos \delta} \frac{\hat{y}}{R+d} - \ln(R+\eta) \right] + \frac{\sin \delta}{\cos \delta} I_4 \\ I_4 = \frac{\mu}{\lambda + \mu} \frac{1}{\cos \delta} [\ln(R+d) - \sin \delta \ln(R+\eta)] \\ I_5 = \frac{\mu}{\lambda + \mu} \frac{2}{\cos \delta} \tan^{-1} \frac{\eta(X+q \cos \delta) + X(R+X) \sin \delta}{\xi(R+X) \cos \delta} \end{cases}$$

Analytical expressions for $U_i(x,y), i=(x,y,z)$



Model parameters:

1) Fault geometry
 $L, W, \alpha, D, \Delta U, \beta$

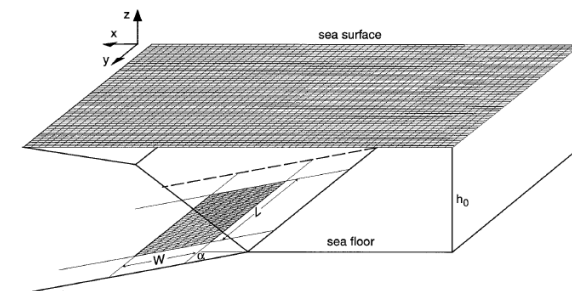
2) Position of obs. point
 x, y

3) Parameters of the media
 λ, μ

Scaling laws

Empirically calibrated relations between earthquakes parameters

We would like to know 3 fault parameters: length (L), width (W) and slip (ΔU) from the seismic moment (M_0) only.



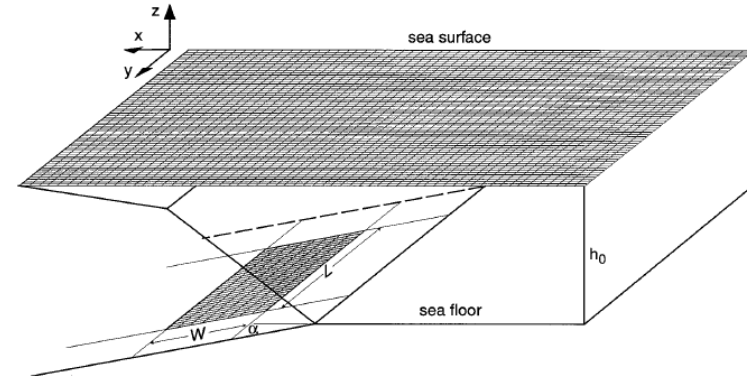
$$M_0 = \mu L W \Delta U$$

If, e.g., $L = L(M_0)$ and $W = W(M_0)$,

then: $M_0 = \mu L(M_0) W(M_0) \Delta U$

and: $\Delta U = M_0 / (\mu L(M_0) W(M_0))$

$$M_0 = \mu L W \Delta U$$



Measured:
 M_0 , location

Finite fault parameters that we do need:

- Length – L
- Width – W
- Dip angle – α
- Depth – D
- Slip – ΔU
- Rake angle – β
- Shear modulus (rigidity) – μ



- M_0 + scaling laws
- M_0 + scaling laws
- subduction zone geometry
- location + subduction zone geometry
- M_0 + scaling laws
- assumed
- material constant

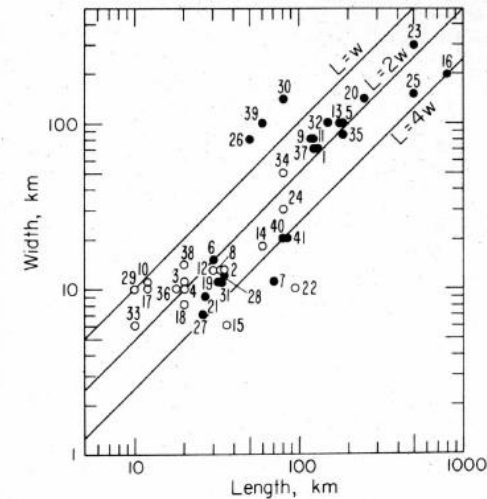
μ : crustal rocks – 30-40 GPa, dry olivine – 74 GPa;

$$M_0 = \mu L W \Delta U$$

Scaling laws: physical reasoning

- Rupture can grow in all directions.
Hence: $L \sim W$
- Max. strain $\epsilon \sim \Delta U/W$ is related to rock *strength*.
Hence: $\Delta U \sim W$
- Thus one might expect that: $M_0 \sim L^3$

Geller (1976)



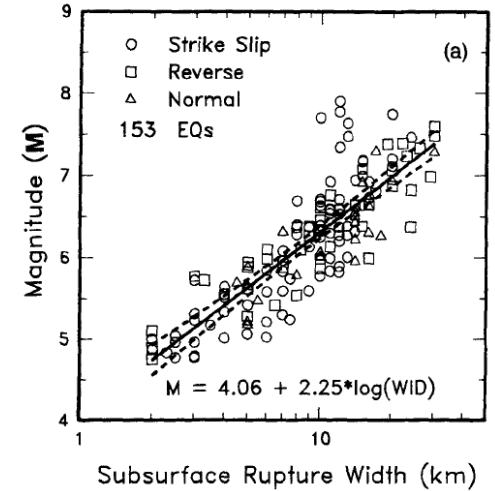
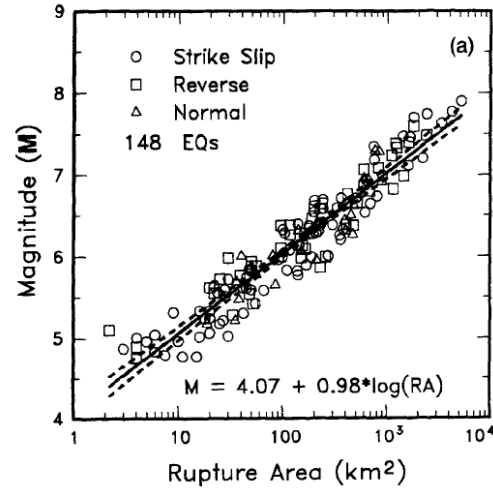
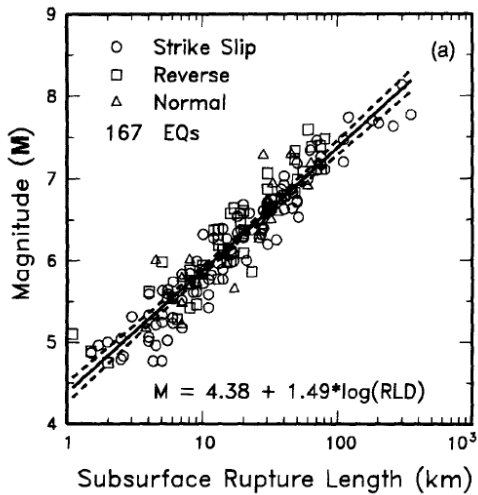
But, for large earthquakes these relations should break down!

- W cannot grow as far as L can do: temperature increases with depth – material is no more brittle
- Similarly, ΔU may stop growing to keep strain
- Hence we might expect that for large events: $M_0 \sim L$

$$M_0 = \mu L W \Delta U$$

Scaling laws

Calibrations of Wells and Coppersmith (1994)



Wells, D.L., Coppersmith, K.J. (1994). New empirical relationships among magnitude, rupture length, rupture width, rupture area, and surface displacement. Bull. Seism. Soc. Am. 84, 974-1002.

Quick fault model: an example

Event with $M_w = 8.5$

L and W from
scaling laws:

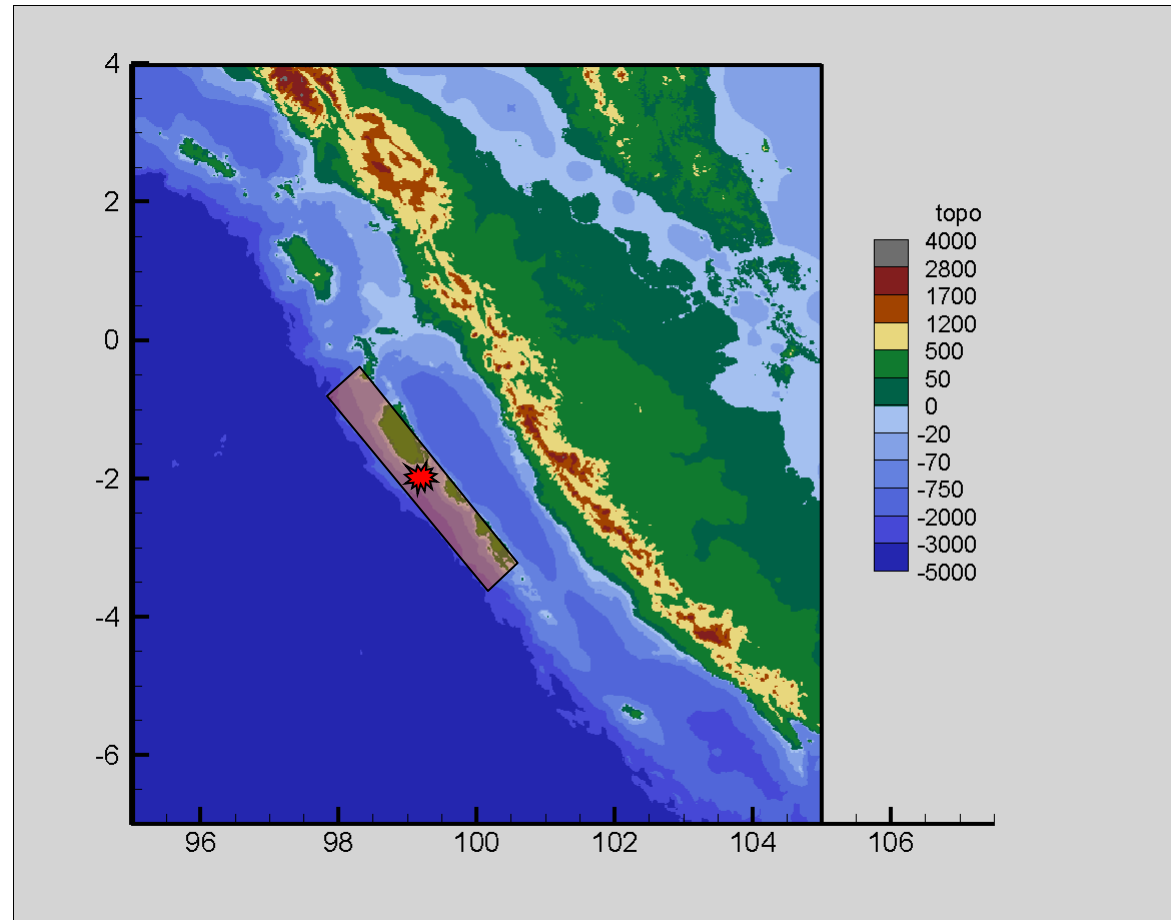
$L \sim 375$ km

$W \sim 50$ km

Slip:

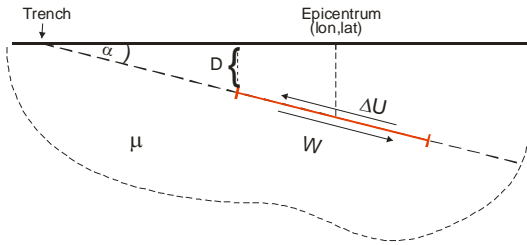
$$\Delta U = M_0 / (\mu L W)$$

$\Delta U \sim 13$ m

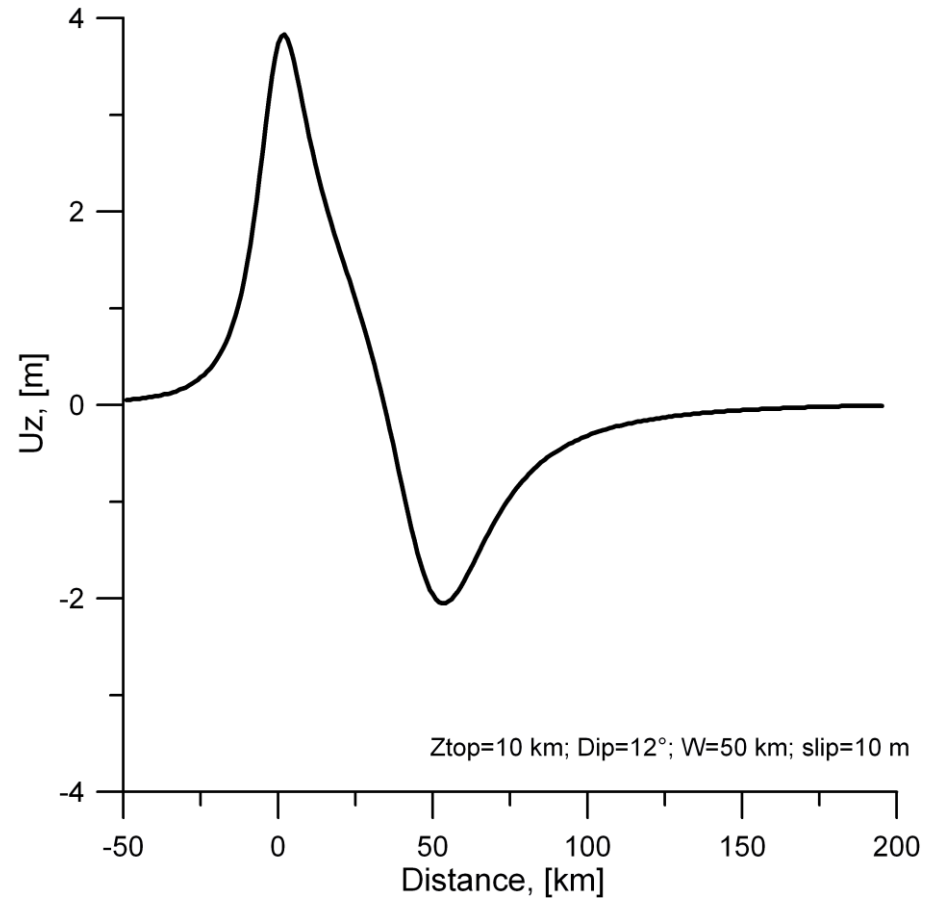


$$M_0 = \mu L W \Delta U$$

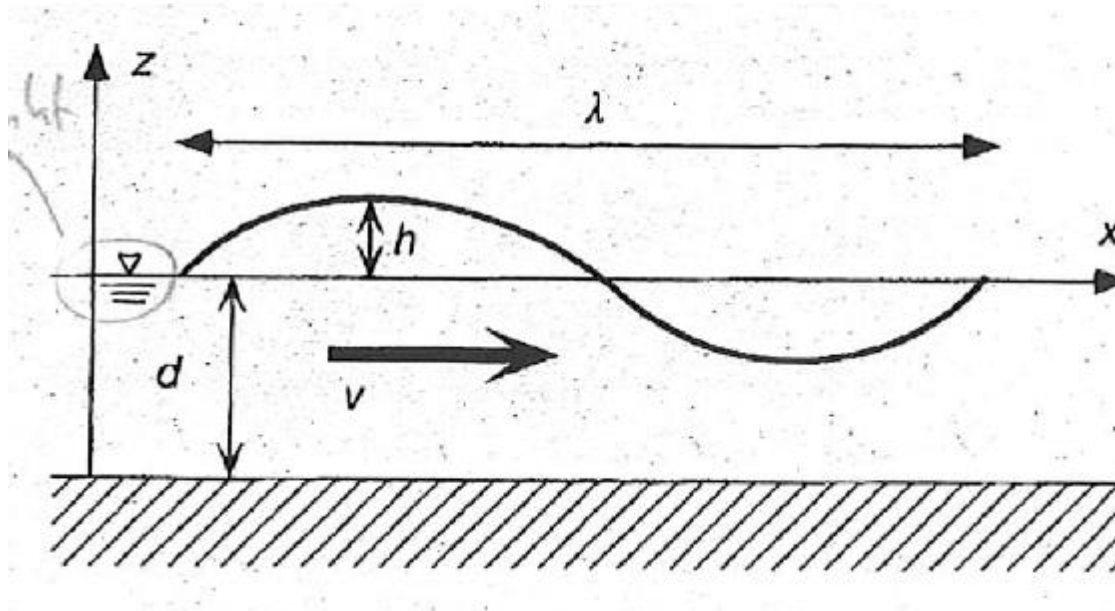
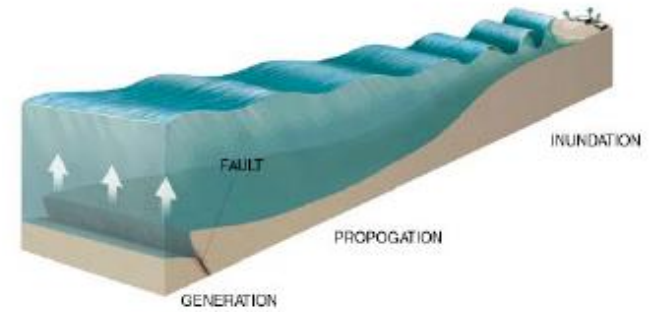
Vertical displacement 1D- perspective



Remark: here and below $Z_{top}=D$



Modeling: Nomenclature

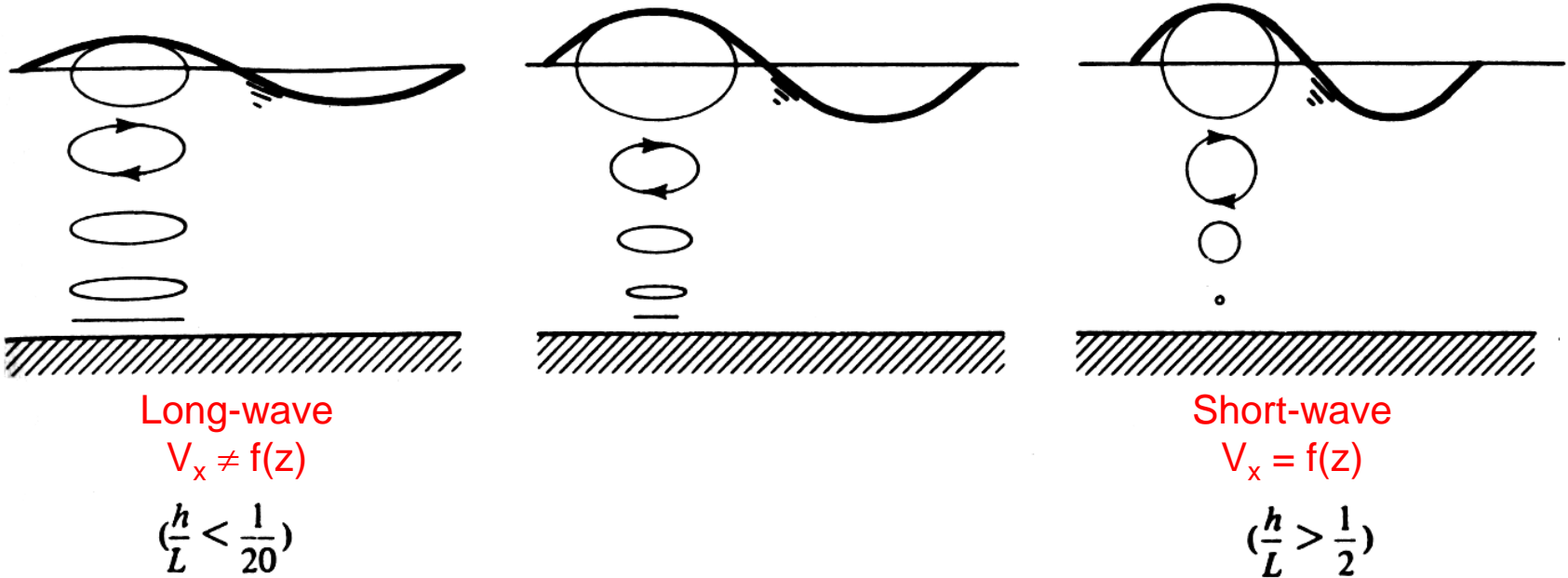


Full 3D model:

$$\rho \frac{\partial \mathbf{u}}{\partial t} + \rho \mathbf{u} \cdot \nabla \mathbf{u} = -\nabla P + \eta \nabla^2 \mathbf{u} \quad \text{- 3D Navier-Stokes equation}$$

$$\nabla \mathbf{u} = 0 \quad \text{- mass conservation (incompressible)}$$

Tsunami is a long wave !



