

ASPECT

Introduction – Tutorial – Applications

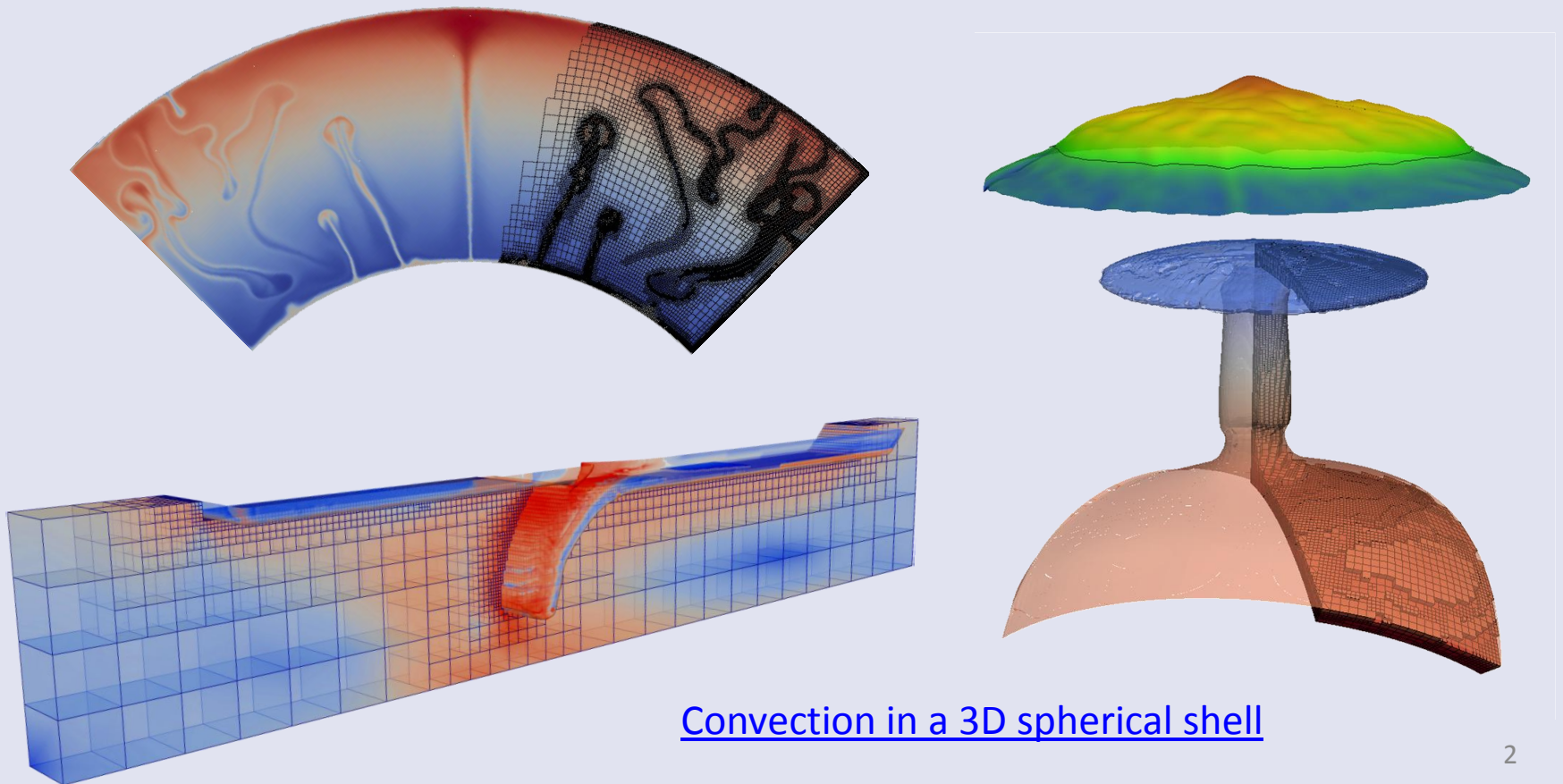
Blockkurs Fortgeschrittene Geodynamik
08.03.2016

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What is Aspect?

ASPECT

- Advanced Solver for Problems in Earth's Convection -



- Some widely used codes
- Almost no codes use adaptively refined meshes
- Almost all codes use lower order elements
- Most codes use “simple” solvers
- No code has been “designed” with a view to
 - extensibility
 - maintainability
 - correctness

Requirements as “community code”:

- solve problems of interest (to geodynamicists)
- well tested
- modern numerical methods
- easy to extend
- freely available = open code

- Mesh adaptation
- Accurate discretizations (choice of finite element for velocity and pressure + nonlinear artificial diffusion for temperature stabilization)
- Efficient linear solvers (preconditioner + algebraic multigrid)
- Parallelization of all the steps above
- Modularity of the code

Credits

Website and manual:

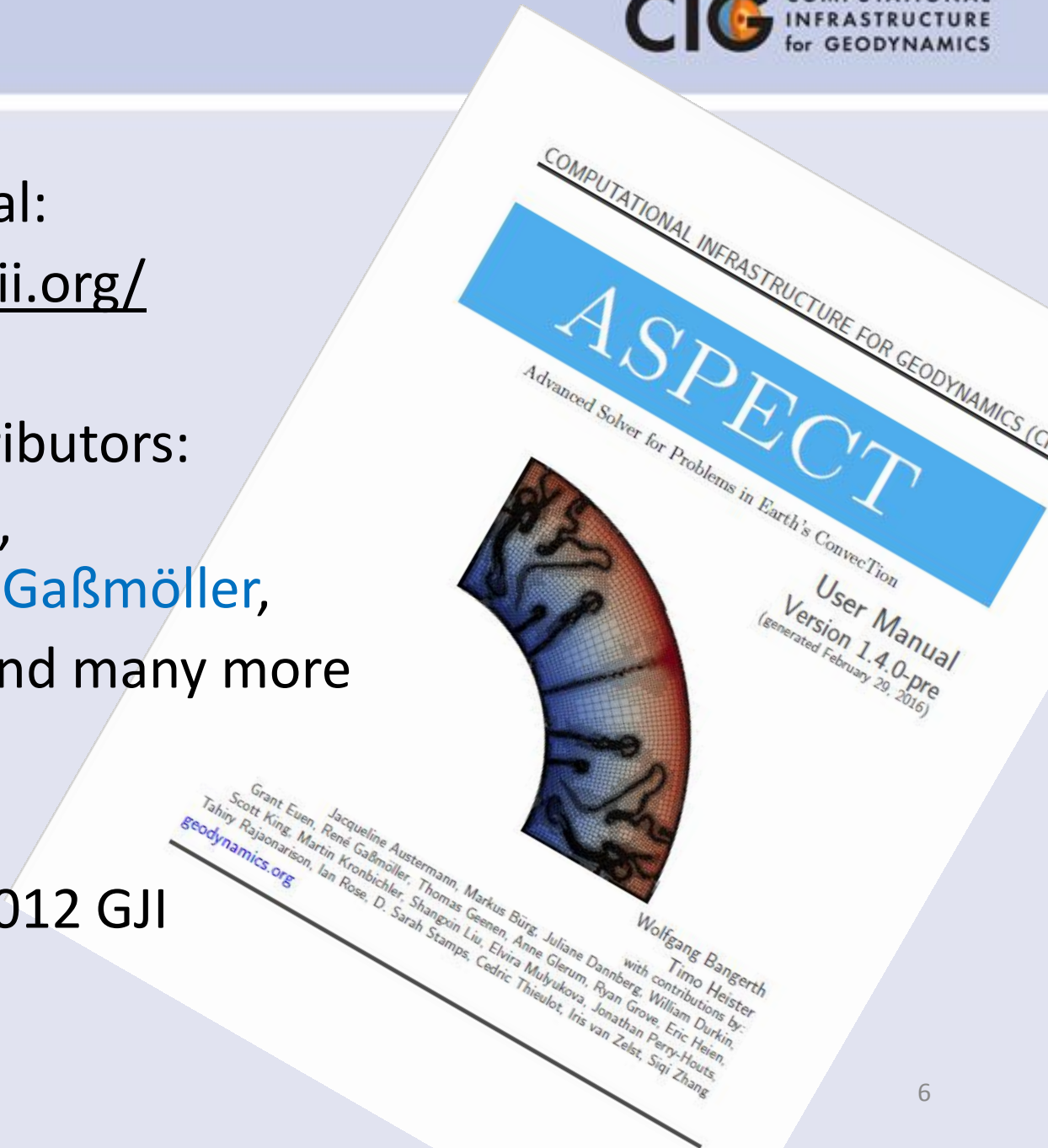
<https://aspect.dealii.org/>

Developers & contributors:

Wolfgang Bangerth,
Timo Heister, René Gaßmöller,
Juliane Dannberg and many more

Publication:

Kronbichler et al. 2012 GJI



- Model key components:
 1. The rules (e.g. equations) for the model
 2. The discretization of the model
 3. Model parameters
 4. Dependent and independent variables
 5. The initial state of the model
 6. The boundary conditions
- Look at the parameter file:
*cd ASPECT_TUTORIAL/models/
gedit tutorial.prm*

- General parameters:

Internal calculations use
seconds, but output in years

2D problem

3	set Dimension	= 2
8	set Use years in output instead of seconds	= true
9	set End time	= 5e10
10	set Output directory	= output

Simulation output will be stored
in the directory named “output”

= 5×10^{10} years
= 50 billion years

Equations

$$-\nabla \cdot \left[2\eta \left(\varepsilon(\mathbf{u}) - \frac{1}{3}(\nabla \cdot \mathbf{u})\mathbf{1} \right) \right] + \nabla p = \rho \mathbf{g}$$

Momentum equation

Divergence of
stress tensor

Only viscous stress
(no
elasticity/plasticity), no
inertia

Pressure
gradient

(Total pressure instead of
only dynamic pressure)

Gravity
force

\mathbf{u}	velocity	$\frac{m}{s}$
p	pressure	Pa
T	temperature	K
$\varepsilon(\mathbf{u})$	strain rate	$\frac{1}{s}$
η	viscosity	Pa · s

ρ	density	$\frac{kg}{m^3}$
\mathbf{g}	gravity	$\frac{m}{s^2}$
C_p	specific heat capacity	$\frac{J}{kg \cdot K}$
k	thermal conductivity	$\frac{W}{m \cdot K}$
H	intrinsic specific heat production	$\frac{W}{kg}$

Equations

$$-\nabla \cdot \left[2\eta \left(\varepsilon(\mathbf{u}) - \frac{1}{3}(\nabla \cdot \mathbf{u})\mathbf{1} \right) \right] + \nabla p = \rho \mathbf{g}$$

Momentum equation

$$\nabla \cdot (\rho \mathbf{u}) = 0$$

Conservation of mass

Includes compressibility

$$\frac{D\rho}{Dt} + \rho \cdot \text{div } \vec{v} = 0$$

(with the assumption $\frac{\partial \rho}{\partial t} = 0$)

Mass change in a given volume

In- / outflux of mass

\mathbf{u}	velocity	$\frac{m}{s}$
p	pressure	Pa
T	temperature	K
$\varepsilon(\mathbf{u})$	strain rate	$\frac{1}{s}$
η	viscosity	Pa · s

ρ	density	$\frac{kg}{m^3}$
\mathbf{g}	gravity	$\frac{m}{s^2}$
C_p	specific heat capacity	$\frac{J}{kg \cdot K}$
k	thermal conductivity	$\frac{W}{m \cdot K}$
H	intrinsic specific heat production	$\frac{W}{kg}$

Equations

$$-\nabla \cdot \left[2\eta \left(\varepsilon(\mathbf{u}) - \frac{1}{3}(\nabla \cdot \mathbf{u})\mathbf{1} \right) \right] + \nabla p = \rho \mathbf{g}$$

Momentum equation

$$\nabla \cdot (\rho \mathbf{u}) = 0$$

Conservation of mass

$$\rho C_p \left(\frac{\partial T}{\partial t} + \mathbf{u} \cdot \nabla T \right) - \nabla \cdot k \nabla T = \rho H$$

Conservation of energy

Change of
energy over
time

Advection

Heat
conduction

Radiogenic heating

$$+ 2\eta \left(\varepsilon(\mathbf{u}) - \frac{1}{3}(\nabla \cdot \mathbf{u})\mathbf{1} \right) : \left(\varepsilon(\mathbf{u}) - \frac{1}{3}(\nabla \cdot \mathbf{u})\mathbf{1} \right)$$

Shear heating

$$- \frac{\partial \rho}{\partial T} T \mathbf{u} \cdot \mathbf{g}$$

Adiabatic heating $\frac{\partial \rho}{\partial T} = -\rho \alpha$

$$+ \rho T \cdot \Delta S \frac{DX}{Dt}$$

latent heat (phase changes)

Equations

$$-\nabla \cdot \left[2\eta \left(\varepsilon(\mathbf{u}) - \frac{1}{3}(\nabla \cdot \mathbf{u})\mathbf{1} \right) \right] + \nabla p = \rho \mathbf{g}$$

Momentum equation

$$\nabla \cdot (\rho \mathbf{u}) = 0$$

Conservation of mass

$$\rho C_p \left(\frac{\partial T}{\partial t} + \mathbf{u} \cdot \nabla T \right) - \nabla \cdot k \nabla T = \rho H$$

Conservation of energy

$$+ 2\eta \left(\varepsilon(\mathbf{u}) - \frac{1}{3}(\nabla \cdot \mathbf{u})\mathbf{1} \right) : \left(\varepsilon(\mathbf{u}) - \frac{1}{3}(\nabla \cdot \mathbf{u})\mathbf{1} \right)$$

$$- \frac{\partial \rho}{\partial T} T \mathbf{u} \cdot \mathbf{g} \quad + \rho T \cdot \Delta S \frac{DX}{Dt}$$

$$\frac{\partial c_i}{\partial t} + \mathbf{u} \cdot \nabla c_i = 0$$

Advection of compositional fields

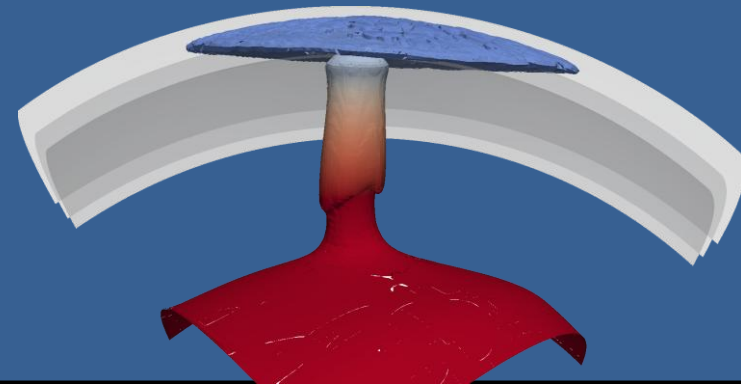
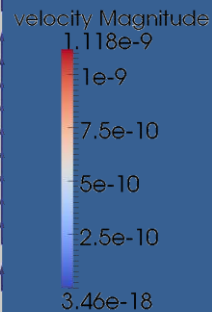
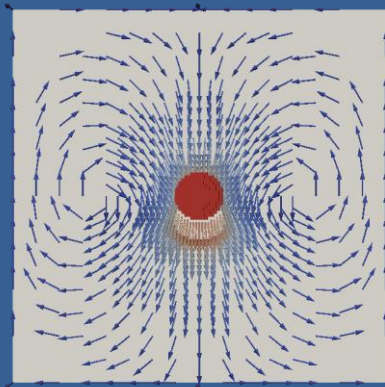
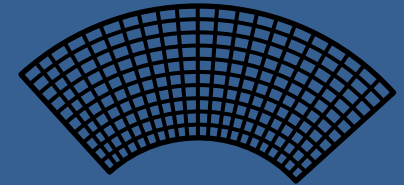
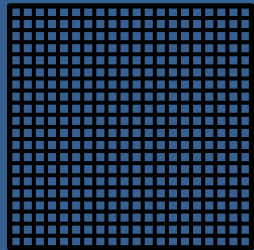
Field method (instead of tracer method)

2D or 3D?