Modeling: Governing equations

The simplest form: Linear shallow water (long wave) equations

$$\frac{\partial u}{\partial x}d + \frac{\partial h}{\partial t} = 0 \quad \text{-- balance of mass}$$

$$\frac{\partial u}{\partial t} + g \frac{\partial h}{\partial x} = 0 \quad \text{-- balance of momentum}$$

Note: Solution (h and u) depends on one single variable: water depth d !

Modeling: Governing equations

$$\begin{array}{l} \frac{\partial u}{\partial x}d + \frac{\partial h}{\partial t} = 0 \\ \frac{\partial u}{\partial t} + g\frac{\partial h}{\partial x} = 0 \end{array} \quad \left| \begin{array}{l} \frac{\partial}{\partial t} \\ \frac{\partial}{\partial x} \end{array} \right.$$

$$\begin{array}{l} \frac{\partial^2 u}{\partial t \partial x}d + \frac{\partial^2 h}{\partial t^2} = 0 \\ \frac{\partial^2 u}{\partial t \partial x} + g\frac{\partial^2 h}{\partial x^2} = 0 \end{array} \Rightarrow \boxed{\frac{\partial^2 h}{\partial t^2} = gd \frac{\partial^2 h}{\partial x^2}} \quad \text{-- wave equation}$$

$$\boxed{c = \sqrt{gd}} \quad \text{-- wave speed}$$

Linear theory for long waves $\lambda \gg h$

Phase and group velocity $c = c_g = \sqrt{gh}$

Energy density (per unit area) $E = \frac{1}{2}\rho ga^2$

Energy flux (per unit length) $F = Ec_g$

Constant wave period and energy flux lead to:

$$\lambda = \lambda_0 \sqrt{\left(\frac{h}{h_0}\right)}, \quad a = a_0 \left(\frac{h_0}{h}\right)^{\frac{1}{4}}$$

Wave length decreases and amplitude increases in shallow water

Gjevik (2004)

Tsunami wave characteristics



Shallow-water equations: Numerical aspects

Numerical schemes:

(1) Finite differences on structural grids

Pro: easy to implement, robust, easy grids, quick, straightforward parallelization of computations

Contra: constant resolution, need for nested grids in coastal regions

Examples: TUNAMI-family, MOST, FUNWAVE

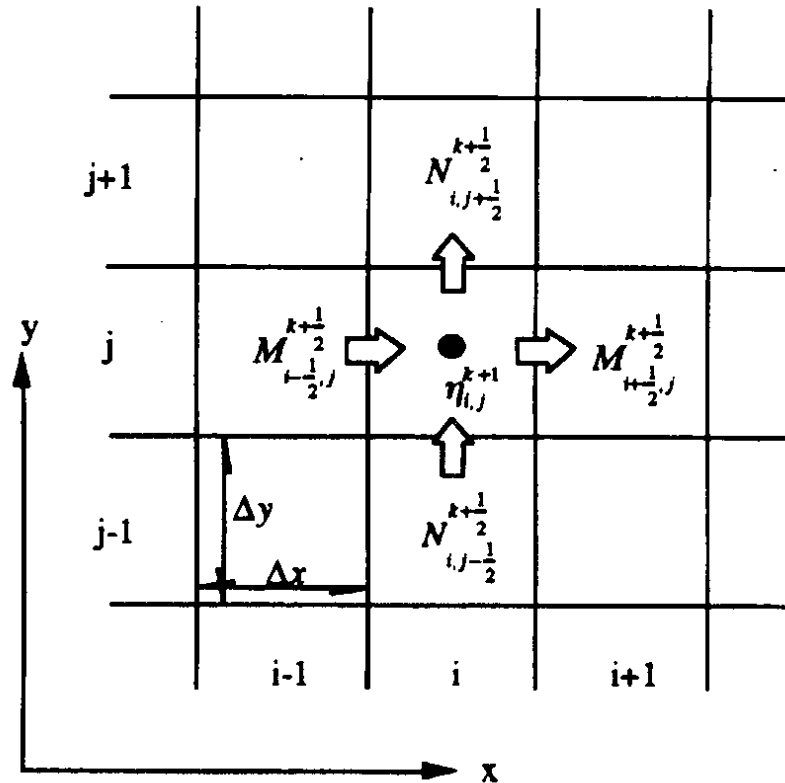
(2) Finite elements on unstructural grids

Pro: single computational domain for deep-ocean propagation and inundation

Contra: time consuming, stability problems, hard to program, complex grids

Examples: TsunAwi, ANUGA, Uni Bologne

Finite differences on structural grids



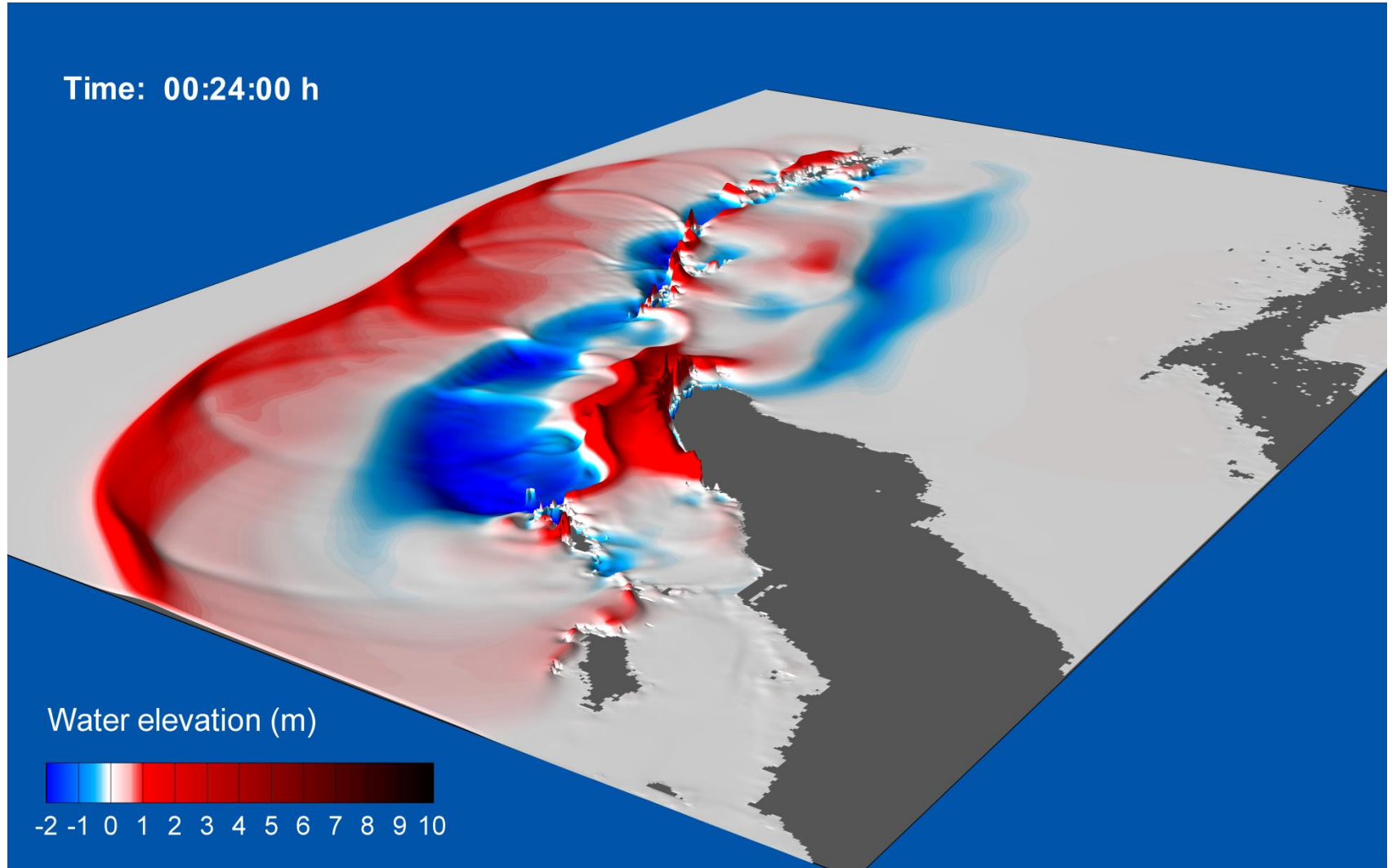
Imamura (1996)

$$\frac{\partial \eta}{\partial t} = \frac{1}{\Delta t} \left[\eta_{i,j}^{k+1} - \eta_{i,j}^k \right]$$

$$\frac{\partial M}{\partial x} = \frac{1}{\Delta x} \left[M_{i+1/2,j}^{k+1/2} - M_{i-1/2,j}^{k+1/2} \right]$$

$$\frac{\partial N}{\partial y} = \frac{1}{\Delta y} \left[N_{i,j+1/2}^{k+1/2} - N_{i,j-1/2}^{k+1/2} \right]$$

24 Dec 2004



Nested grids to increase resolution in critical places

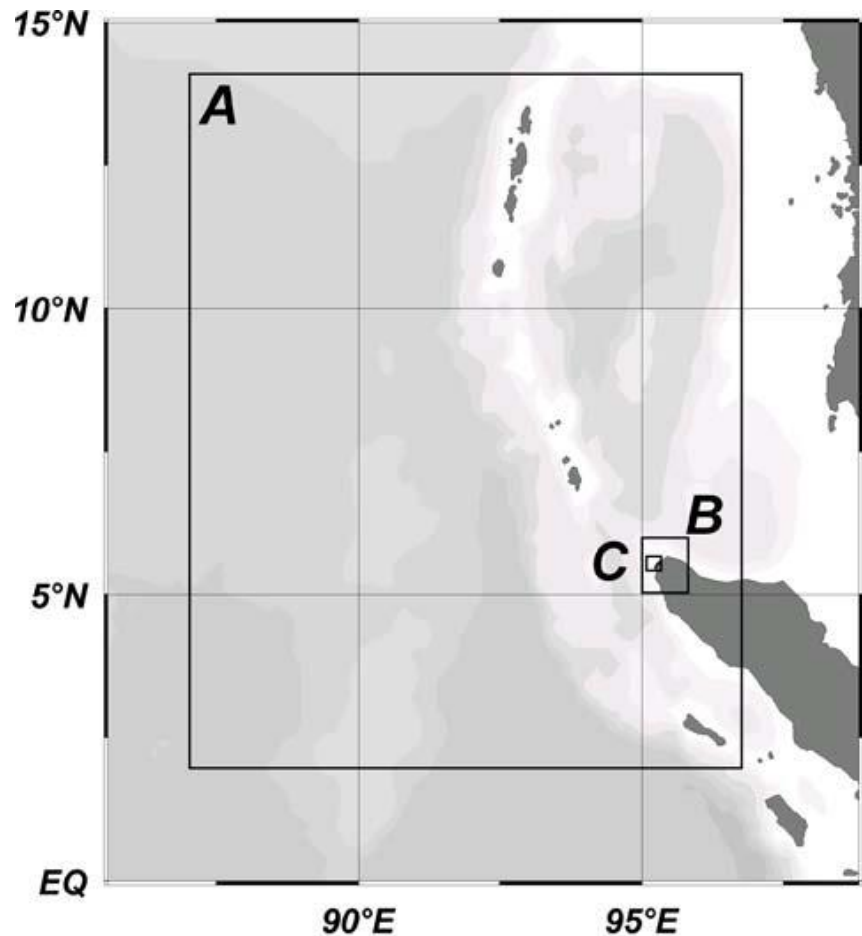
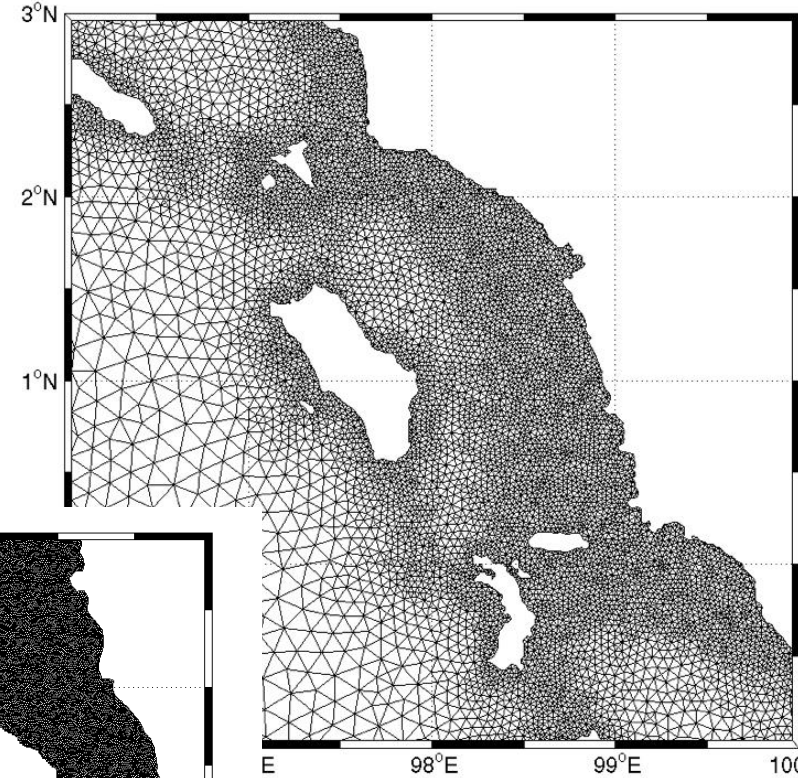
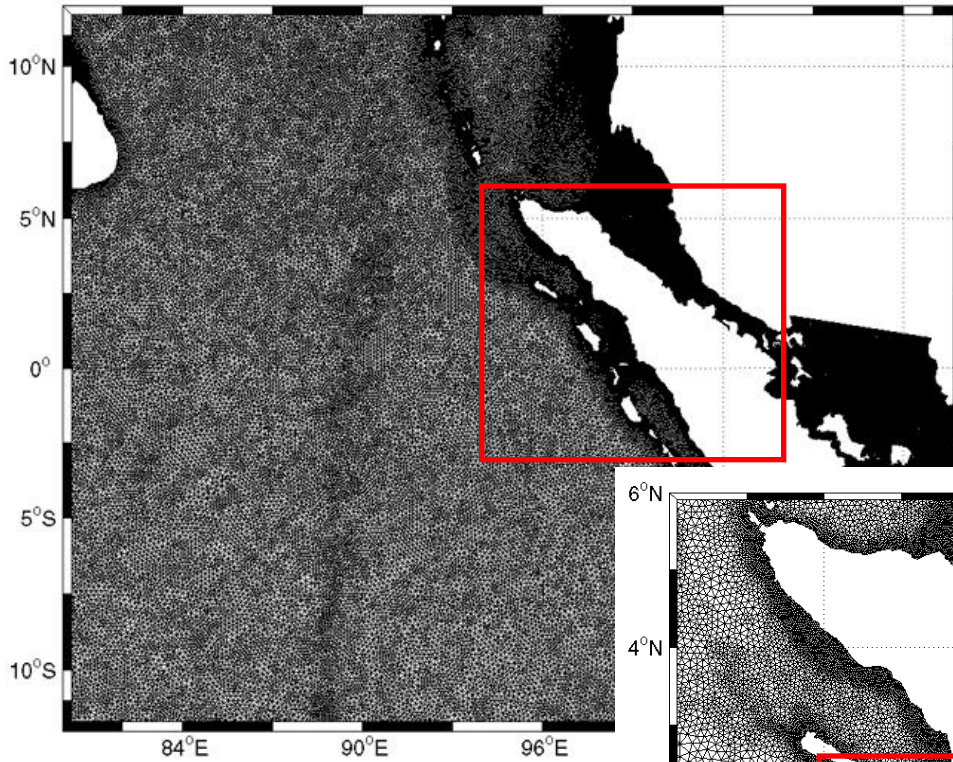


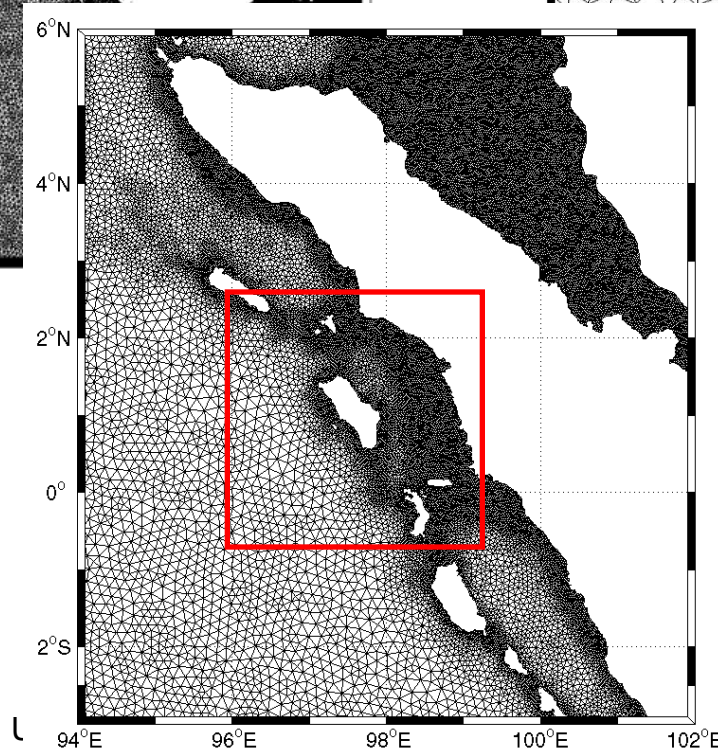
Fig. 2 The *upper panel* shows the nested grids *A*, *B*, and *C* in TUNAMI (*grid A*: $1,280 \times 1,354$ nodes, $dx = 900$ m; *grid B*: 297×357 nodes, $dx = 300$ m; *grid C*: 289×274 nodes, $dx = 100$ m).