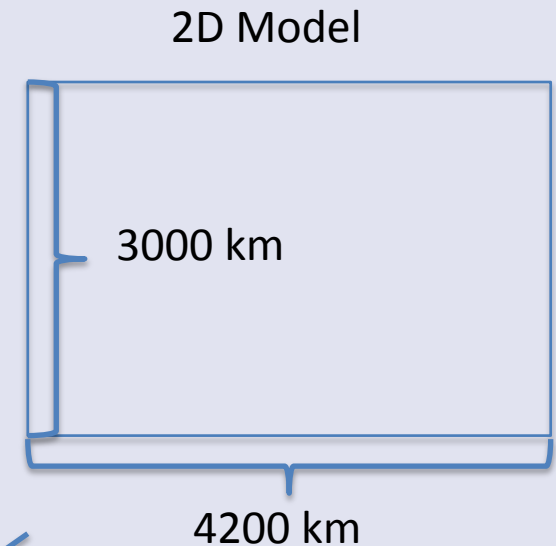
Geometry model

Box

Spherical shell

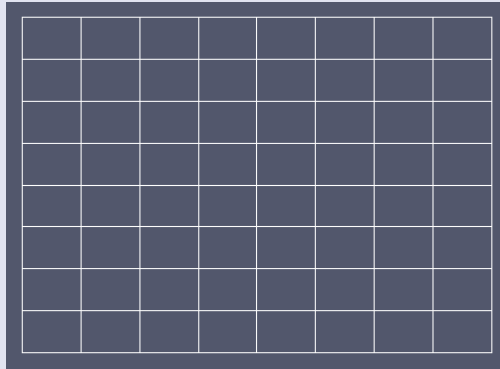


- 2D box = rectangle,
3D box = cuboid
- Depth of the box = 3×10^6 m
- Width of the box = 4.2×10^6 m
- Make sure that various units fit together!

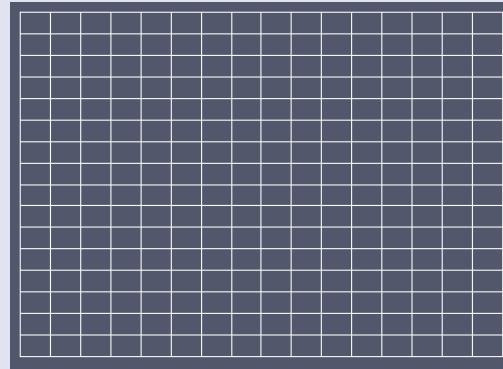


```
21 subsection Geometry model
22     set Model name = box
23     subsection Box
24         set X extent = 4.2e6
25         set Y extent = 3e6
26     end
27 end
```

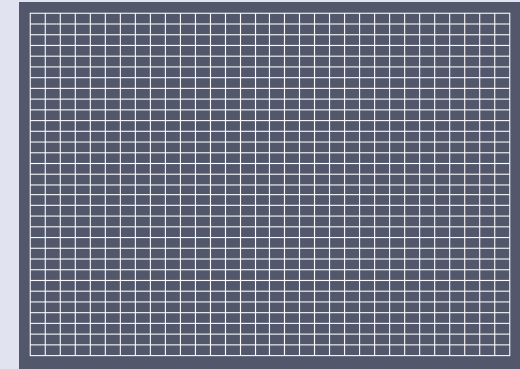
ASPECT - Discretization



REFINE=3 (8x8 cells)



REFINE=4 (16x16 cells)



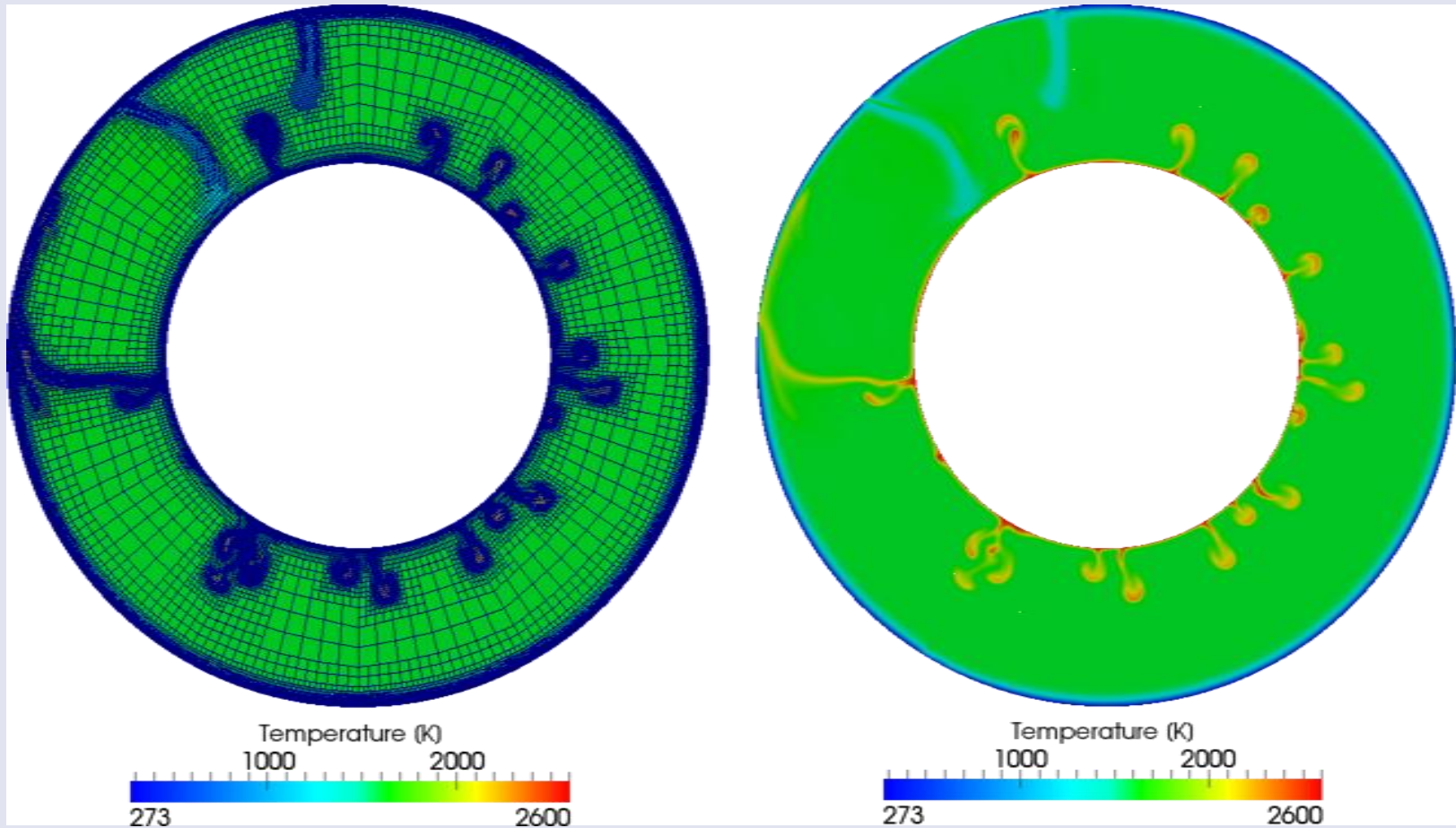
REFINE=5 (32x32 cells)

```
34 subsection Mesh refinement
35     set Initial global refinement = REFINE
36     set Initial adaptive refinement = 0
37     set Time steps between mesh refinement = 0
38 end
```