Harig et al. (2008)

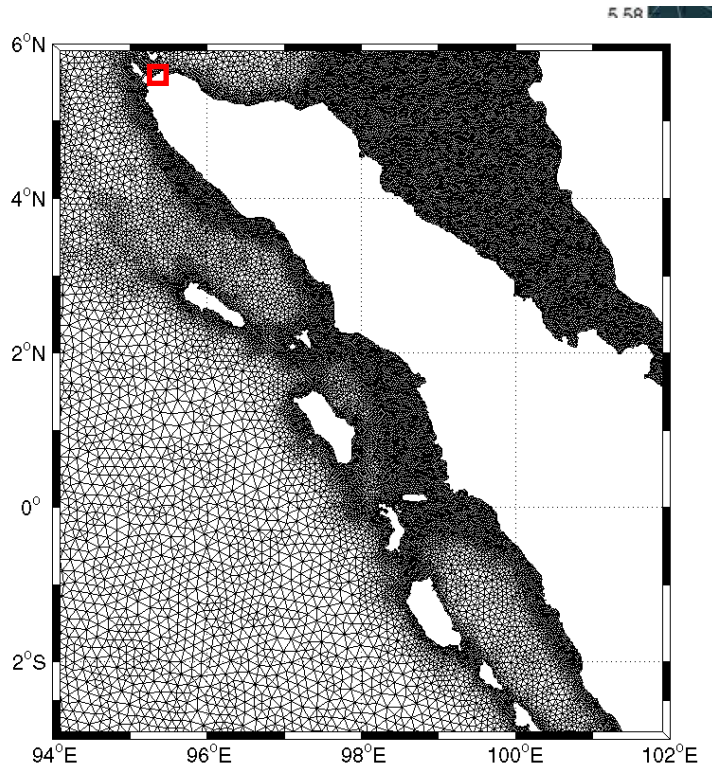
FEM calculations



GITEWS Indonesian grid:
> 4 Mio elements with
resolution down to 50 m

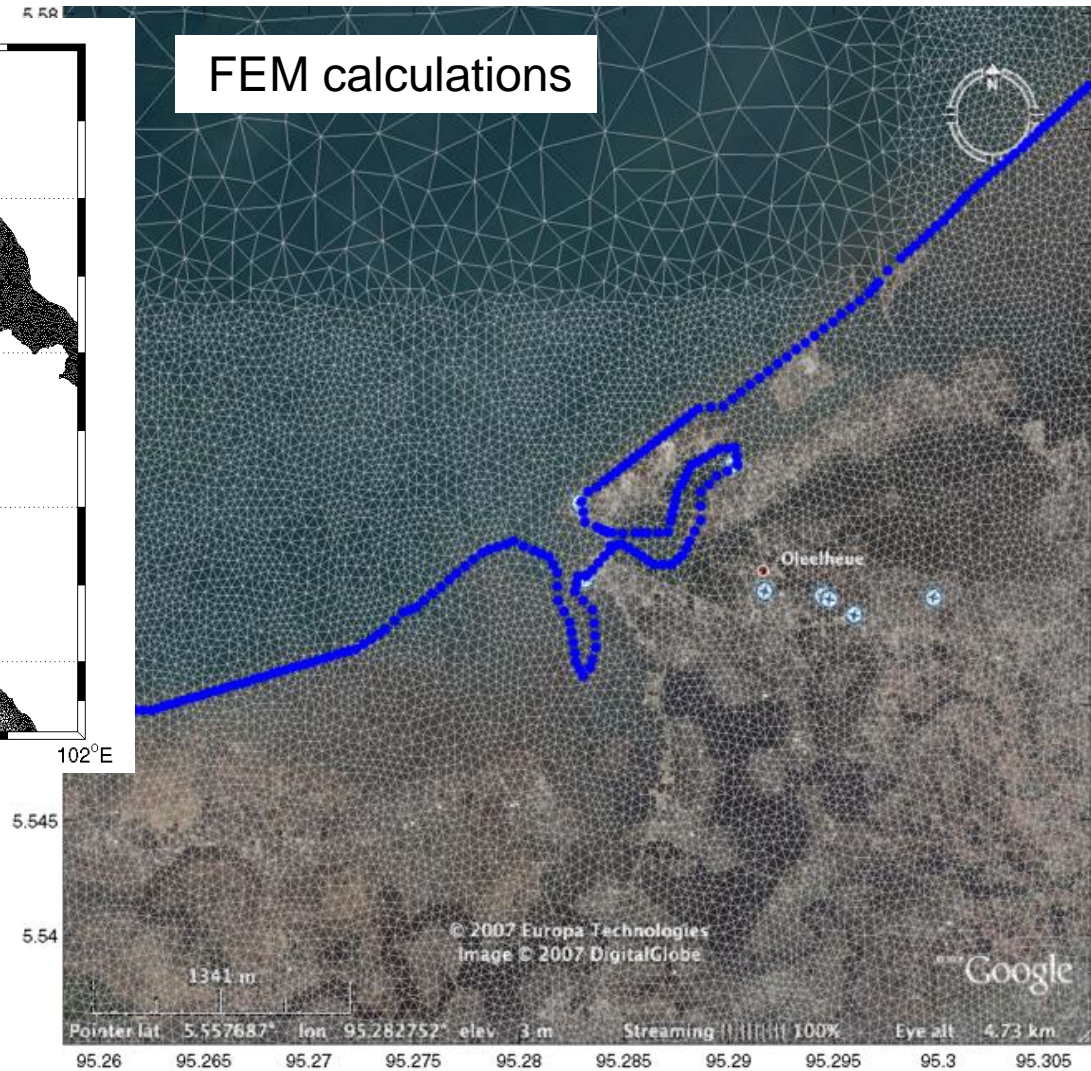


Harig et al. (2008)



Harig et al. (2008)

GITEWS Indonesian grid:
> 4 Mio elements with
resolution down to 50 m



Comments on simulation of wave run-up and coastal inundation

- Most demanding to data resolution and accuracy as well as to computational cost
 - Global bathymetry and topography datasets not enough
 - Grid resolution ~10 m: tens of million of nodes
- High-resolution local data on topography often not available
- Approximations from deep water (~ 50-100 m depth) is commonly used
 - Green's law: $h_2 = h_1 * (d_2/d_1)^{1/4}$
 - Use precomputed 1D characteristic profiles

Numerical Modeling for:

1. Tsunami early warning
2. Tsunami hazard assessment
3. Integrative testing of the TEWS
4. Personnel teaching and training

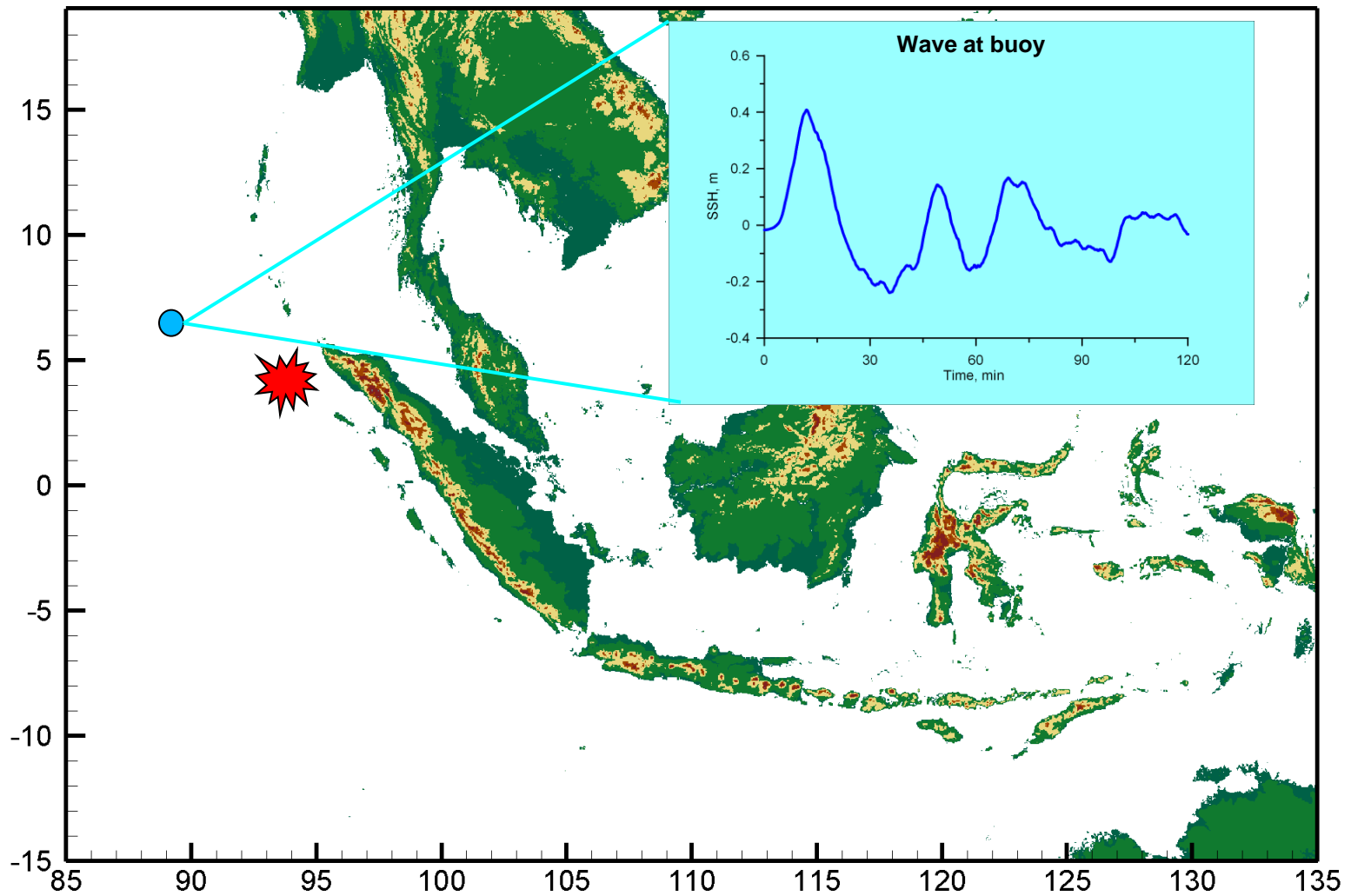
Numerical Modeling for:

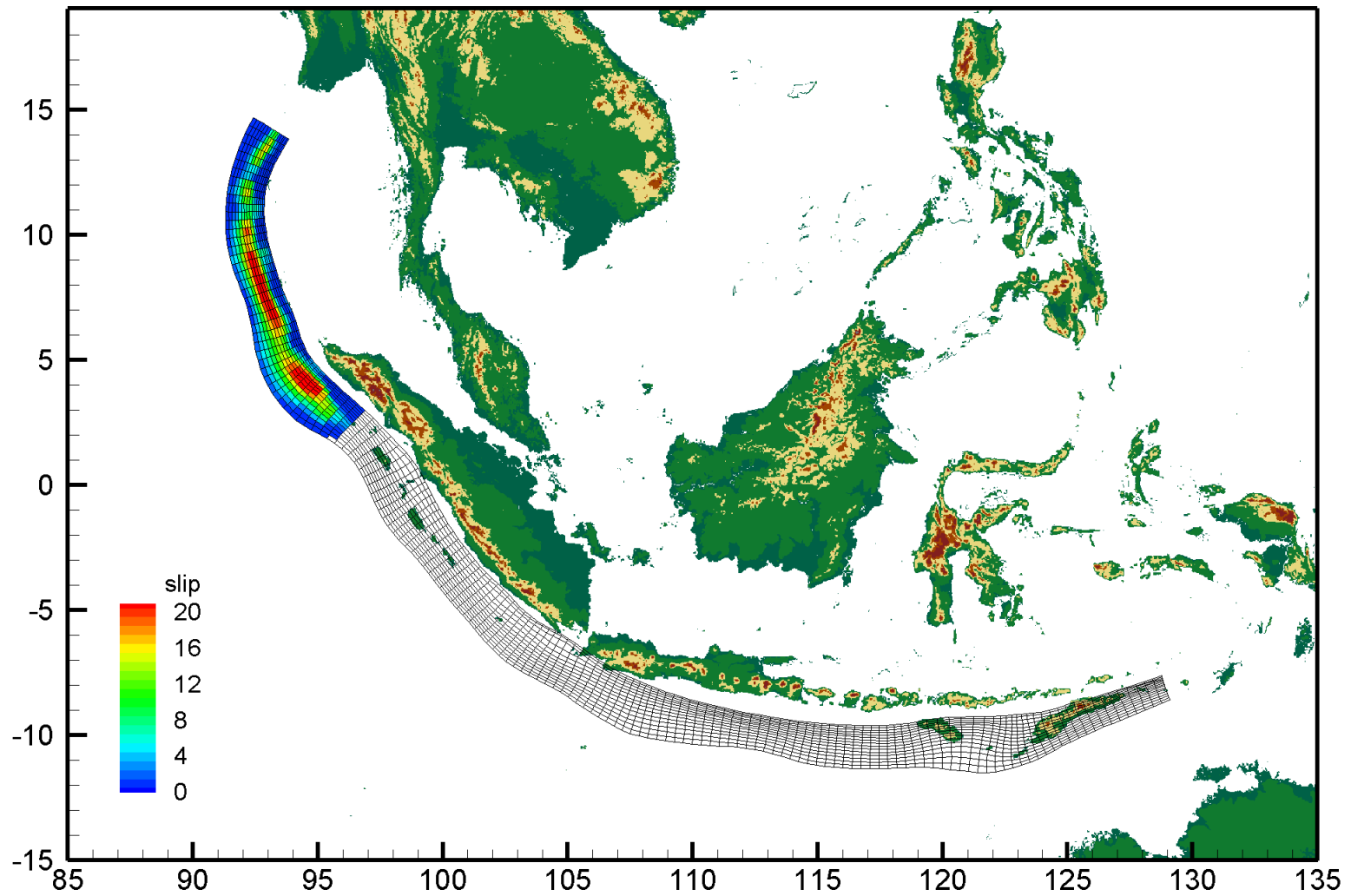
1. Tsunami early warning
2. Tsunami hazard assessment
3. Integrative testing of the TEWS
4. Personnel teaching and training

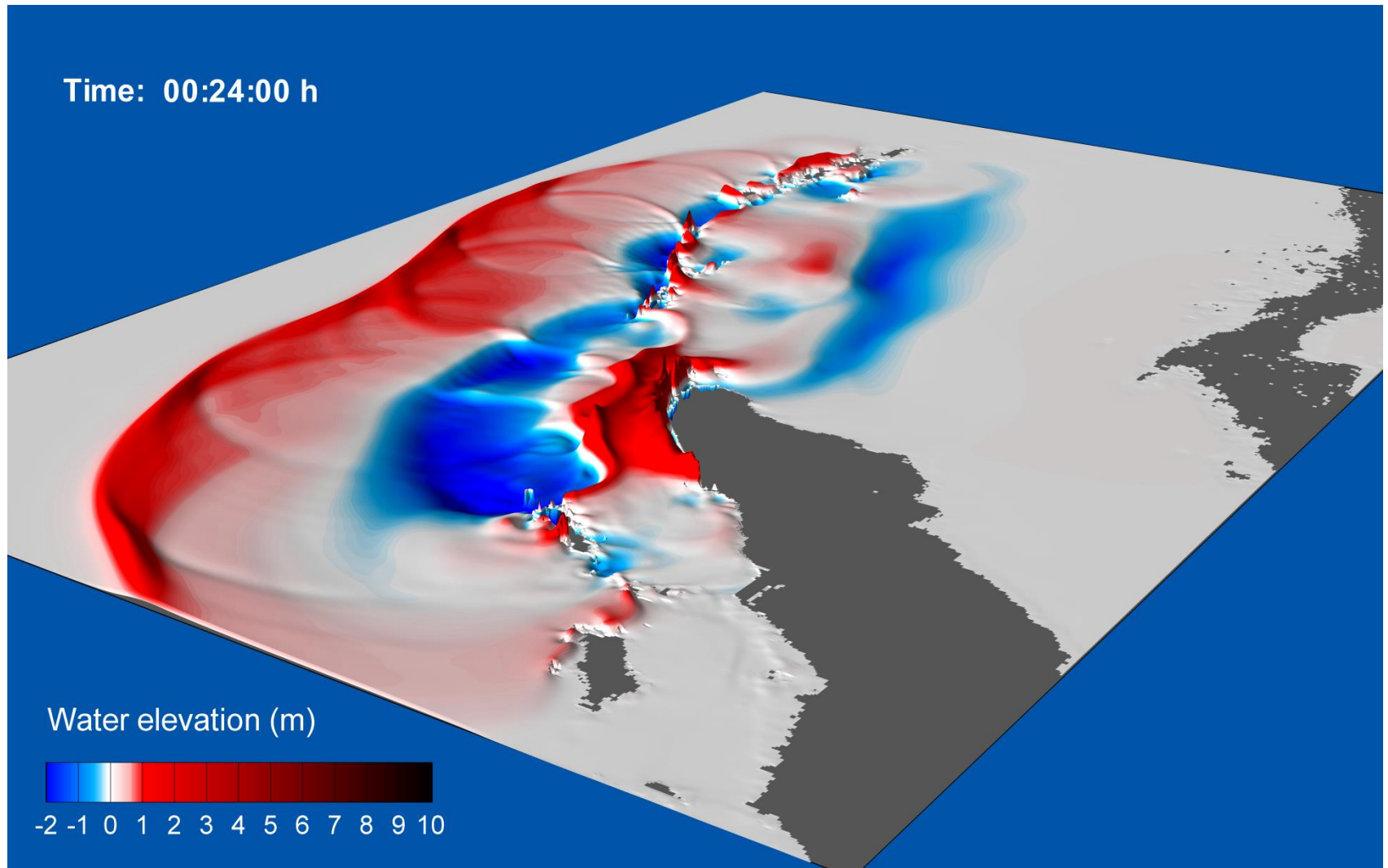
Modeling for Tsunami Early Warning ...

... to understand a physical process.

To get a consistent picture of what has happened,
what is still going and what is expected to be ...