“grid spacing” of the mesh, for this tutorial:
REFINE = 3 or 4 or 5

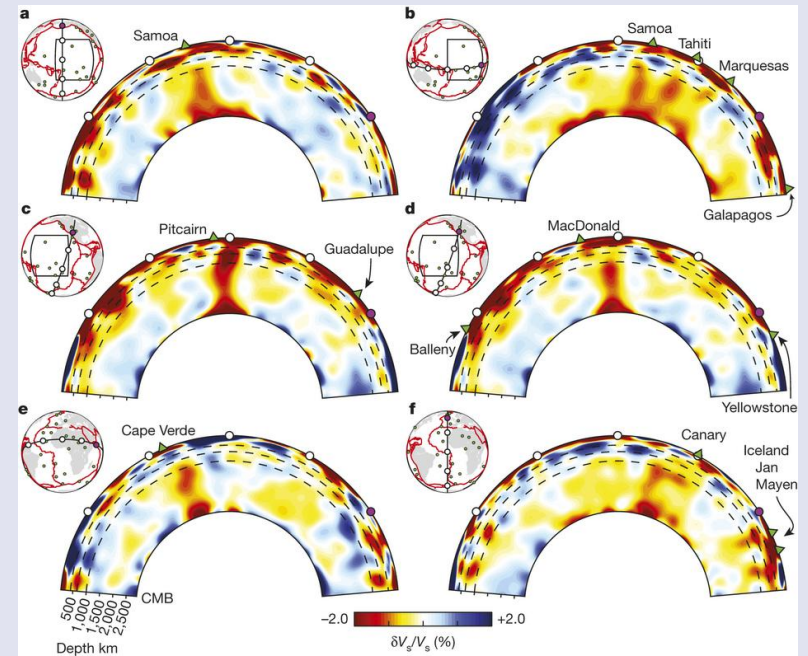
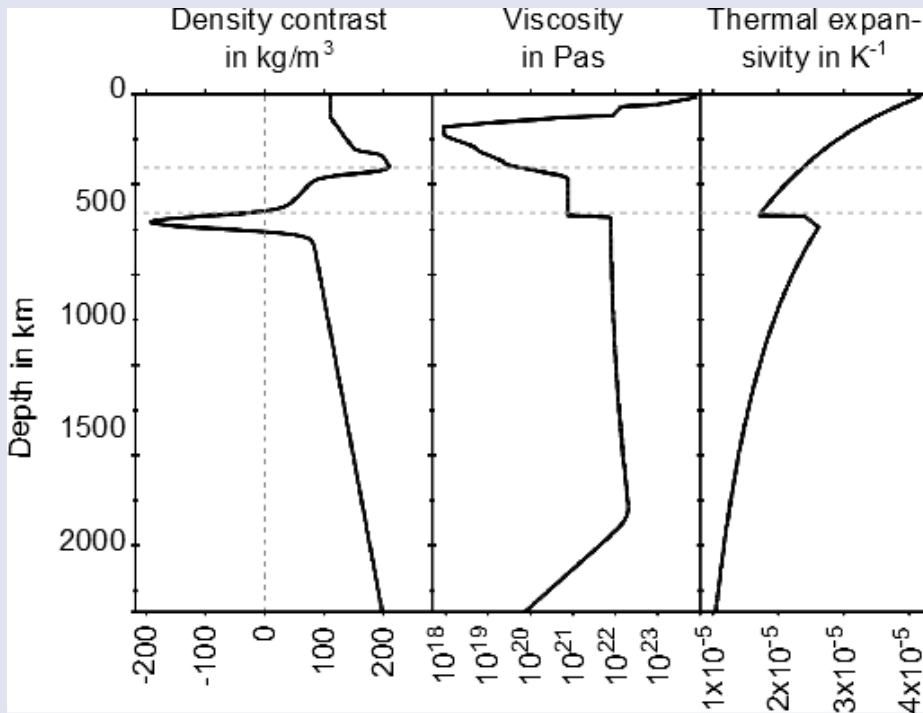
turned off → the mesh does not change during the simulation

Mesh adaptation



Material model

Input:
Temperature, pressure, composition, strain rate, position



Densities for example from seismic tomography velocities

- Use a built in material model or implement your own
- Several parameters which control reference density, temperature dependence of viscosity, etc.

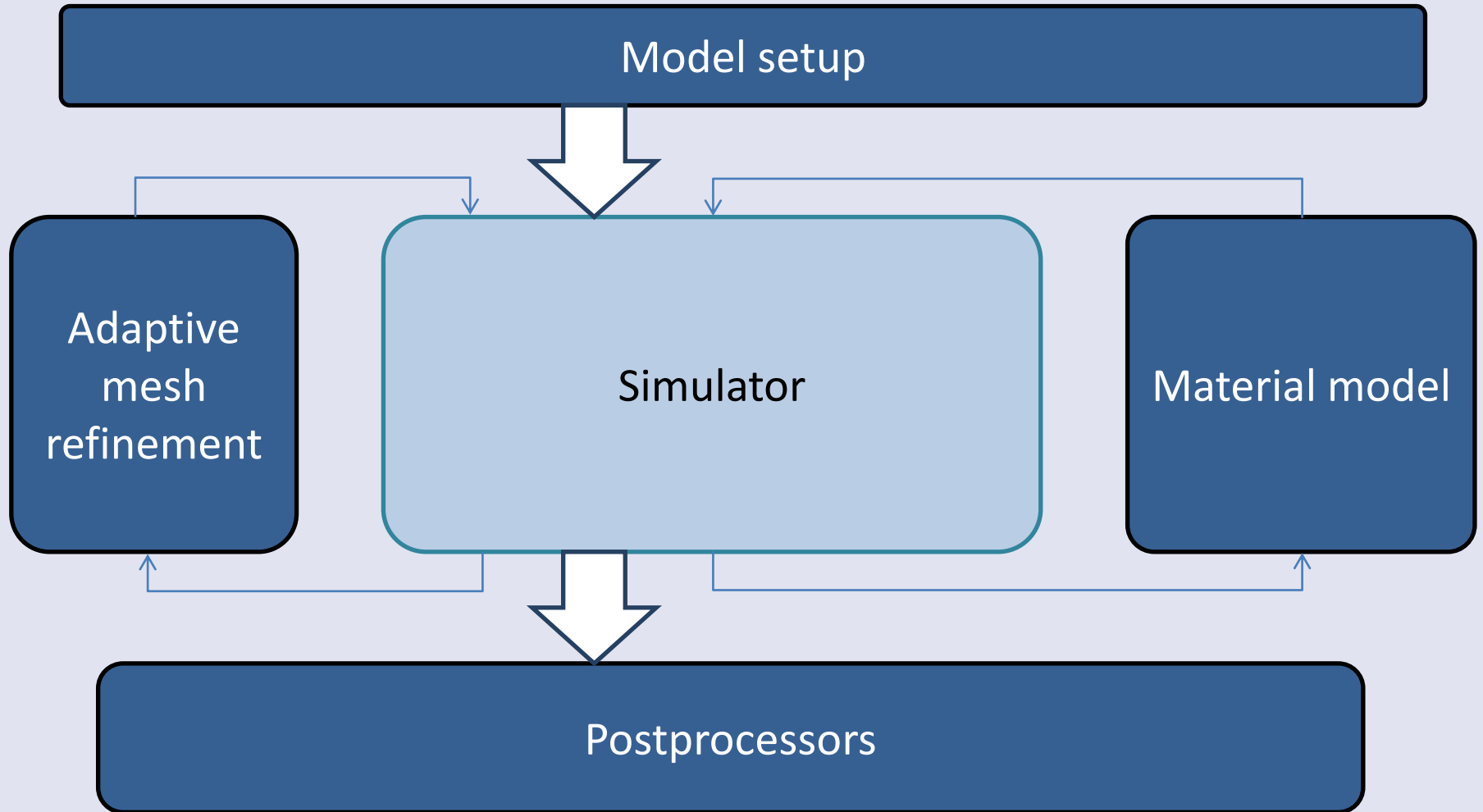
Default Values:

$$\rho_0 = 3300, g = 9.8, \alpha = 2 \times 10^{-5}, \Delta T = (3600 - 273) = 3327$$

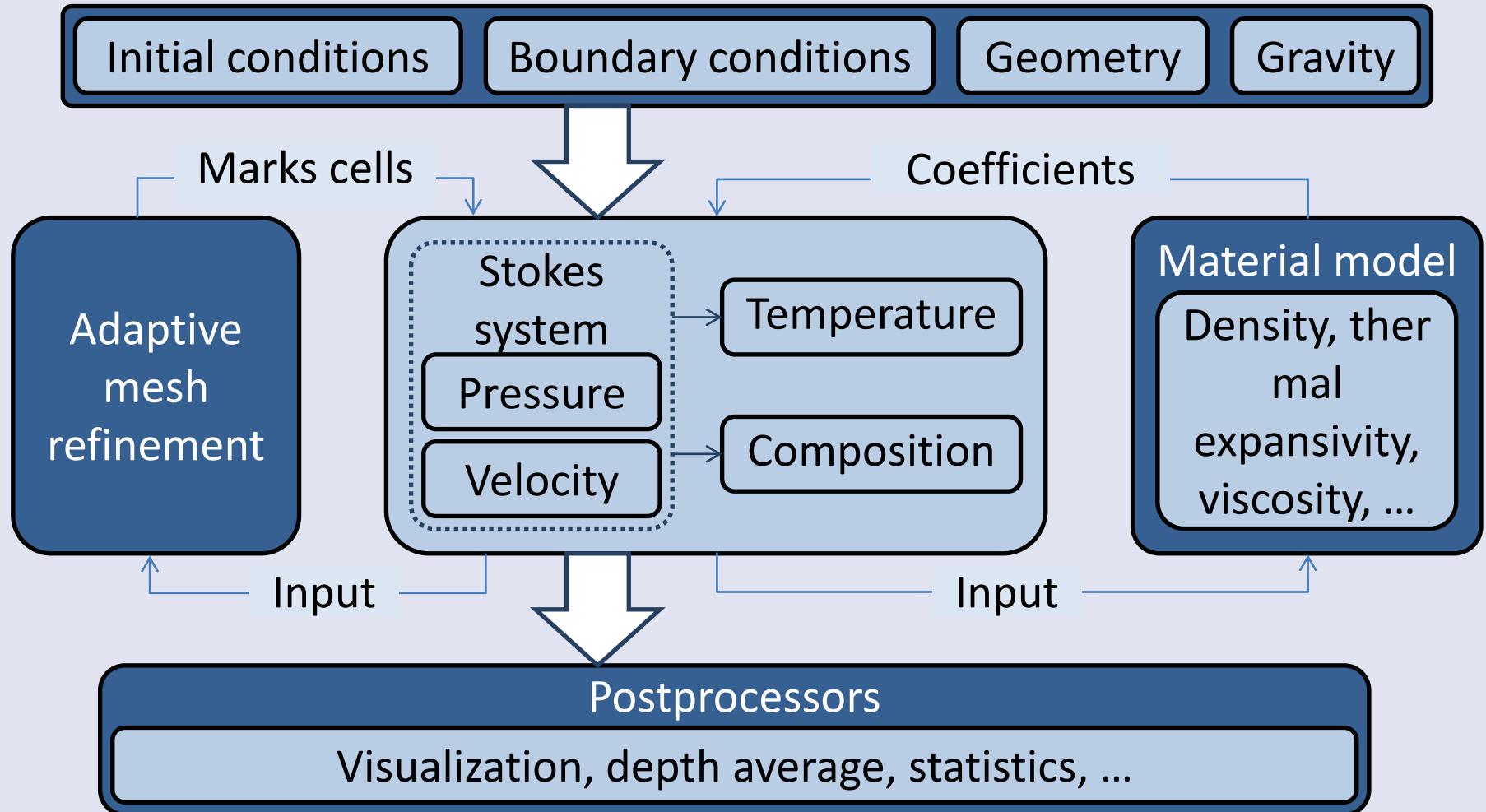
$$D = 3 \times 10^6, k = 4.7, c_p = 1250, \kappa = \frac{k}{\rho_0 c_p} = 1.1394 \times 10^{-6}$$

44	subsection Gravity model	51	subsection Material model
45	set Model name = vertical	52	set Model name = simple
46	subsection Vertical	53	subsection Simple model
47	set Magnitude = 9.8	54	set Viscosity = VISCOSITY
48	end	55	end
49	end	56	end

Modularity

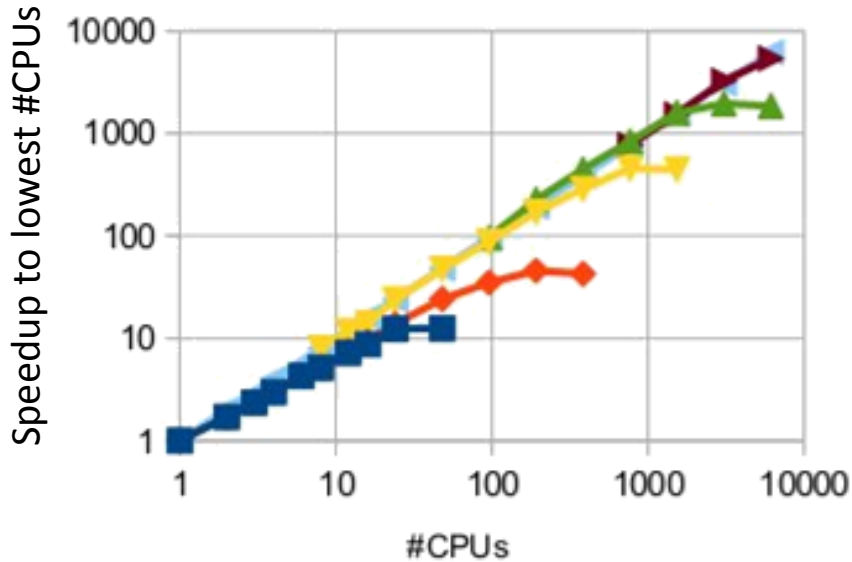


Modularity

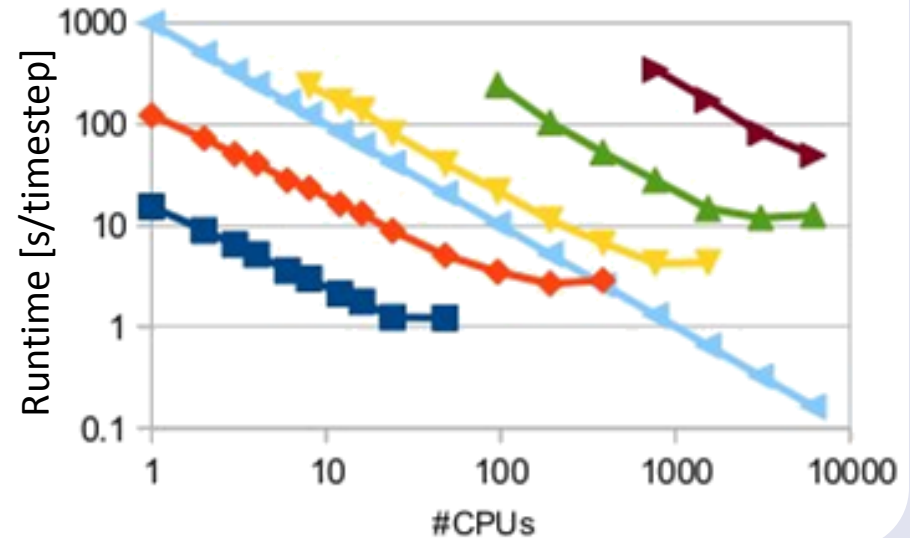


Scaling

Speedup to maximal #DOFs/CPU



Strong Scaling



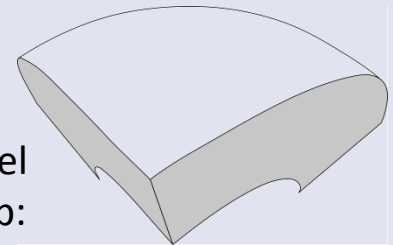
#DOFs

- 8.5e4
- ◆ 6.4e5
- ▲ 5.0e6
- ▲ 3.9e7
- ▲ 3.1e8
- ▲ Optimal

Resolution in km

- 360
- ◆ 180
- ▲ 90
- ▲ 45
- ▲ 22
- ▲ Optimal

Model Setup:



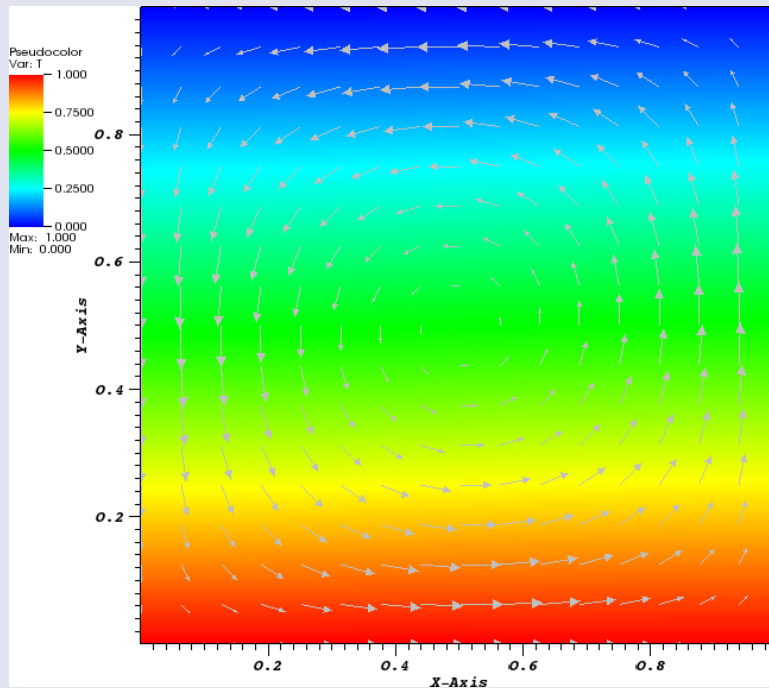
Scales almost linearly = excellent parallelization!