Tsunami Early Warning Systems: Principles of Operation

Far-field (PTWC, India, Australia,...):

there is some time to take decision

more tolerant to the source: important are Mw and orientation

Near-field (Japan, Indonesia, Chile,...):

extremely short warning times

needs source position, geometry and slip distribution

Far-field: Pacific Tsunami Warning Center

New: **SIFT** – **Short-term Inundation Forecasting for Tsunamis**
based on concept of unit sources and their Green's functions

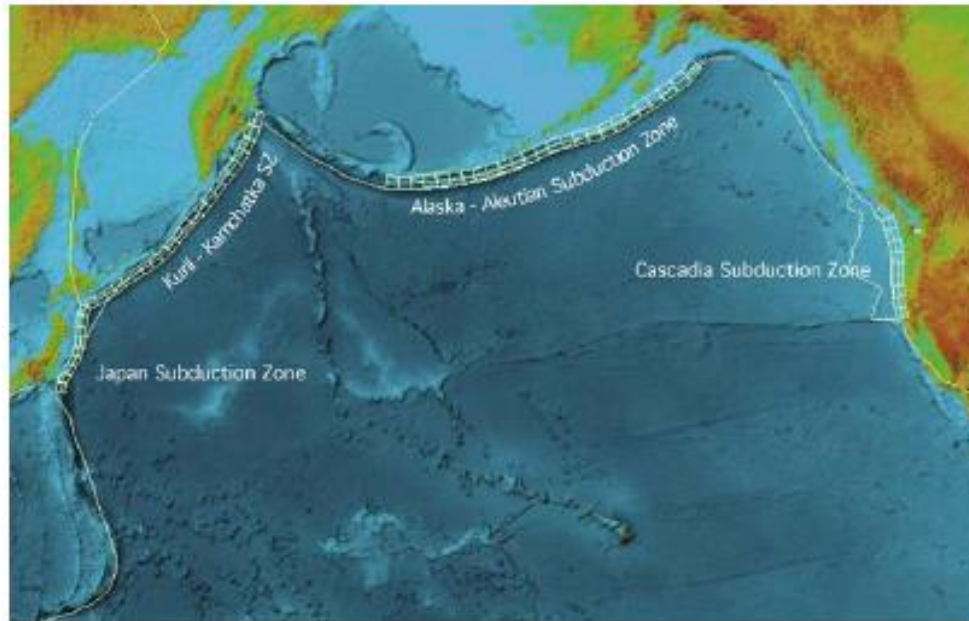
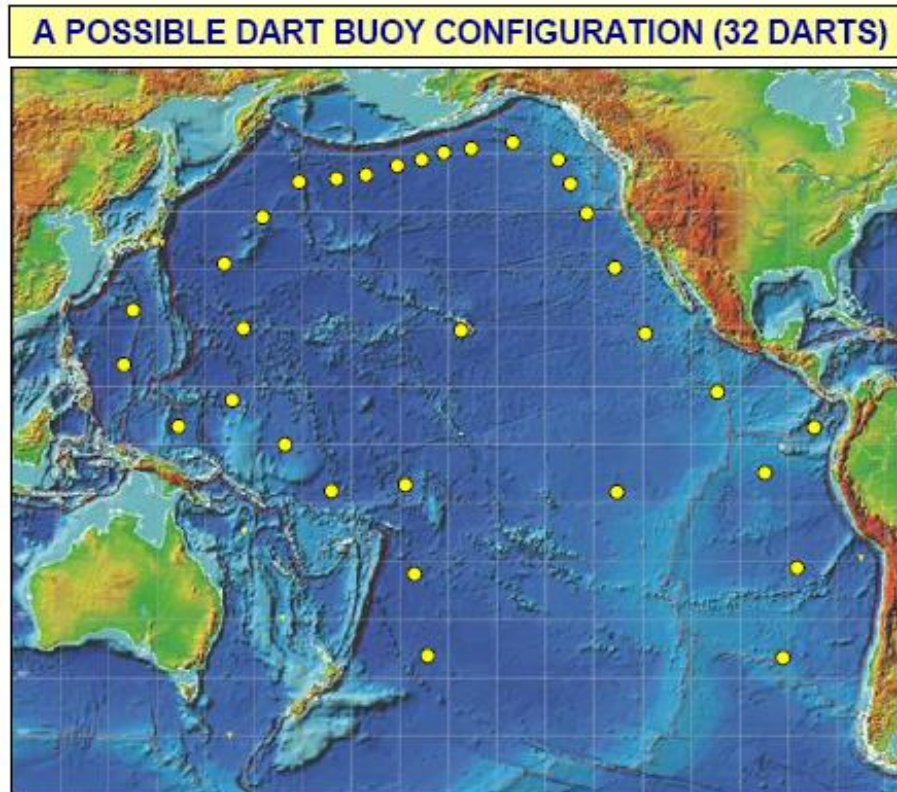


Figure 5. North Pacific details of the Pacific-wide forecast model database. Bathymetric data for the database computation is shown as a shaded relief map. White rectangles show fault planes for the unit sources included in the database. Major plate boundaries are shown as white lines.

Titov et al. (2005)

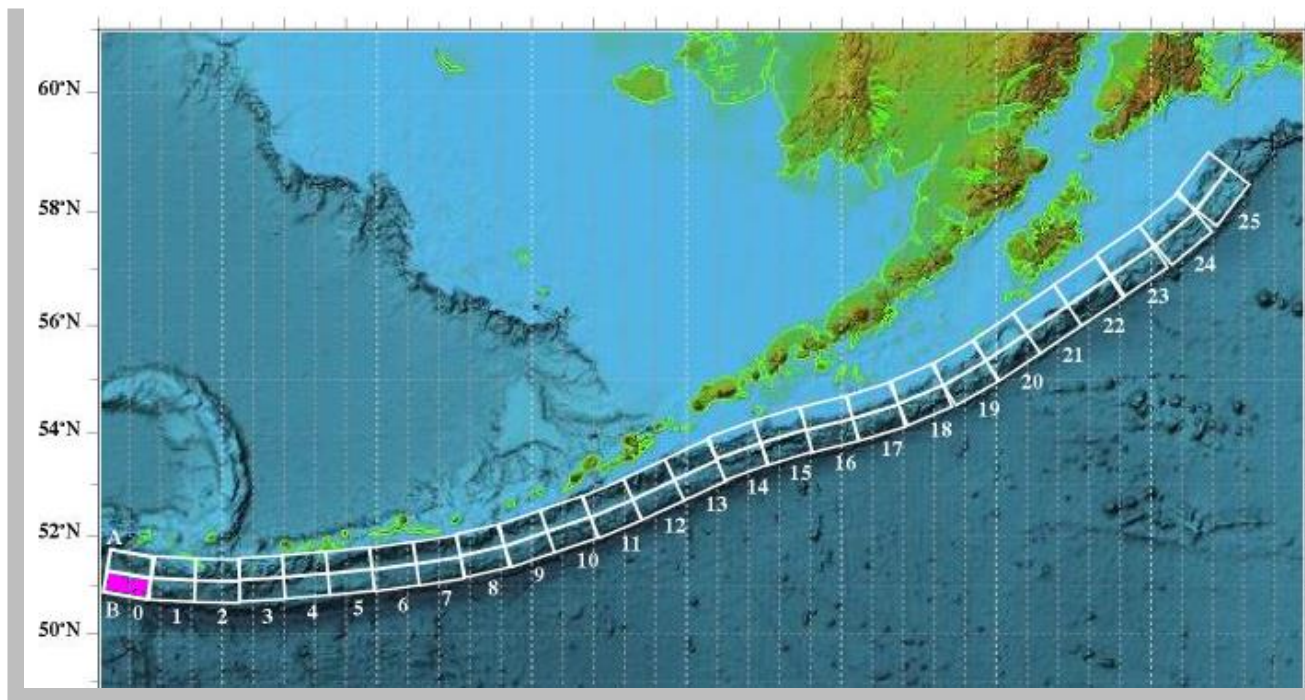
New: **SIFT** – **Short-term Inundation Forecasting for Tsunamis**



from presentation of McCreery (2005)

New: **SIFT** – **Short-term Inundation Forecasting for Tsunamis**

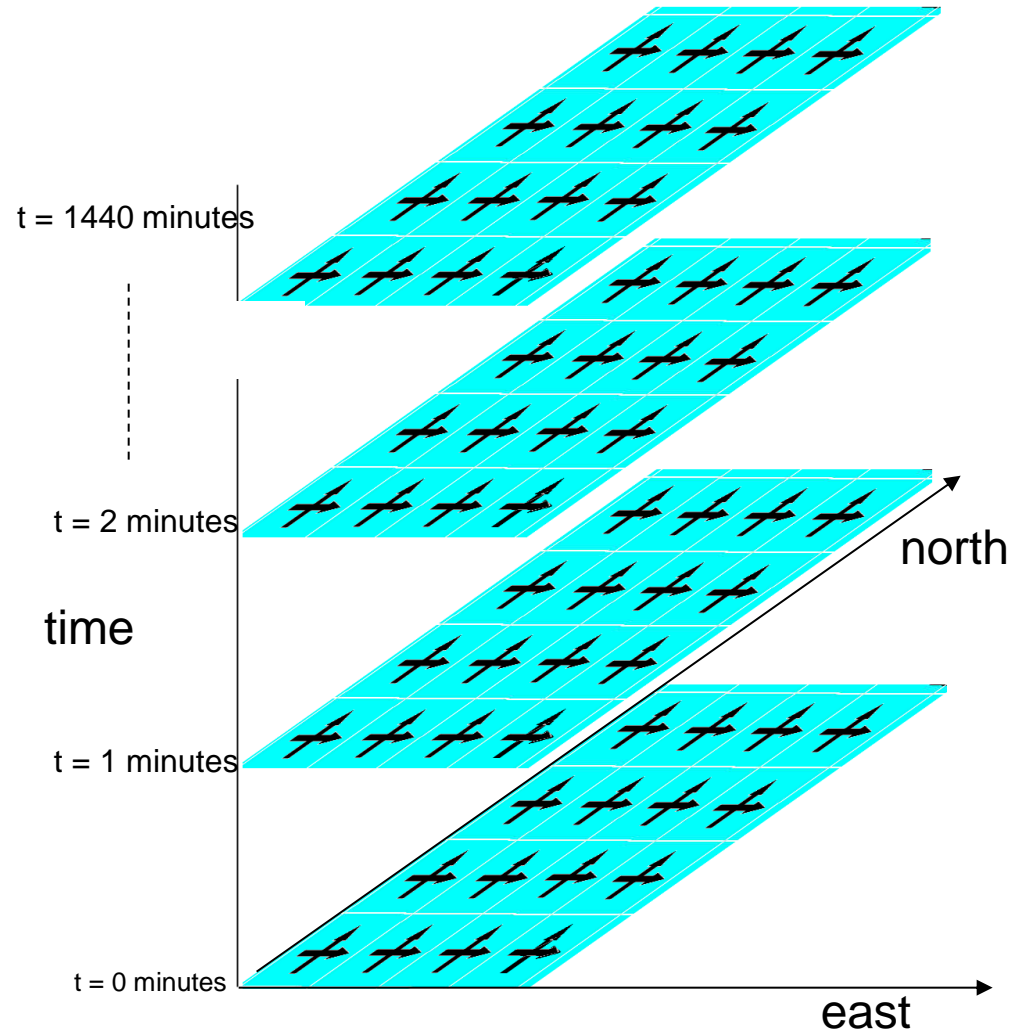
- Each 'fault box' (labeled a0..an, b0...bn below) is an independent source location. One ~7 GByte dataset is computed for each box, using an Mw 7.5 , 1 m slip seismic source. This defines a 'unit source'.
- A weighted combination of stored data from several sources produces the final wave prediction we will use during an event.
- The 'best' combination is obtained by matching prediction to real time DART data. That's the inversion step



from presentation of G. Freyer (2006)

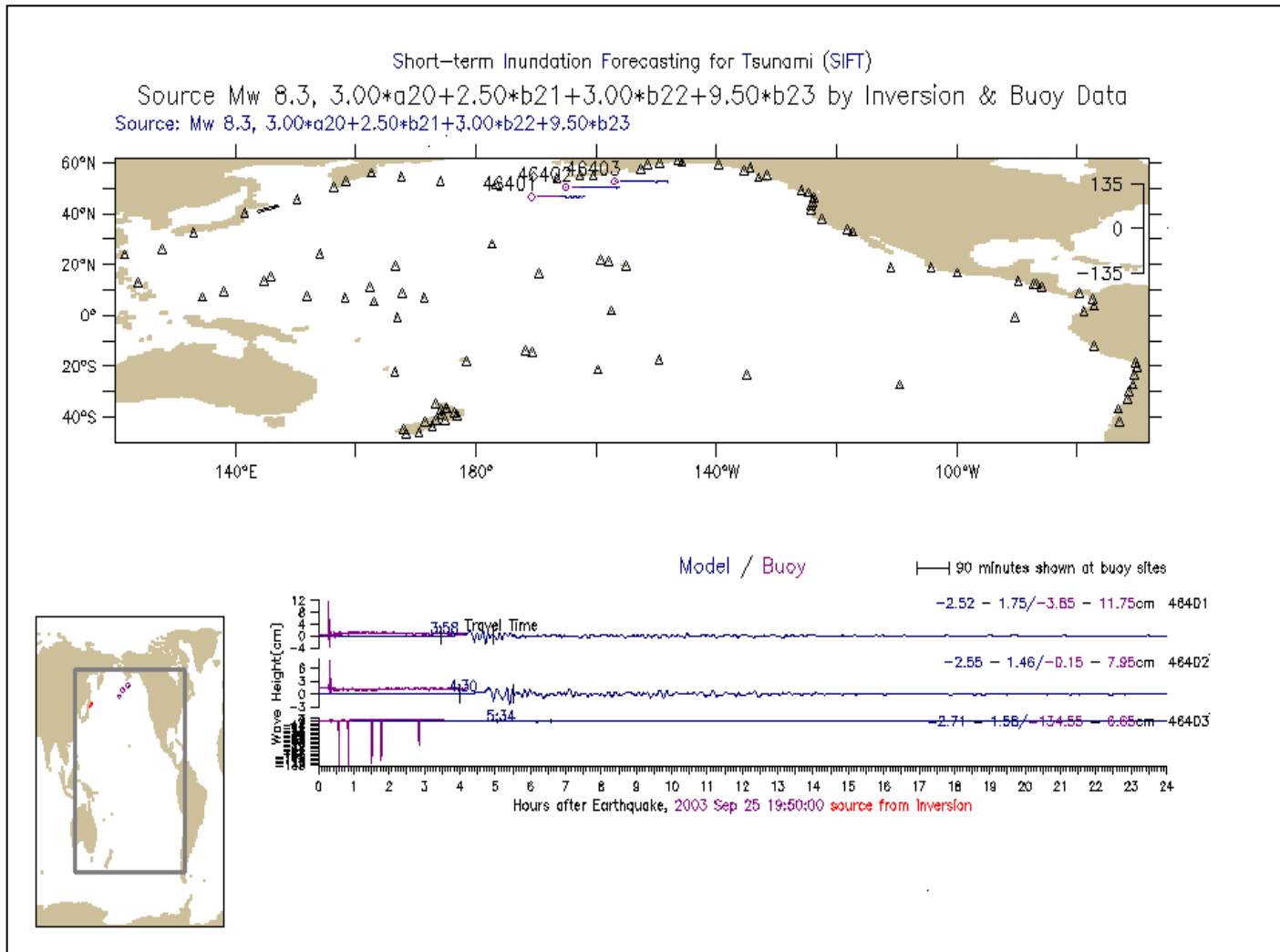
New: **SIFT** – **Short-term Inundation Forecasting for Tsunamis**

- One 16 min x 16 min full Pacific 'snapshot' is stored for each minute of wave evolution starting at event time ($t = 0$) and ending 1 full day later. So, 1441 'snapshots'
- 3 variables per cell and roughly 200,000 rectangular cells cover the Pacific from 50S to 62N. This requires 0.6 million stored output values for each one-minute snapshot.
- Multiplying the above by 1441 one minute snapshots gives about 7 Gbytes of storage space required for each wave source.



from presentation of G. Freyer (2006)

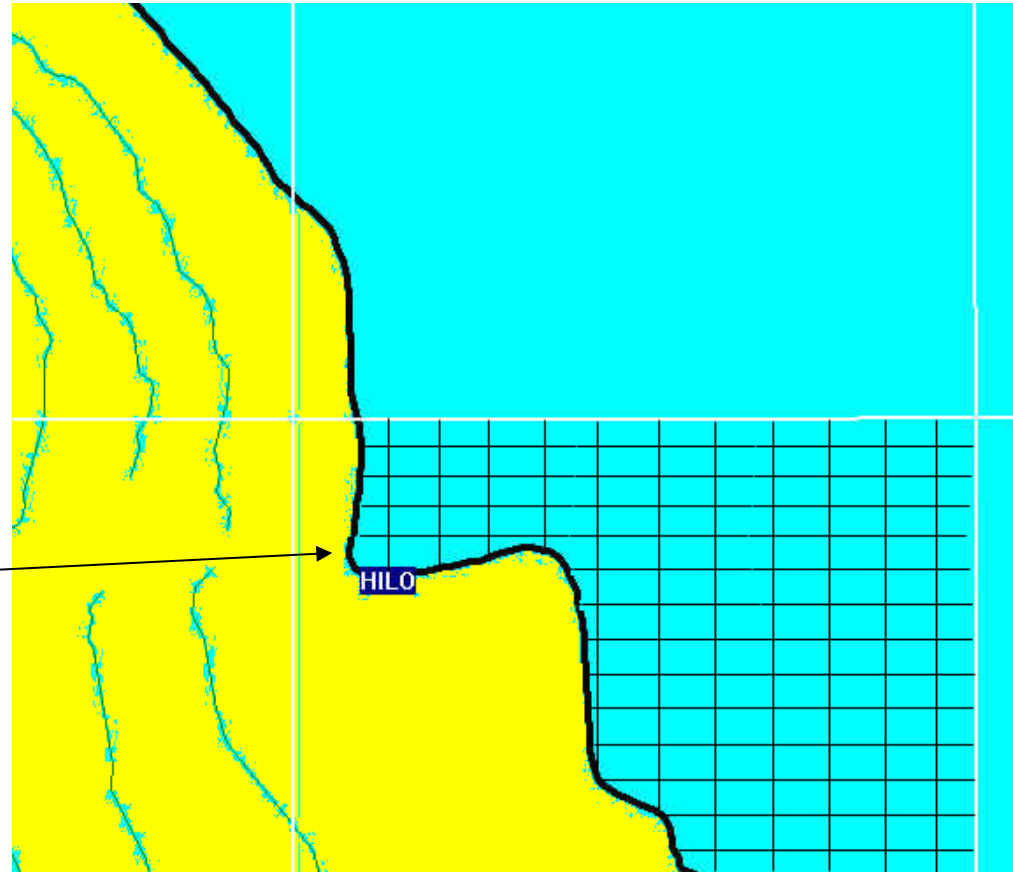
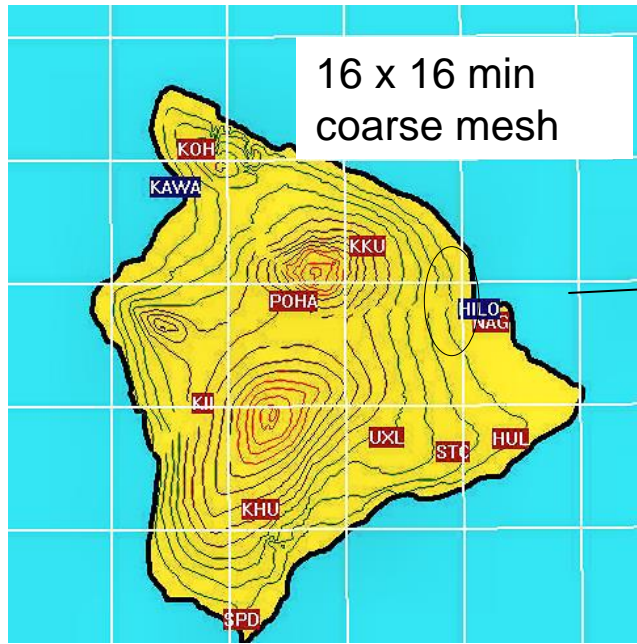
New: SIFT – Short-term Inundation Forecasting for Tsunamis



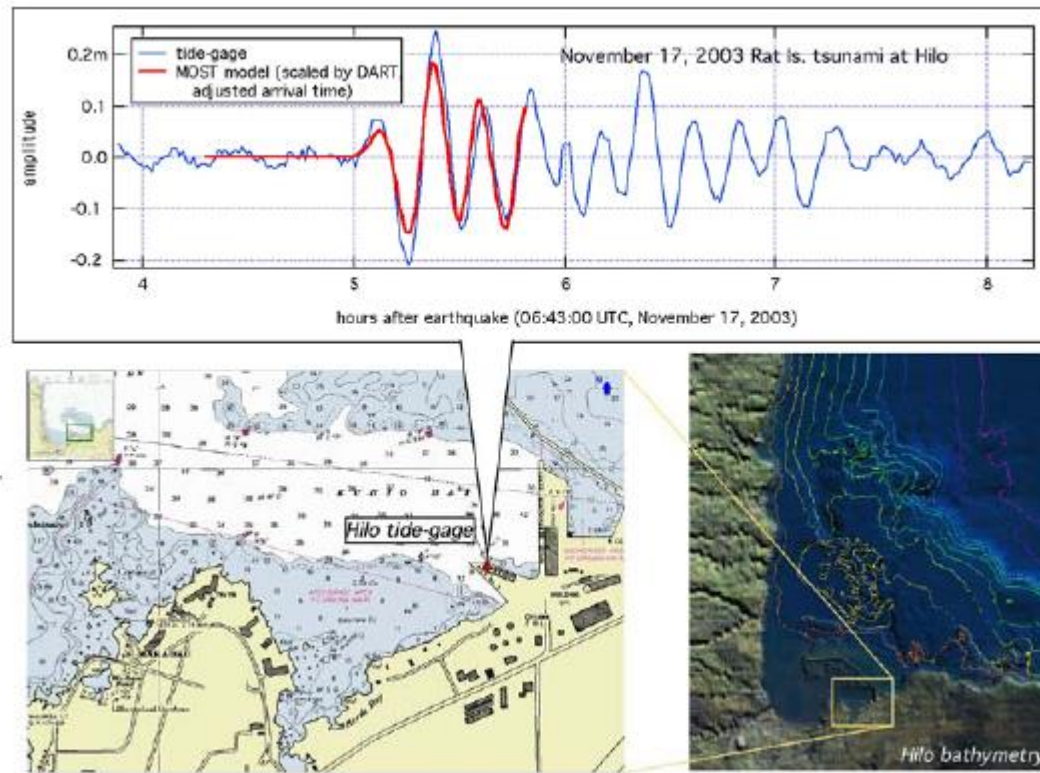
from presentation of G. Freyer (2006)

New: **SIFT** – Short-term Inundation Forecasting for Tsunamis

After the best 16 min x 16 min solution is obtained, the data is used to 'drive' more finely meshed coastal regions for prediction of warning point runup.



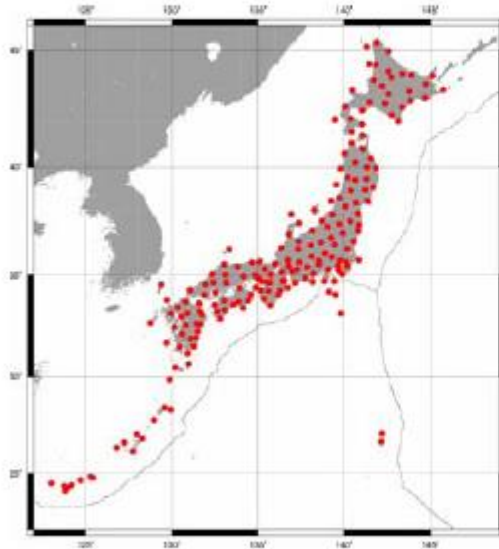
from presentation of G. Freyer (2006)

New: **SIFT** – **Short-term Inundation Forecasting for Tsunamis**

from presentation of McCreery (2005)

Japanese Tsunami Warning System

JMA Seismic Network

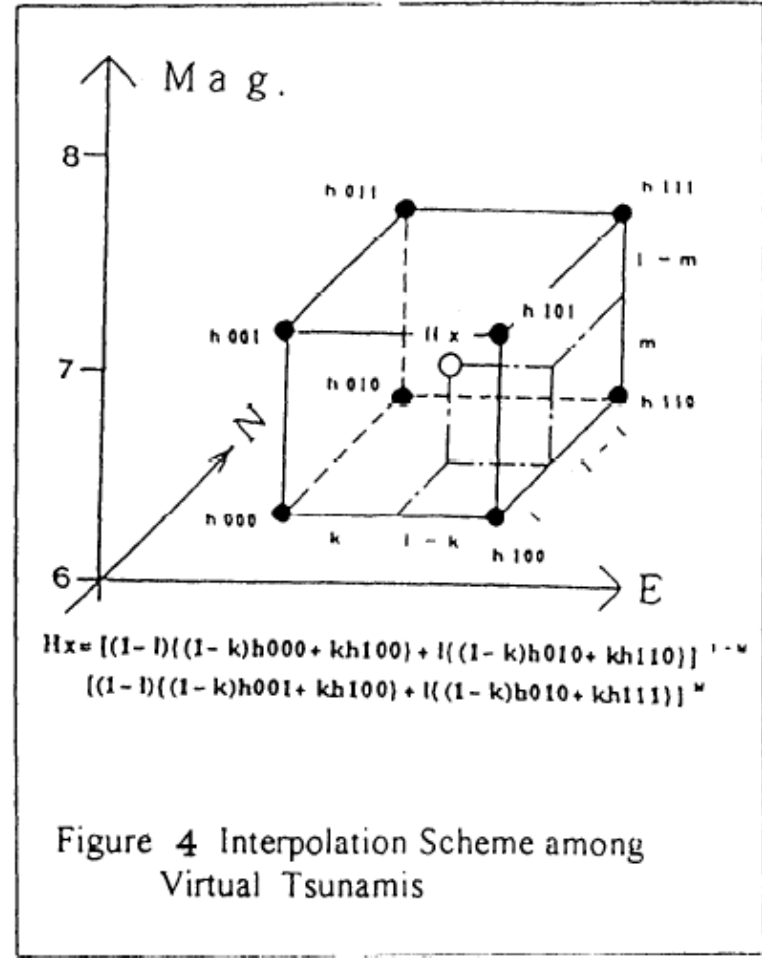
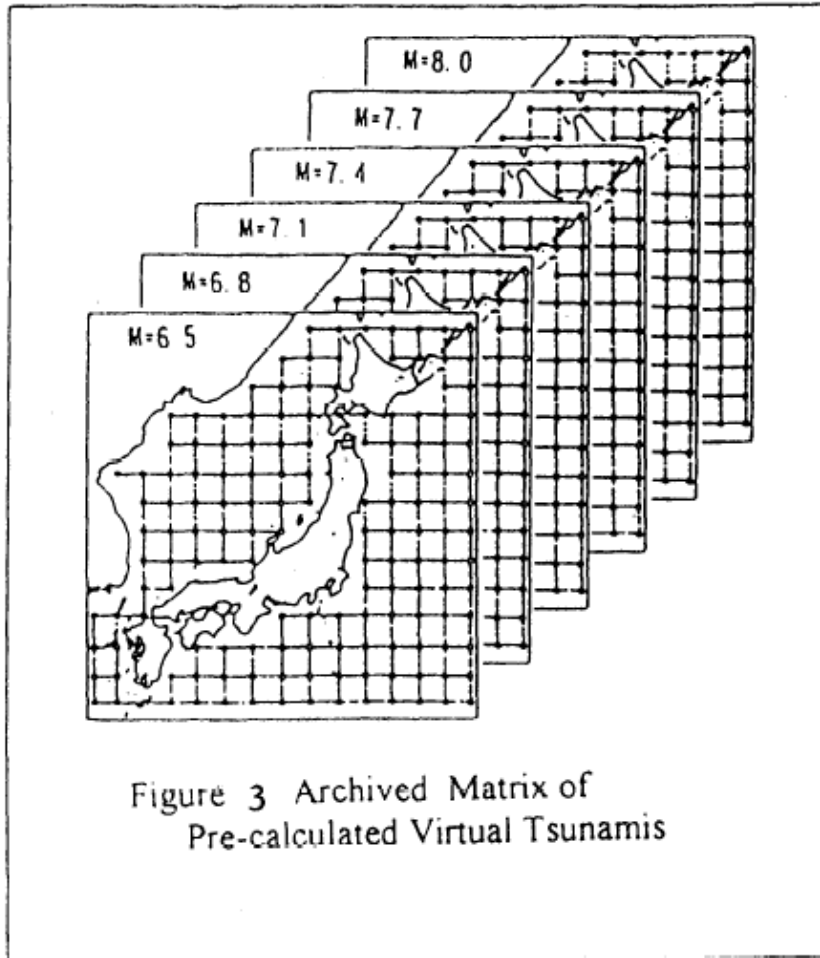


Sea Level Network



Satake (2005)

Databank of virtual tsunamis



Science of Tsunami Hazards, Vol 17, No. 2 (1999) page 101

Furumoto et al. (1999)

Tsunami Warning System: Example

21:37 earthquake



21:40 First bulletin

An earthquake occurred at
21:37 Feb. 26, 2005

First bulletin at 21:40
"Seismic intensities 3 and 4
reported"



21:41 Second bulletin

Second bulletin 21:41
"An earthquake occurred at 21:37,
Latitude 40.7N, longitude 142.5E
Depth 70 km, M 5.4
No tsunami from this earthquake"

Satake (2005)

Numerical Modeling for:

1. Tsunami early warning
2. Tsunami hazard assessment
3. Integrative testing of the TEWS
4. Personnel teaching and training

- Similar to earthquakes, tsunamis will take place in the future worldwide and collect their toll
- To minimize negative impact, society needs preparedness and early warning
- Preparedness starts from hazard assessment

Tsunami hazard assessment: 2 approaches

Deterministic scenario-based

- Worst case scenarios
- Does not provide recurrence periods of tsunamis
- Challenges high-resolution modeling

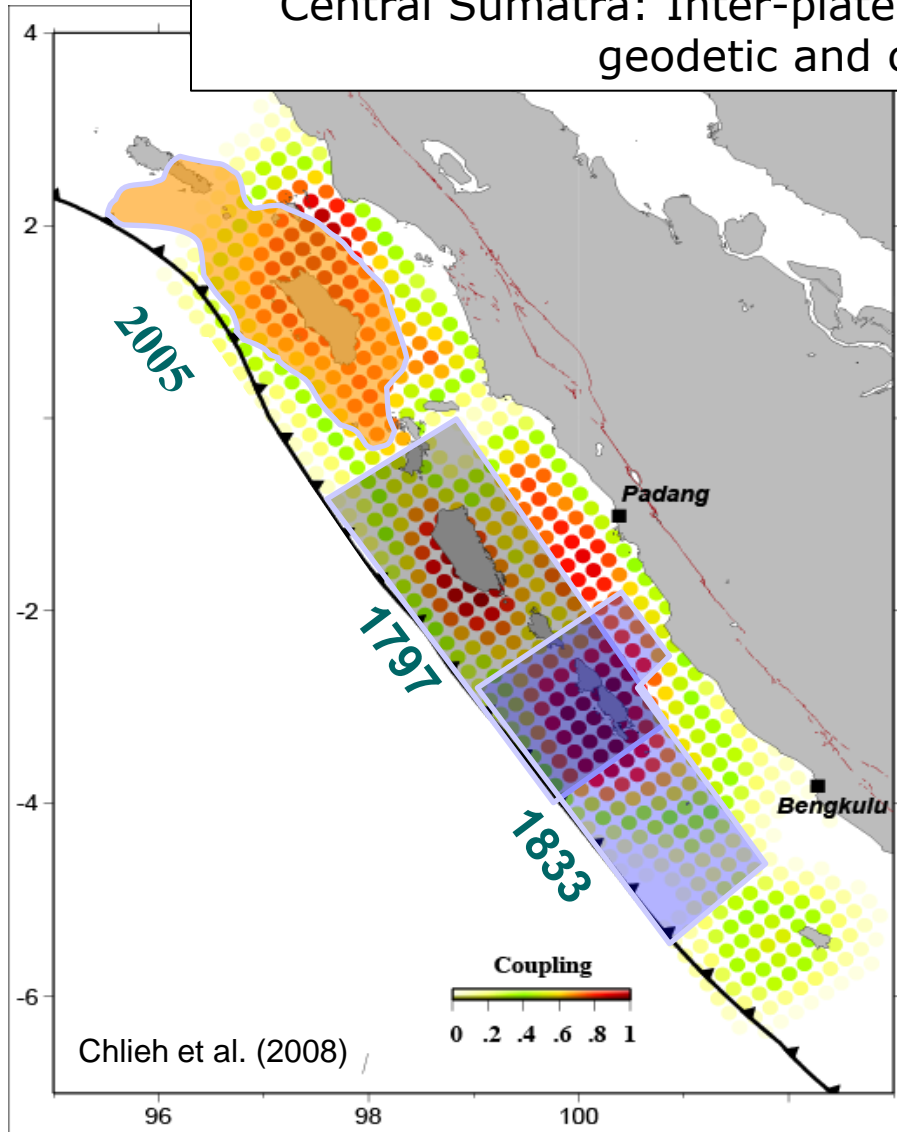
Oriented at coastal planning and early warning

Probabilistic approach

- Huge number of scenarios aggregated
- Provides recurrence periods of tsunamis of different wave heights (hazard curves)

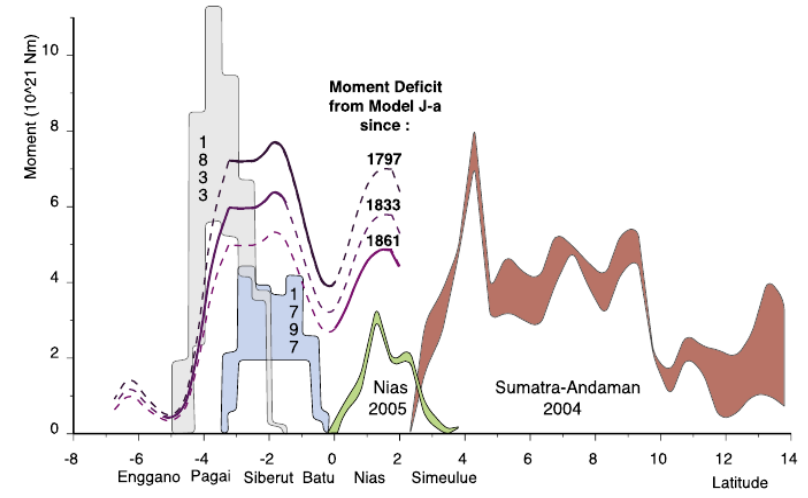
Oriented at engineering and risk assessment

Central Sumatra: Inter-plate coupling as revealed by geodetic and coral data

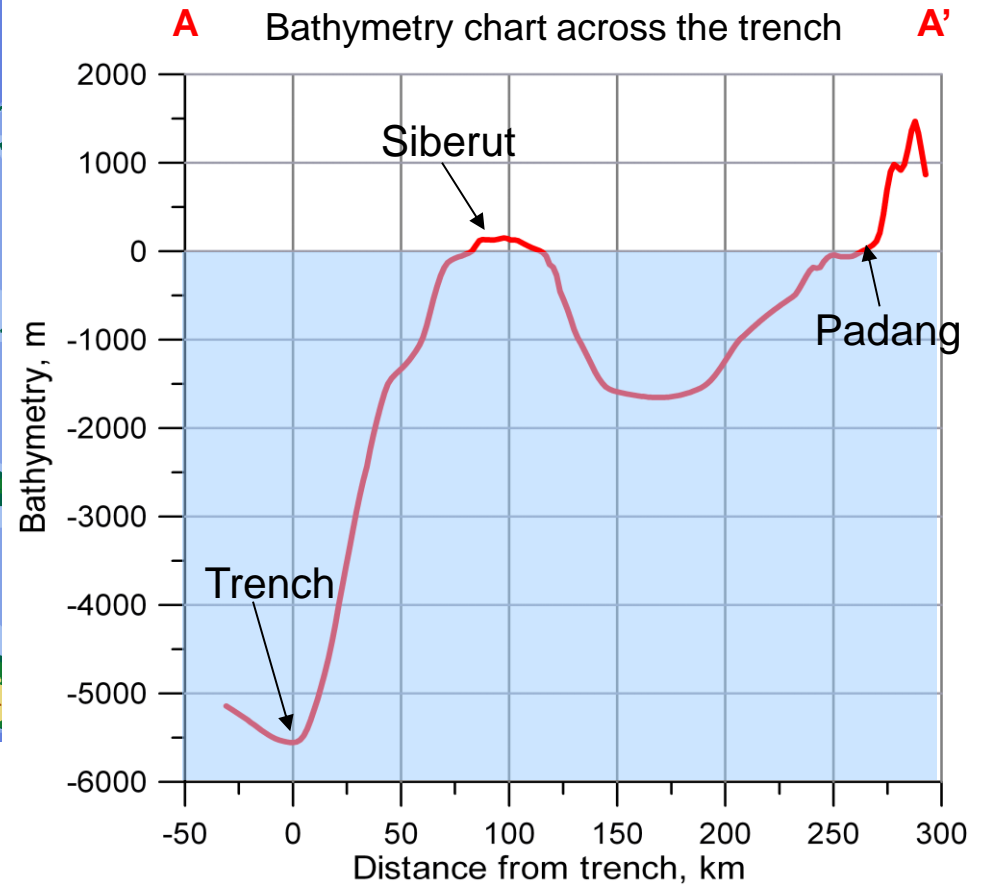
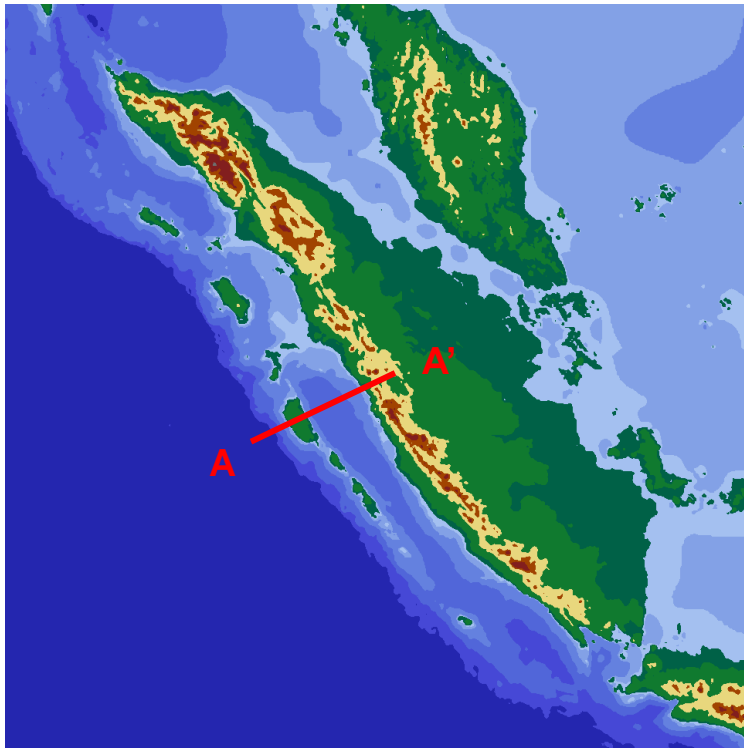


Full locking during ~200 years results in about:
 $200 \text{ y} * 5.5 \text{ cm/y} = 11 \text{ m}$
 accumulated slip.