Exercise 1

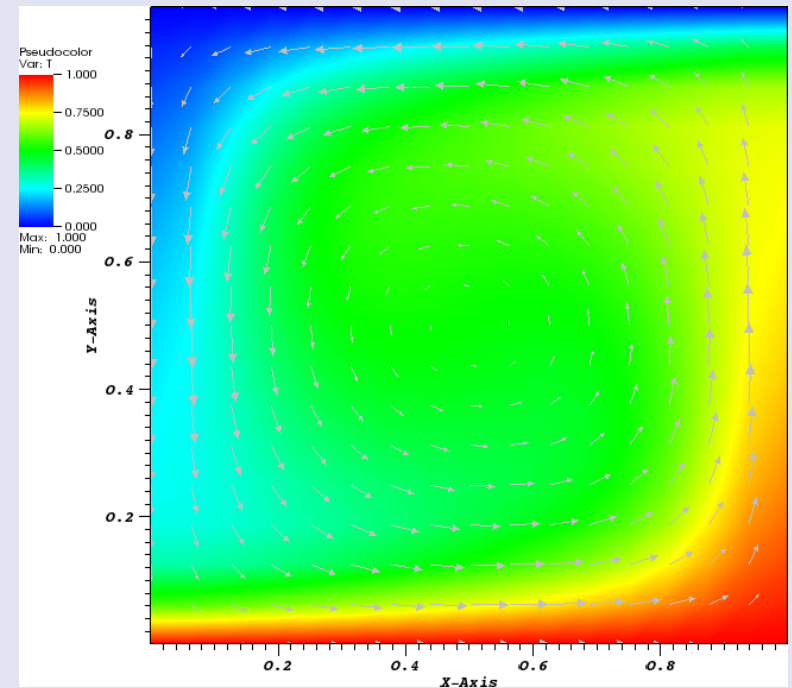
Convection in a 2D Box

Nusselt-Rayleigh Relationship &
Visualization with ParaView

Convection in a 2D Box (free slip boundaries)



Initial temperature and
velocity field



Final temperature and
velocity field

- In this tutorial, you control the

Rayleigh number Ra with the viscosity η :

$$Ra = \frac{\rho_0 g \alpha \Delta T D^3}{\eta \kappa}$$

Ra = dimensionless parameter,
indicates the presence and strength of
convection in the mantle

$$\eta = \frac{\rho_0 g \alpha \Delta T D^3}{\kappa Ra}$$

$$= \frac{5.0993 \times 10^{28}}{Ra}$$

ρ_0 = reference density

g = gravity acceleration

α = thermal expansion coefficient

T = temperature

D = depth

κ = thermal diffusivity

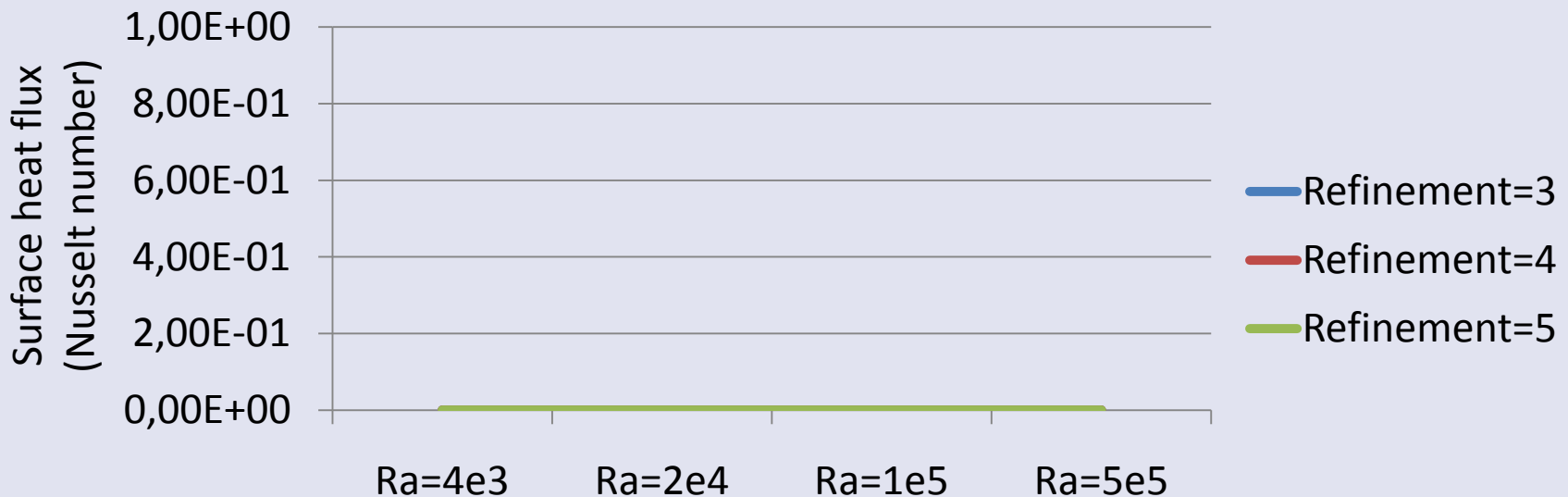
- **Nusselt number Nu** = the ratio of convective to conductive heat transfer, related to the **surface heat flux**
-

Questions

- If the Rayleigh number goes up, how does the Nusselt number change?
- How does the mesh resolution affect the accuracy of these results?

Nusselt-Rayleigh Relationship

	Ra=4,000	Ra=20,000	Ra=100,000	Ra=500,000
End Time	1e12	2e11	3e10	5e9
Viscosity	1.275E25	2.550E24	5.099E23	1.020E23
Refine = 3	(???)	(???)	(???)	(???)
Refine = 4	(???)	(???)	(???)	(???)

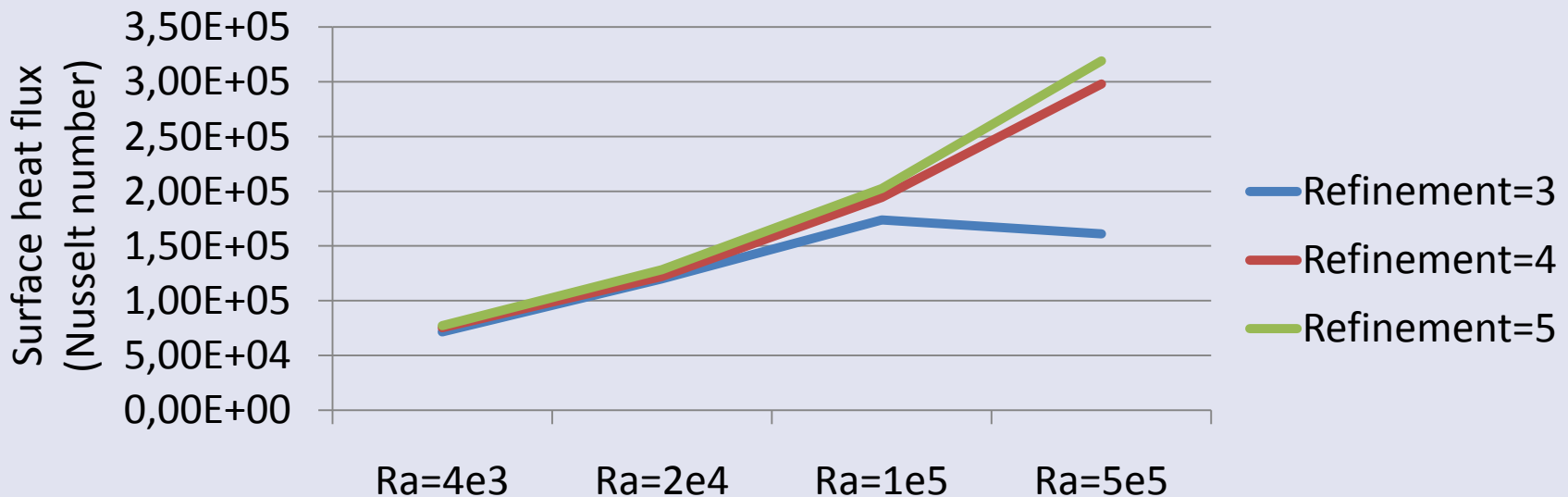


1. Modify the **refinement**, **end time**, and **Rayleigh number** in tutorial.prm
2. Run ASPECT with the tutorial parameter file
aspect tutorial.prm
3. Look at the log
gedit output/log.txt
4. Look at the statistics output
gedit output/statistics
5. Plot the results in gnuplot (time vs. heat flux)
gnuplot
plot "output/statistics" using 2:20 with lines;

Just a hint: To stop the calculations, press **Ctrl + C**

Nusselt-Rayleigh Relationship

	Ra=4,000	Ra=20,000	Ra=100,000	Ra=500,000
End Time	1e12	2e11	3e10	5e9
Viscosity	1.275E25	2.550E24	5.099E23	1.020E23
Refine = 3	7.14e4	1.20e5	1.74e5	1.61e5
Refine = 4	7.54e4	1.22e5	1.94e5	2.98e5
Refine = 5	7.72e4	1.28e5	2.02e5	3.19e5



- If the Rayleigh number goes up, how does the Nusselt number change?

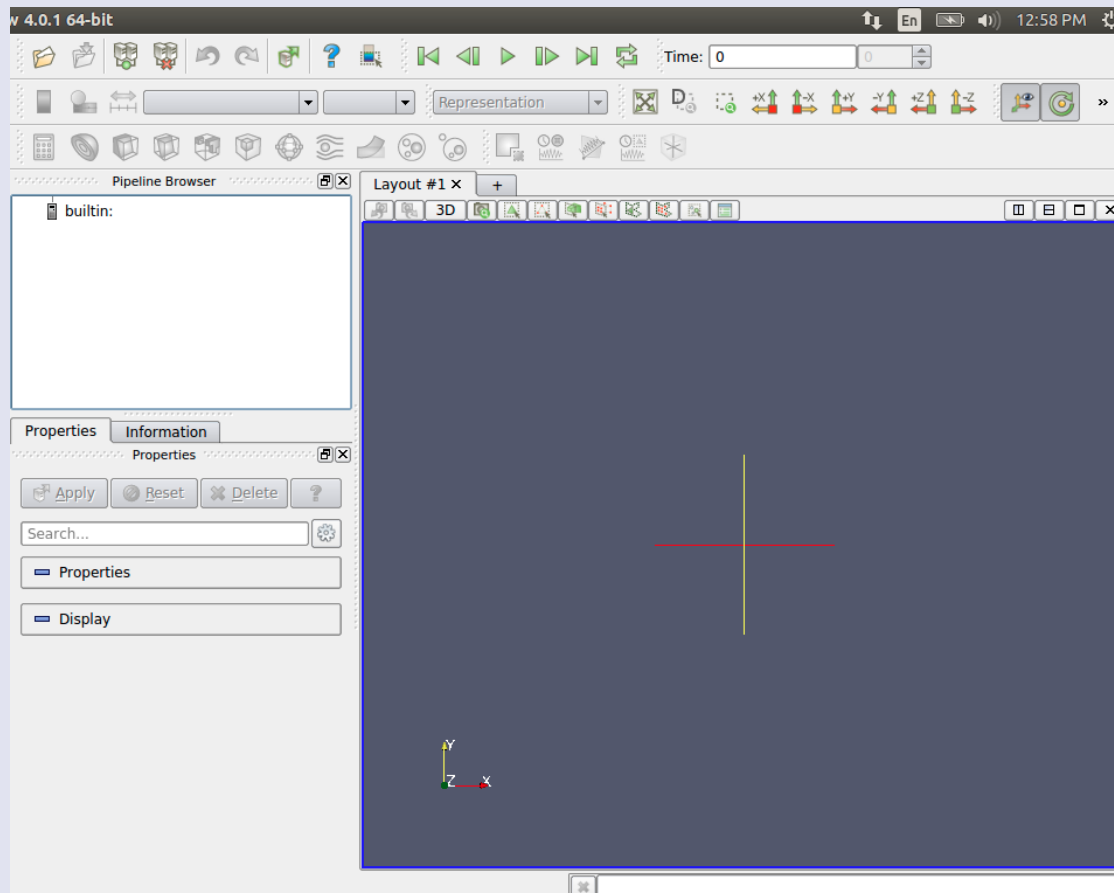
if Ra goes up \rightarrow Nu goes up

- How does the mesh resolution affect the accuracy of these results?

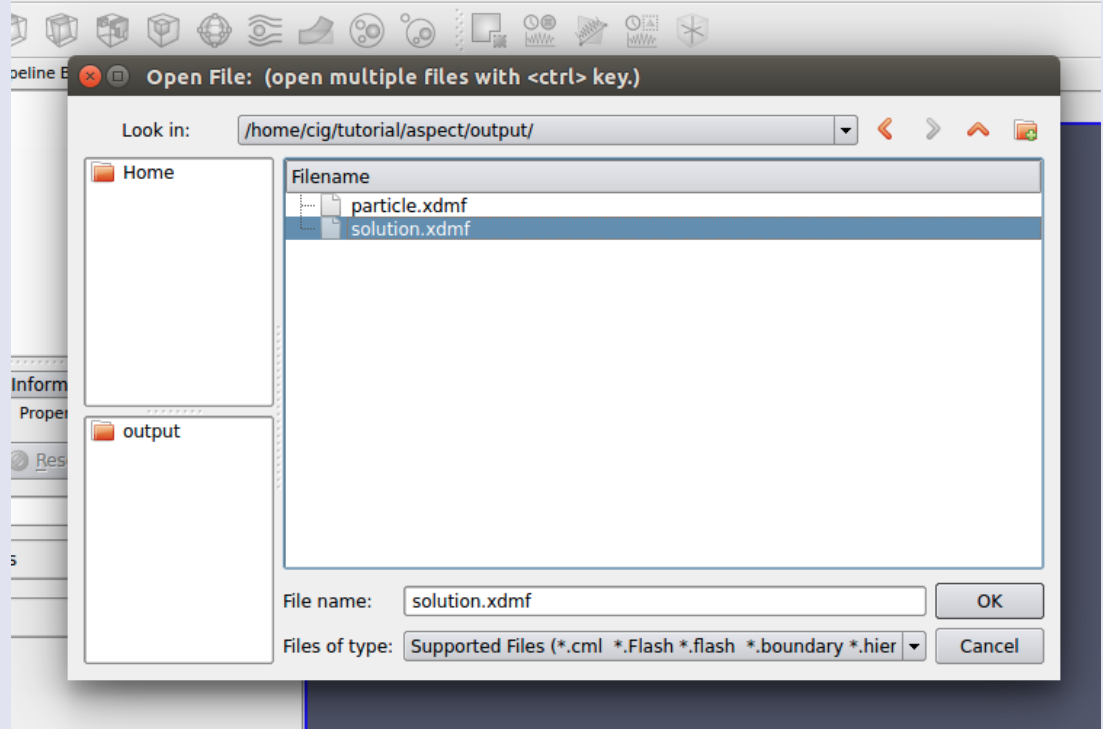
if mesh refinement is too low, the result for high Ra is no longer accurate!



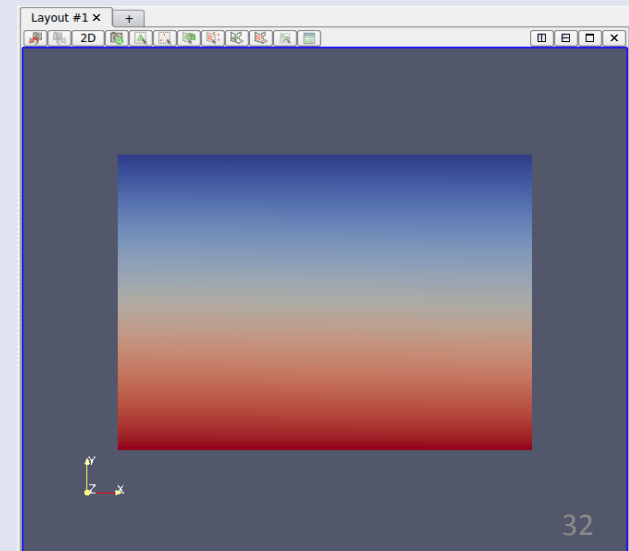
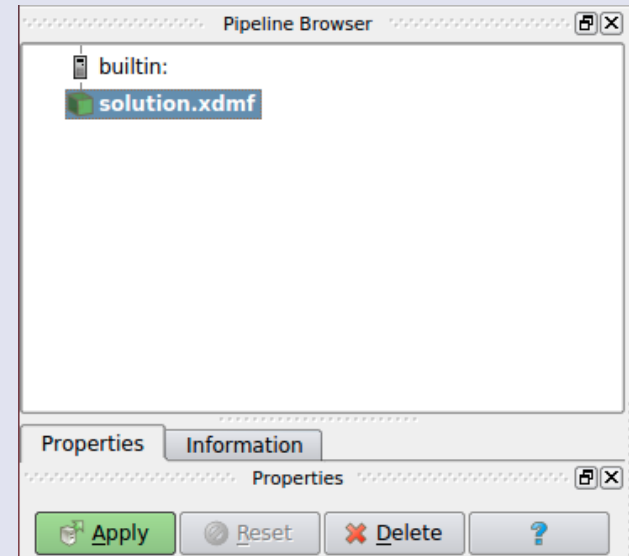
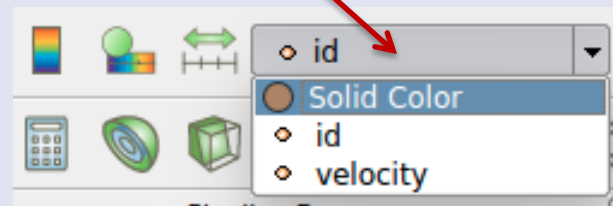
= program for visualization
of large data sets