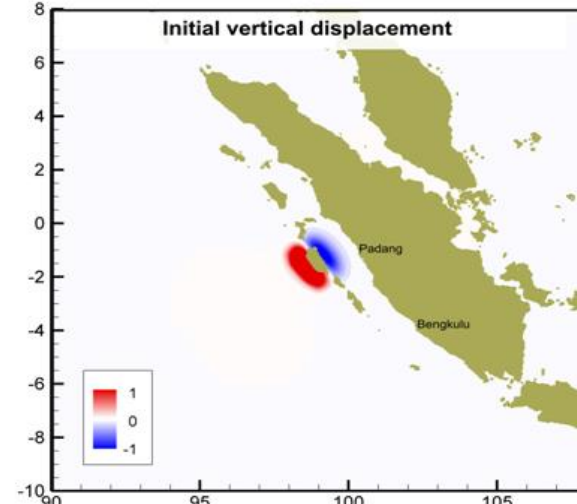
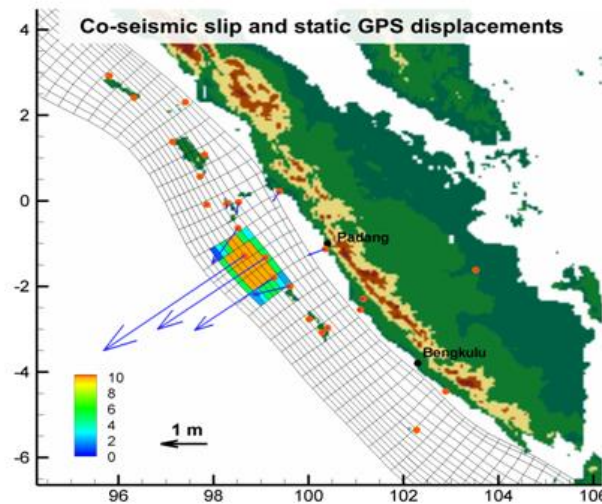
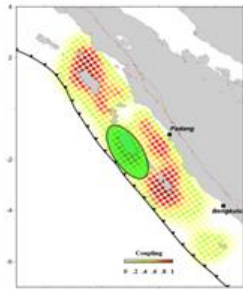
Accumulated seismic moment deficit after Chlieh et al. (2008)



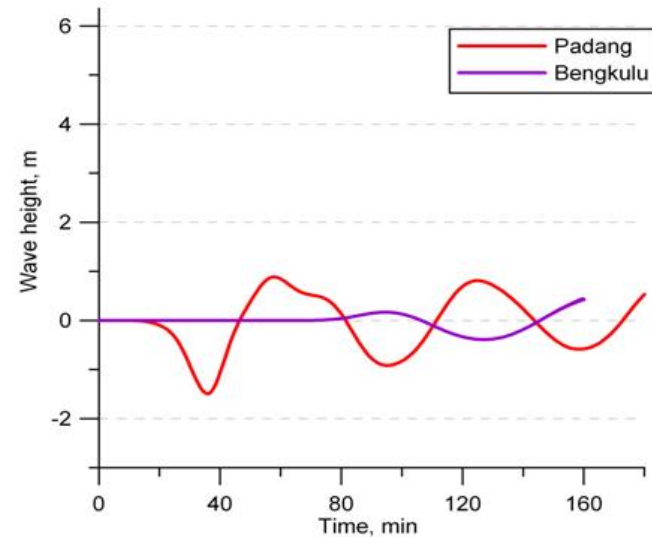
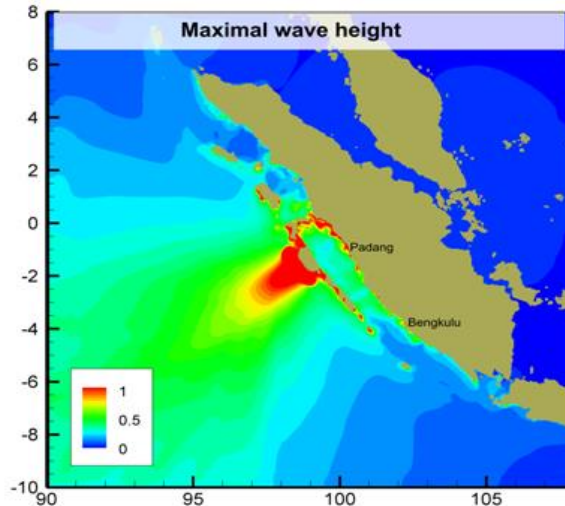
Bathymetry off Padang: An important player



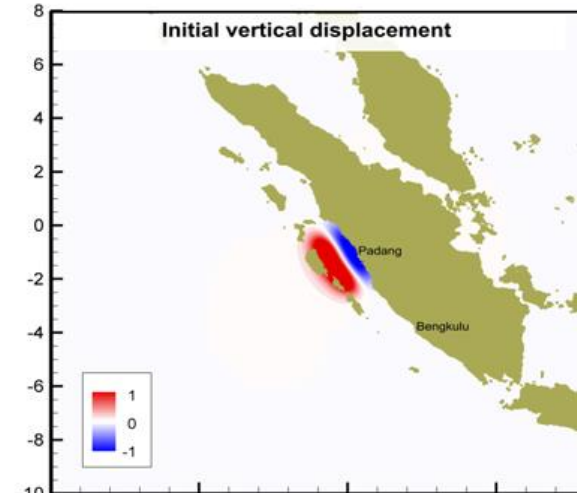
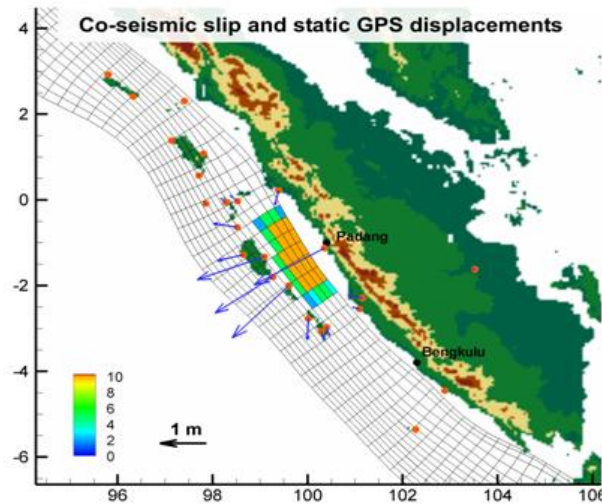
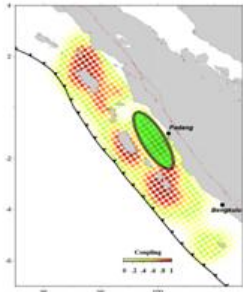
RUPTURING PATCH P1



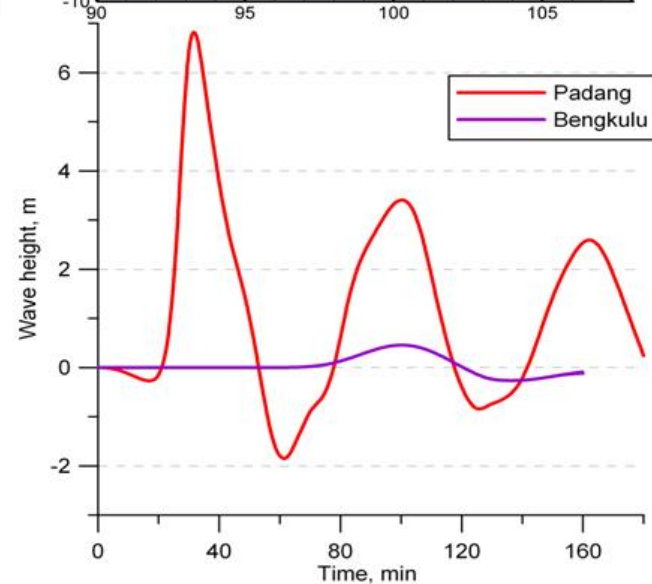
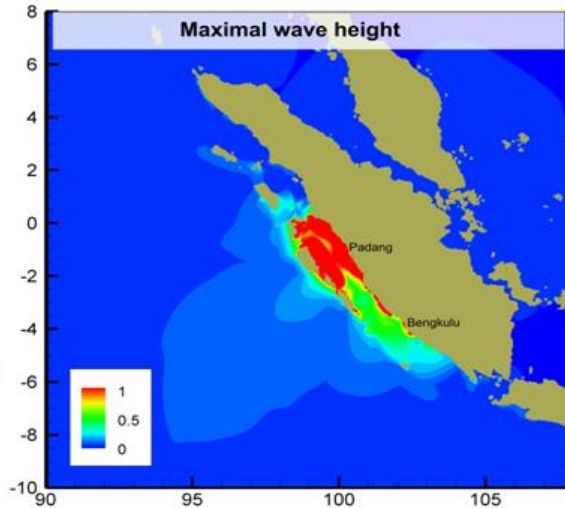
Padang is effectively protected by the Mentawai islands: minor tsunami after ~50 min.



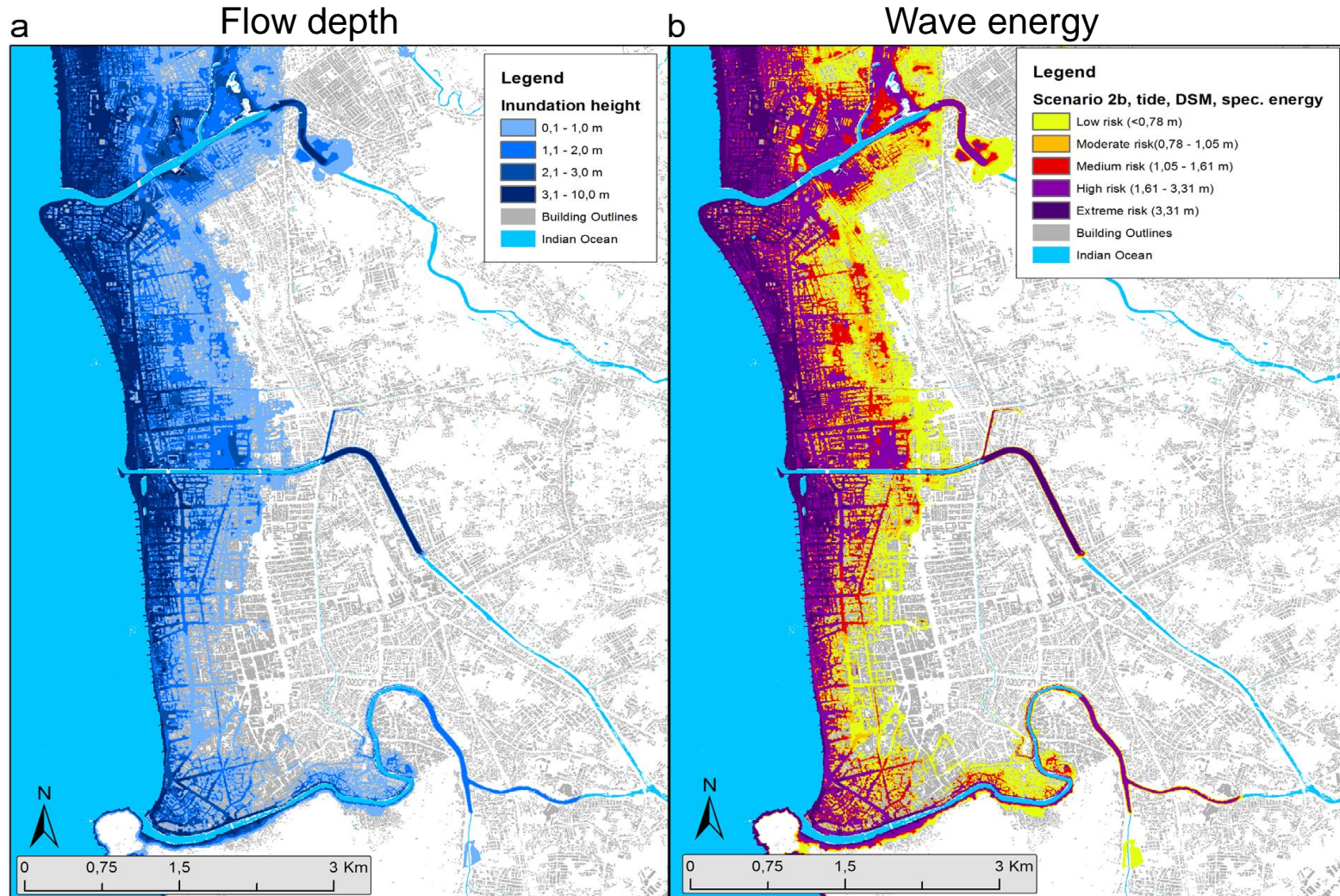
RUPTURING PATCH P2



Tsunami energy is trapped between the Mentaway chain and Sumatran coast. Strong inundation after 30 min in Padang.



High-resolution inundation modeling for city of Padang, Sumatra (Indonesia)

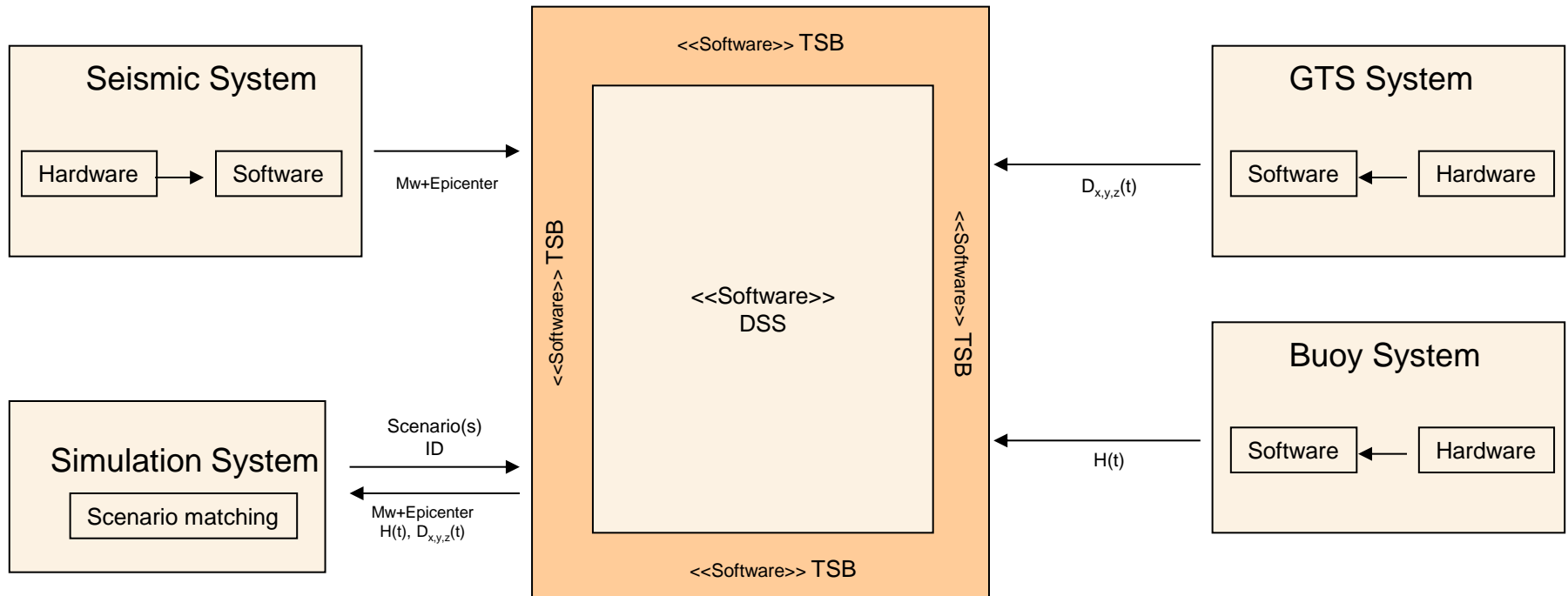


Taubenböck et al. 2013

Numerical Modeling for:

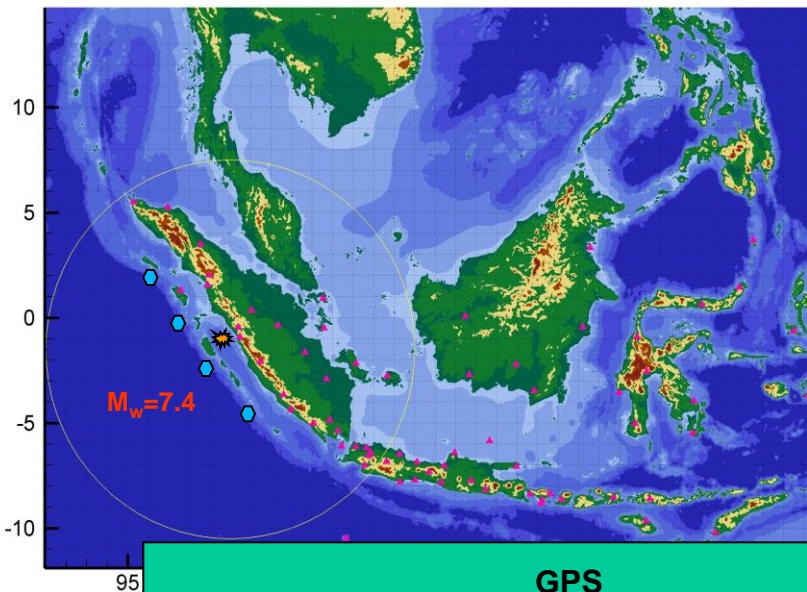
1. Tsunami early warning
2. Tsunami hazard assessment
3. Integrative testing of the TEWS
4. Personnel teaching and training

Simplified System Architecture

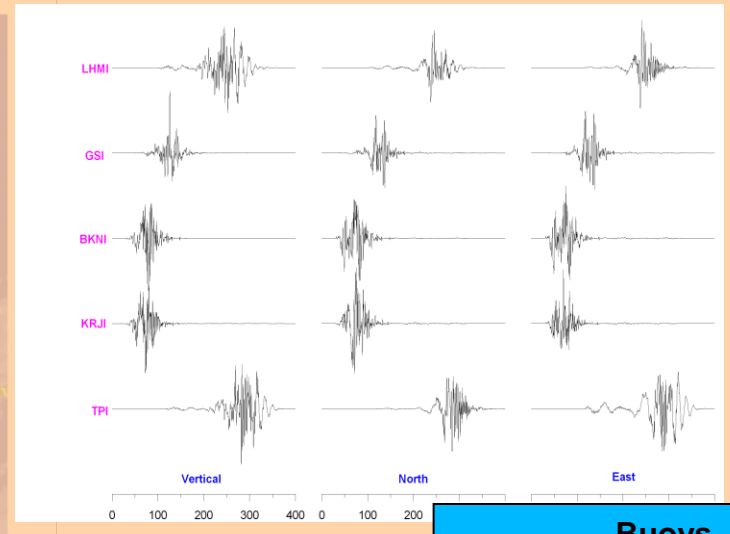


Complete synthetic scenarios of rupture and corresponding sensor responses

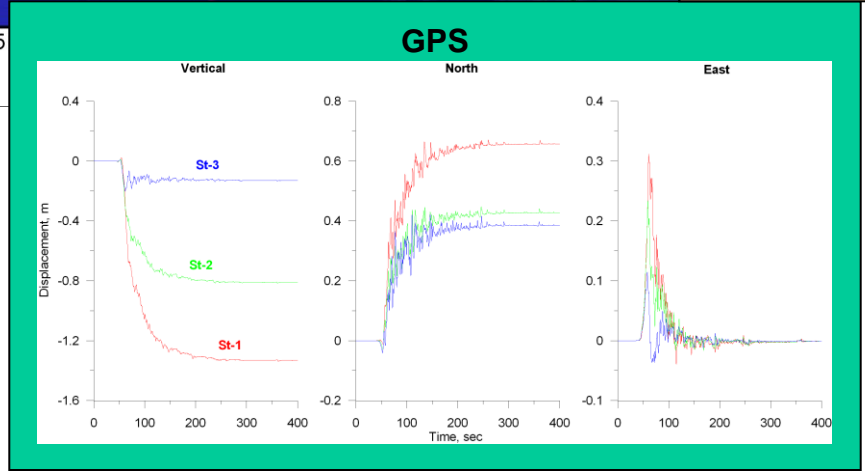
Synthetic Earthquake



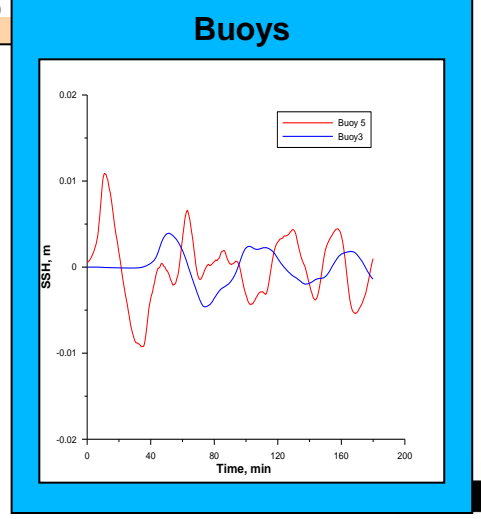
Seismic



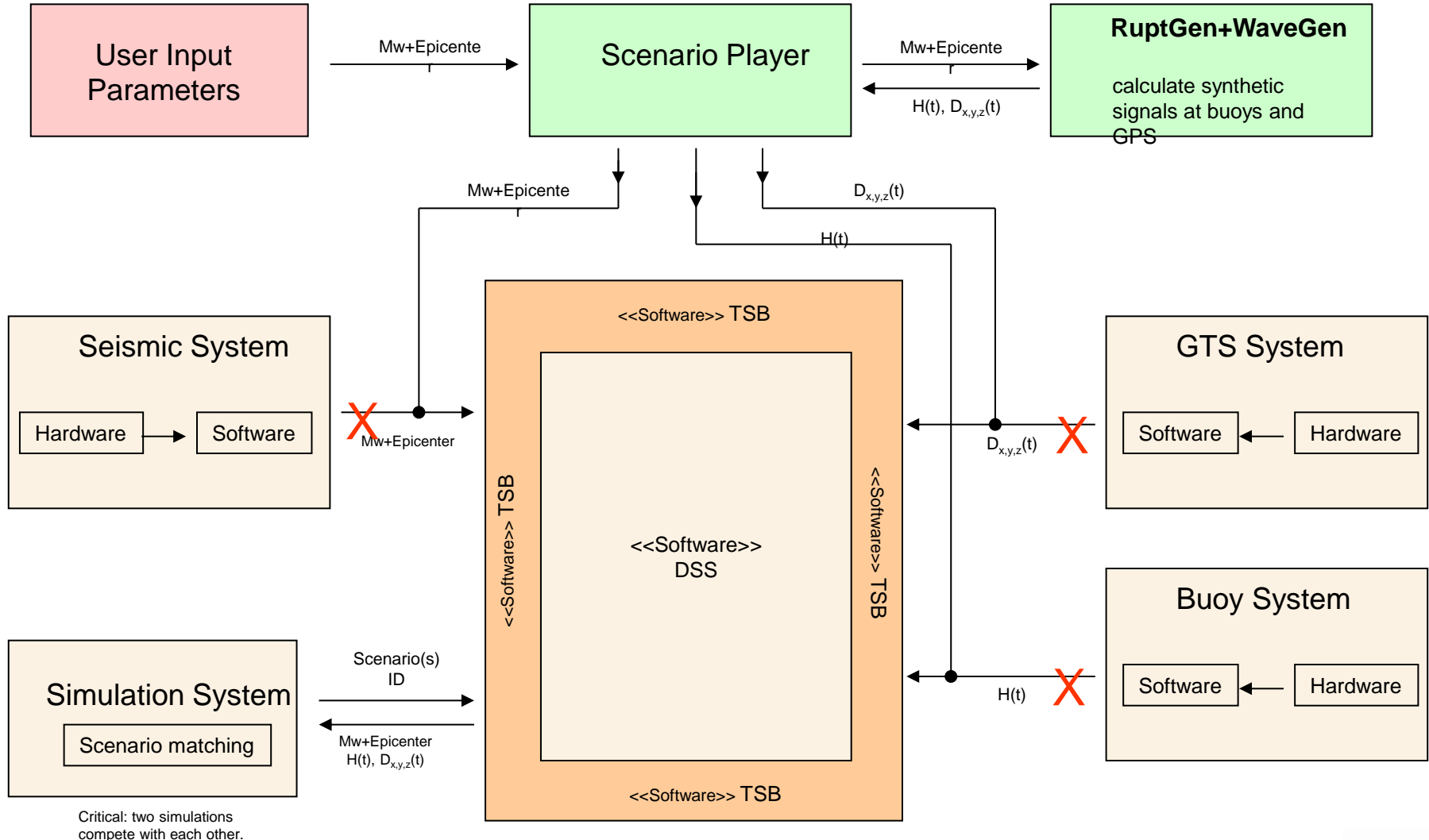
GPS



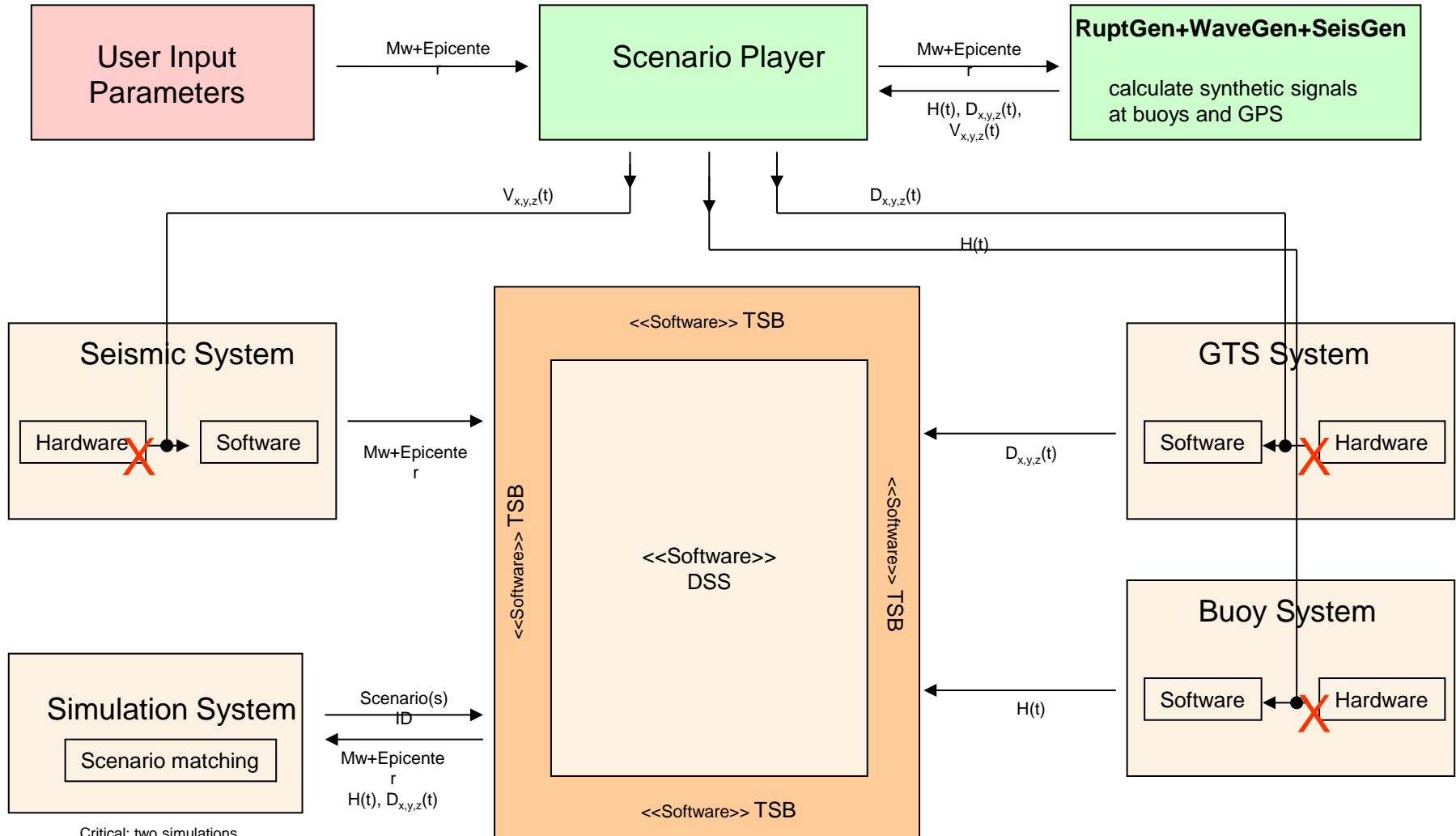
Buoys



Simulated sensor data are realistic and consistent with each other in time and magnitude.
 Simulation is probably the only way to supply TSB and DSS with feeds of fully consistent sensor data of various nature.



Simulated sensor data are realistic and consistent with each other in time and magnitude.
 Simulation is probably the only way to supply TSB and DSS with feeds of fully consistent sensor data of various nature.



Critical: two simulations compete with each other.

Numerical Modeling for:

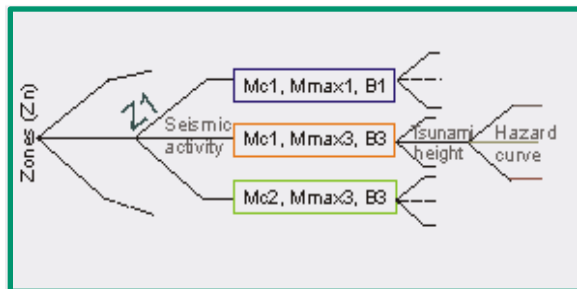
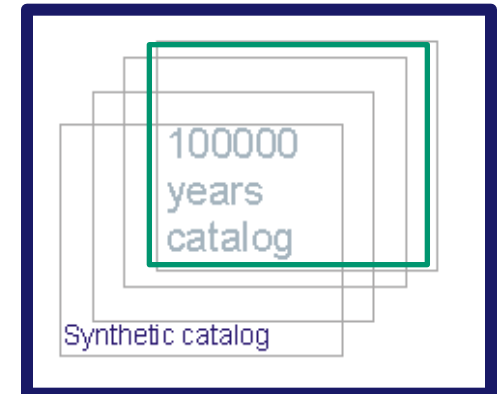
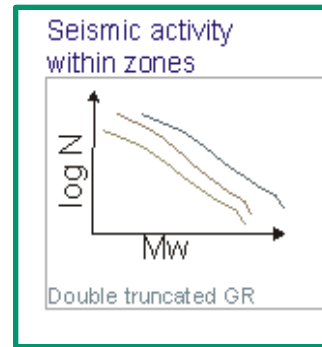
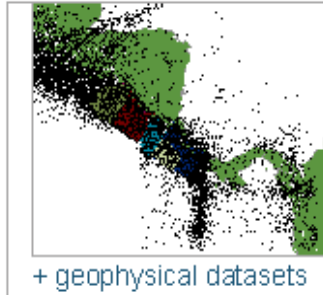
1. Tsunami early warning
2. Tsunami hazard assessment
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Probabilistic approach: seismic PTHA

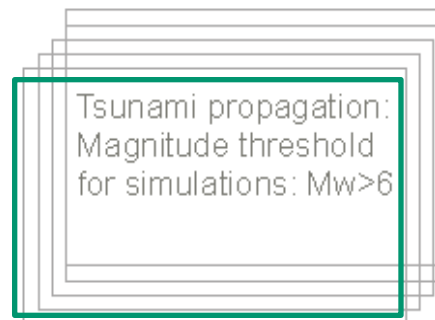
- a. Based on extensive local catalogs of tsunamis: **empirical**
- b. Based on earthquake catalogs and tsunami simulations: **computational**

Steps of probabilistic analysis

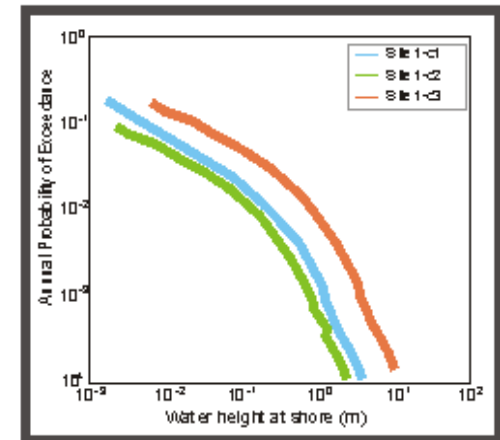
Seismic catalog



Logic trees: epistemic uncertainty



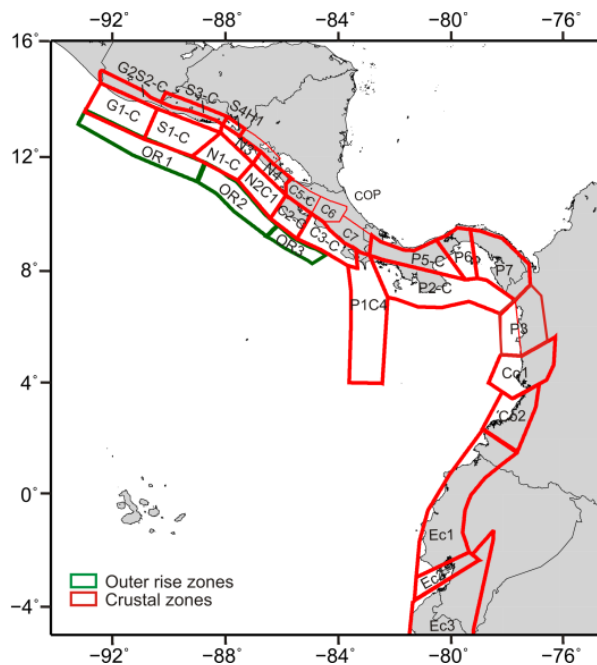
Wave heights at shore:
Tsunami Green Function



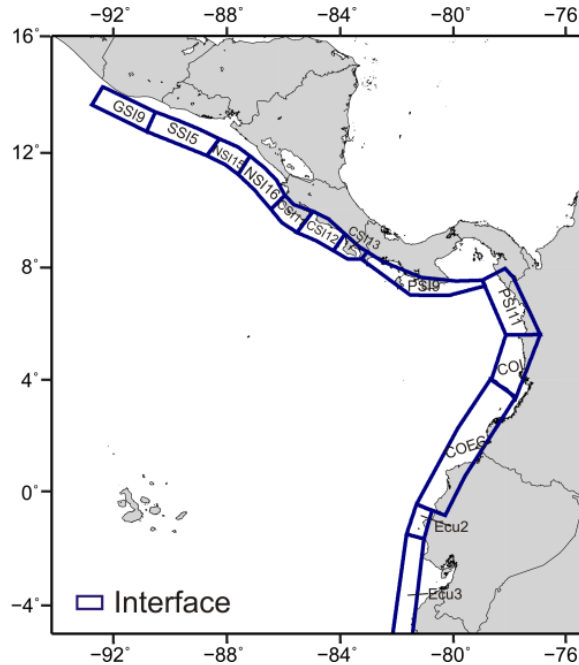
Hazard curves only Zone 1

Seismic source zones in Central America

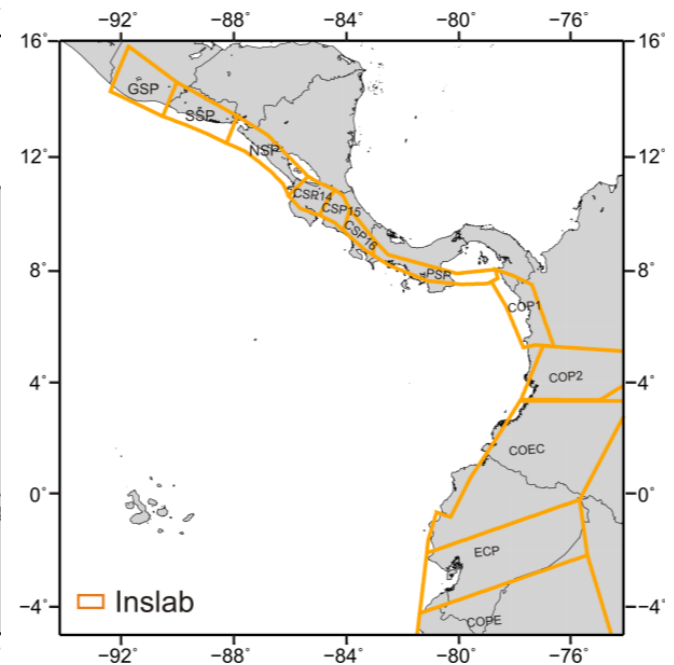
1. Outer rise and crustal upper plate



2. Subduction plate interface



3. Intra-slab



Based on seismic catalog: CAT2011

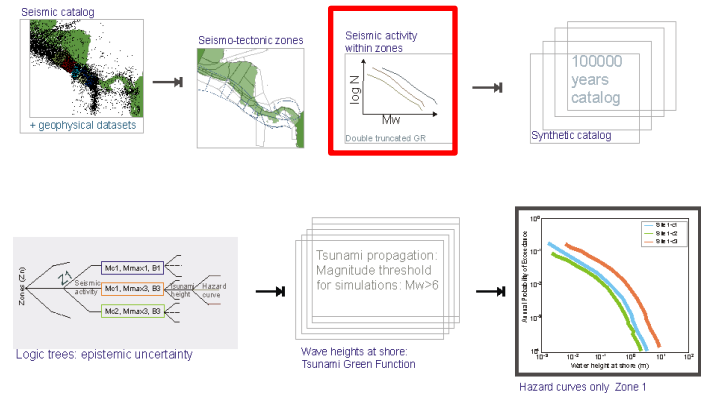
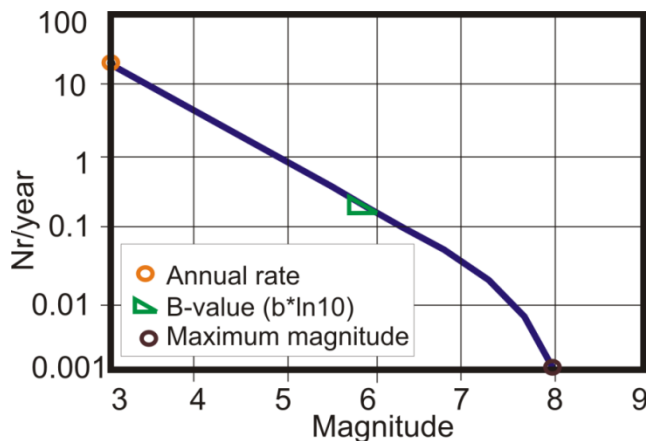
Deriving parameters for Monte-Carlo simulations

Gutenberg-Richter type magnitude–frequency relation:
 $\log N = a - bM$

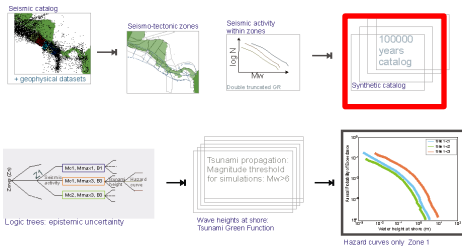
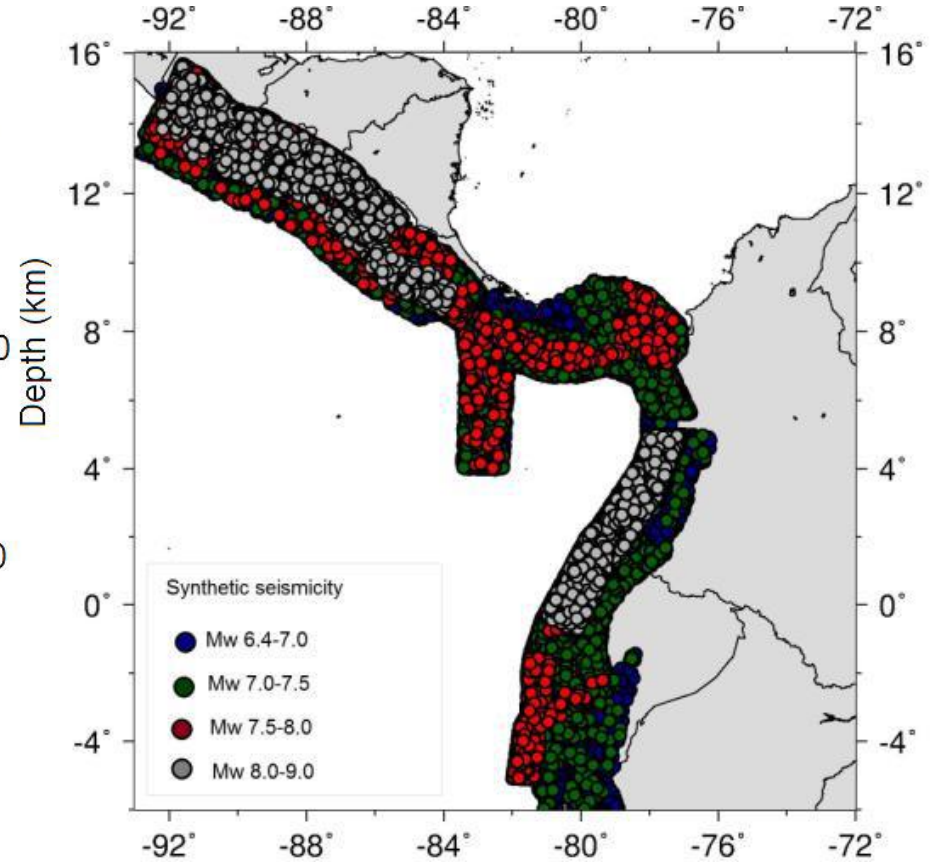
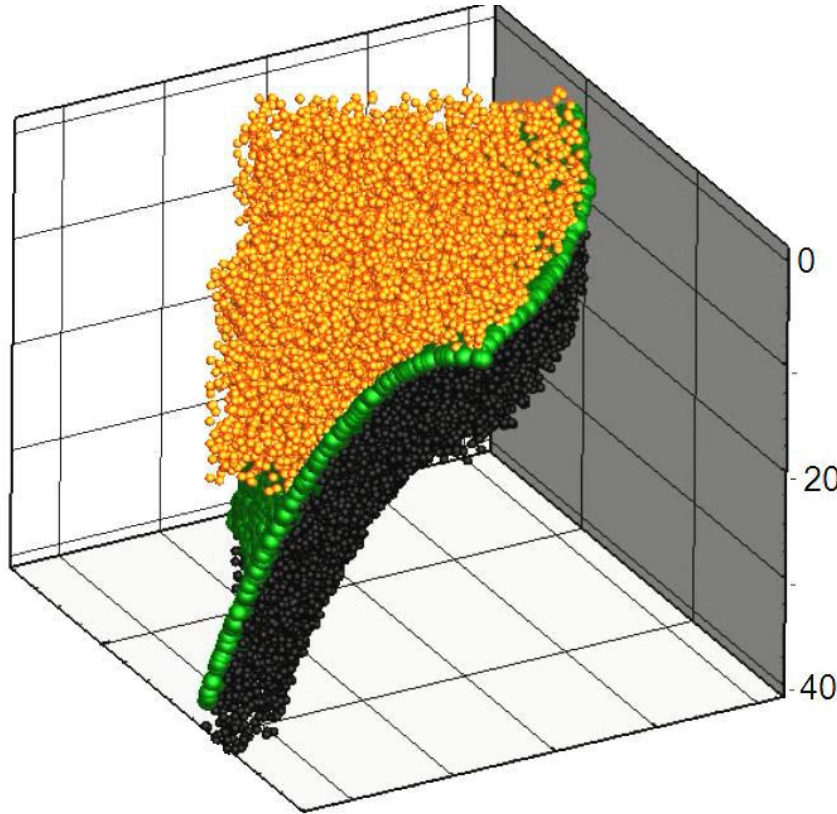
$$P[E > M_i] = \frac{e^{-\beta(M_i)} - e^{-\beta(M_{max})}}{e^{-\beta(M_{min})} - e^{-\beta(M_{max})}}$$

M_c : magnitude of completeness of seismic catalogue
 $\beta = b \cdot \ln 10$

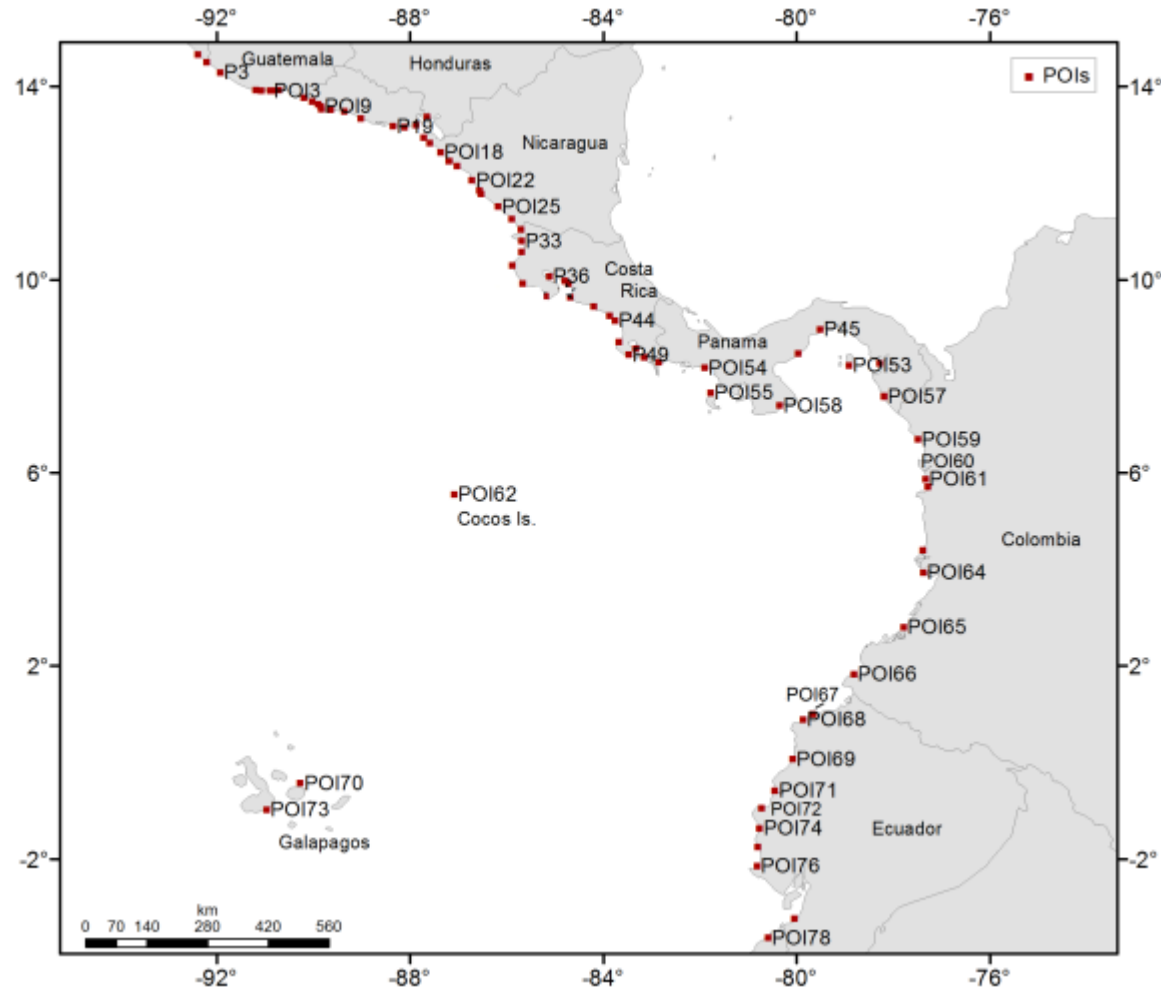
<p><i>CRN1</i> <i>b: 0.77 +/- 0.03</i> <i>a: 5.6</i> <i>Mc: 3.7 +/- 0.05</i></p>	<p><i>NIC1</i> <i>b: 1.3 +/- 0.03</i> <i>a: 6.73</i> <i>Mc: 4.6 +/- 0.01</i></p>
<p><i>CRC2</i> <i>b: 1.01 +/- 0.03</i> <i>a: 6.73</i> <i>Mc: 3.6 +/- 0.02</i></p>	<p><i>CRC3</i> <i>b: 1.01 +/- 0.03</i> <i>a: 5.82</i> <i>Mc: 3.7 +/- 0.06</i></p>



Synthetic catalog for 100 000 years



Selecting Points Of Interest (POI)

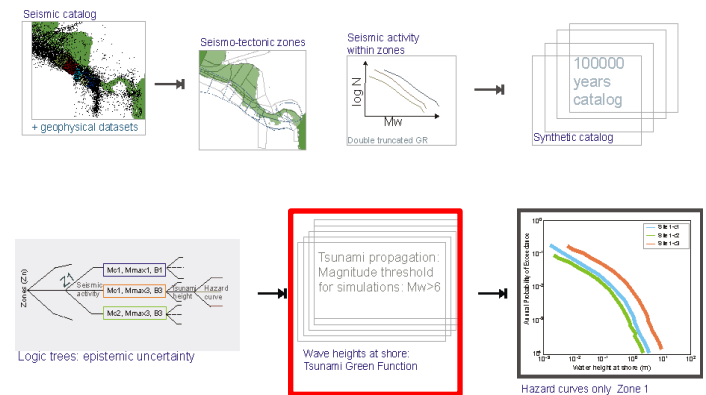


Computing wave heights at POIs for all the sources

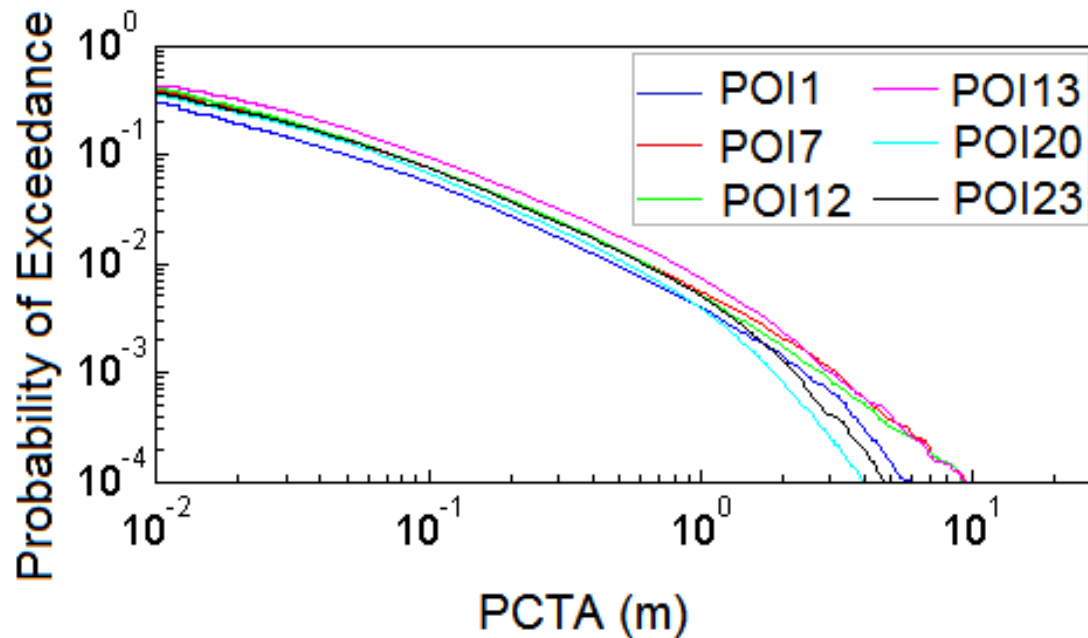
Extensive computational task: Hundreds of thousands of scenarios

Different approaches:

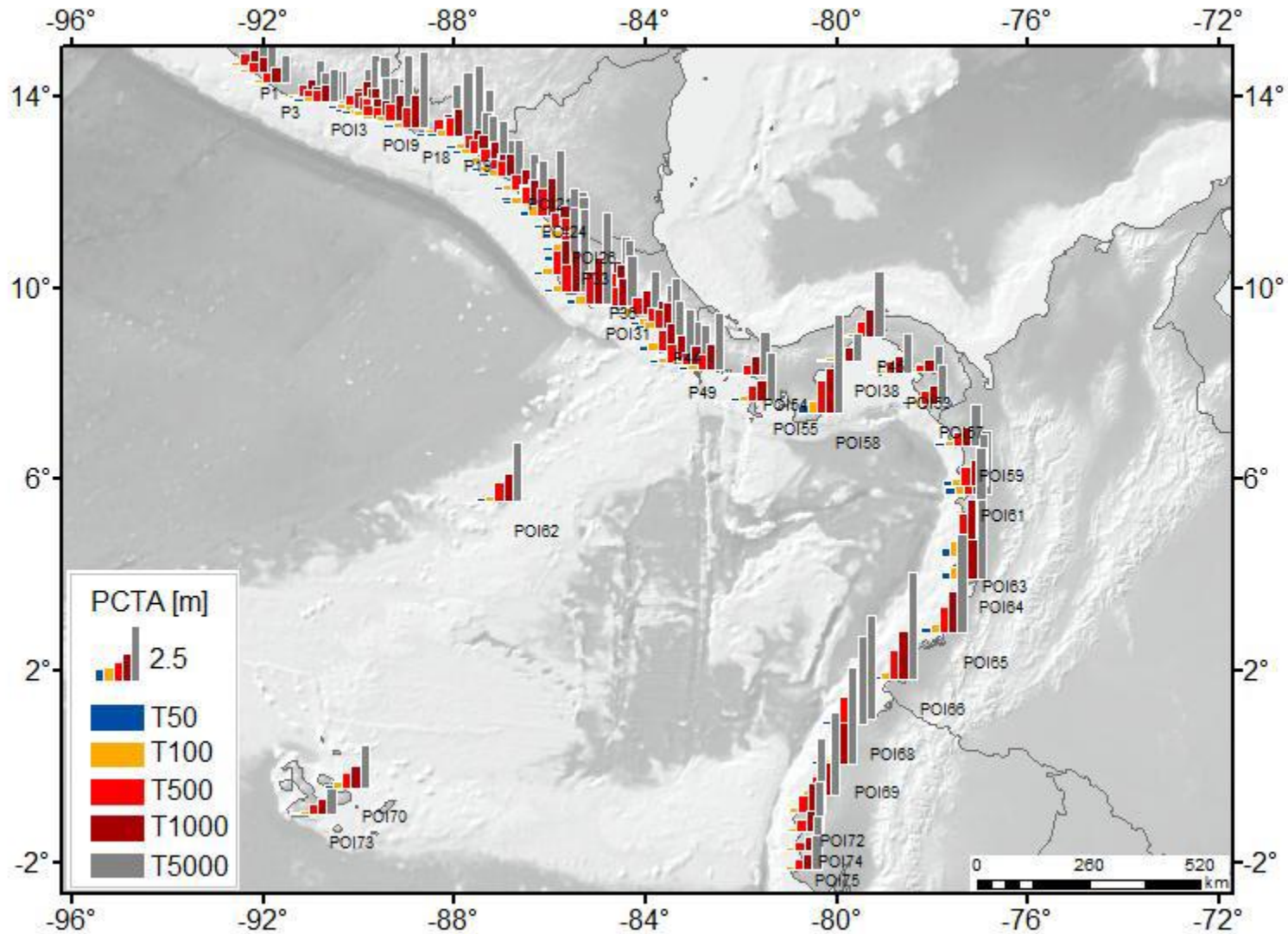
- Using pre-computed linear Green's Functions
- Direct computations of offshore amplitudes with fast (linear) numerical algorithms



Hazard results: hazard curves @ selected POIs



Wave heights expected @ different return periods



Wave heights expected @ different return periods: Another view