- Aspect creates the file **solution.pvd**
- choose “Open” from the File menu
- The file is in **ASPECT_TUTORIAL/models/output/**

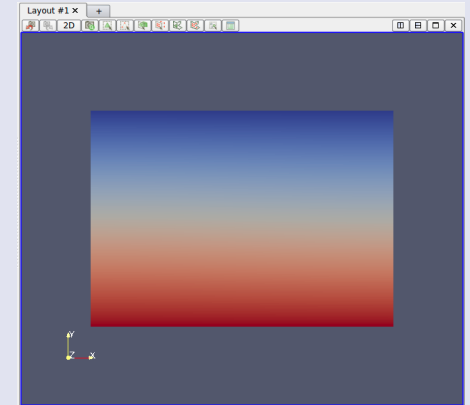


- the file contains the variables temperature (T), pressure (p), and velocity
- click “Apply” + Select “T” in the toolbar to show the temperature field



Visualization with ParaView

- change the time in the top toolbar + click “Play”

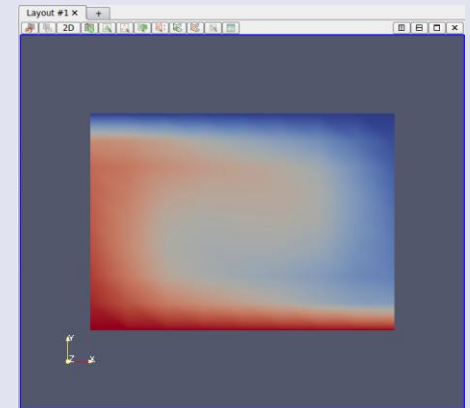


Frame 0

Previous Frame Next Frame Loop

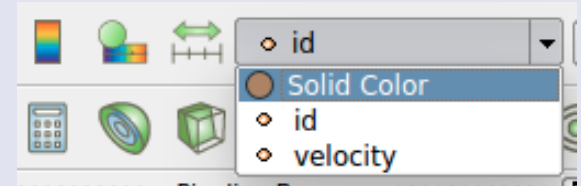
Time: 1.90612e+10 69

First Frame Play/Pause Last Frame Simulation Time Time step number

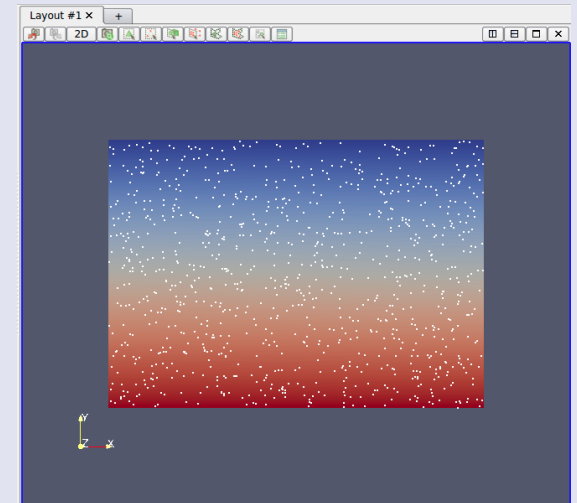


Frame 231

- Open the file **particle.pvd** and click “Apply” to see the tracer particles
- Click “play” to see how material is flowing with the tracer particles



Change the coloring scheme to “Solid Color”



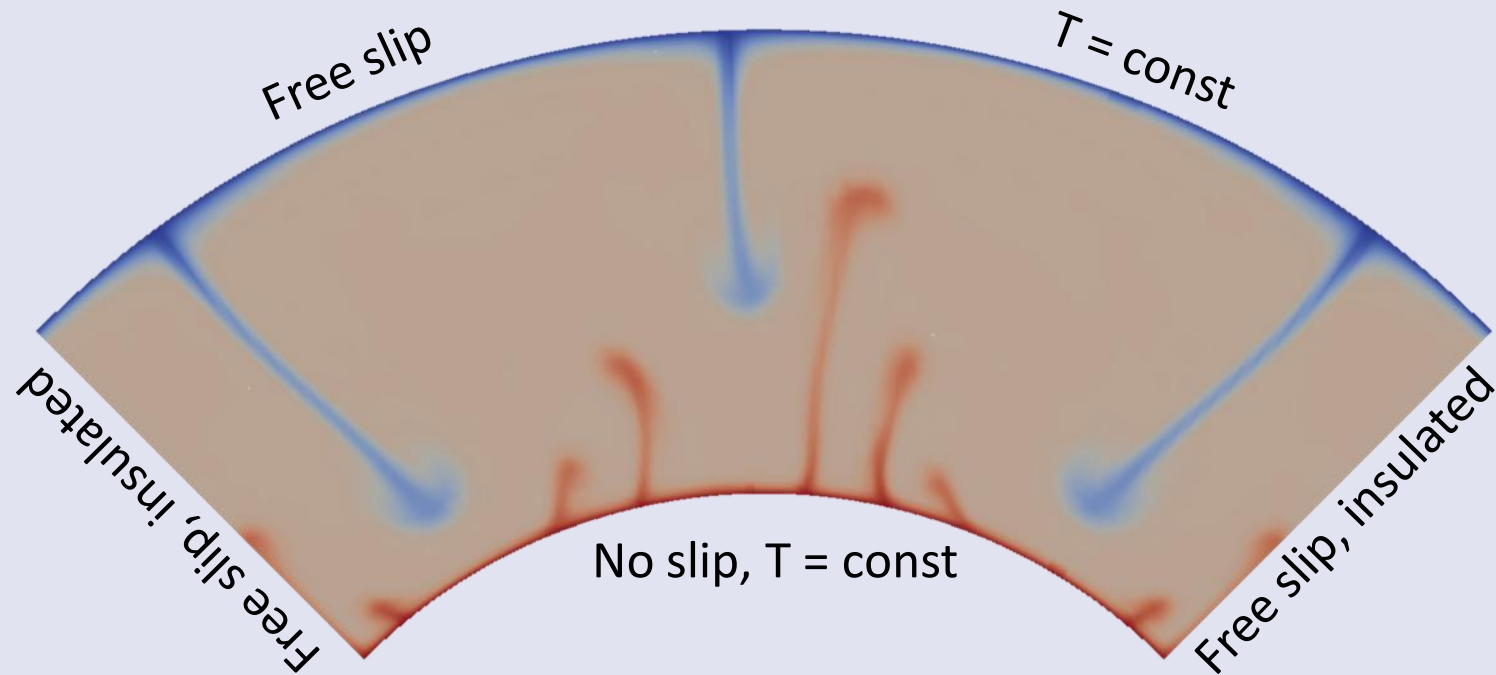
Temperature field with tracer particles

Exercise 2

Convection in a 2D spherical shell

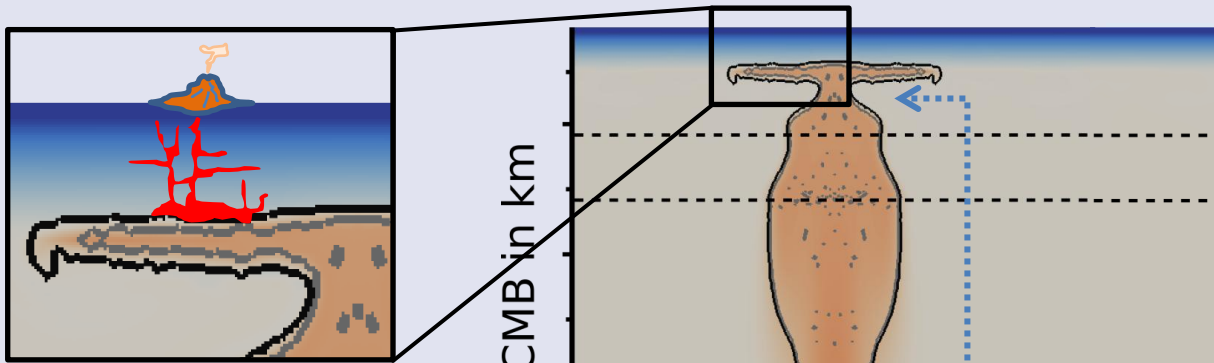
Adaptive mesh refinement &
Spherical shell geometry &
Visualization

Setup: Convection in a Shell

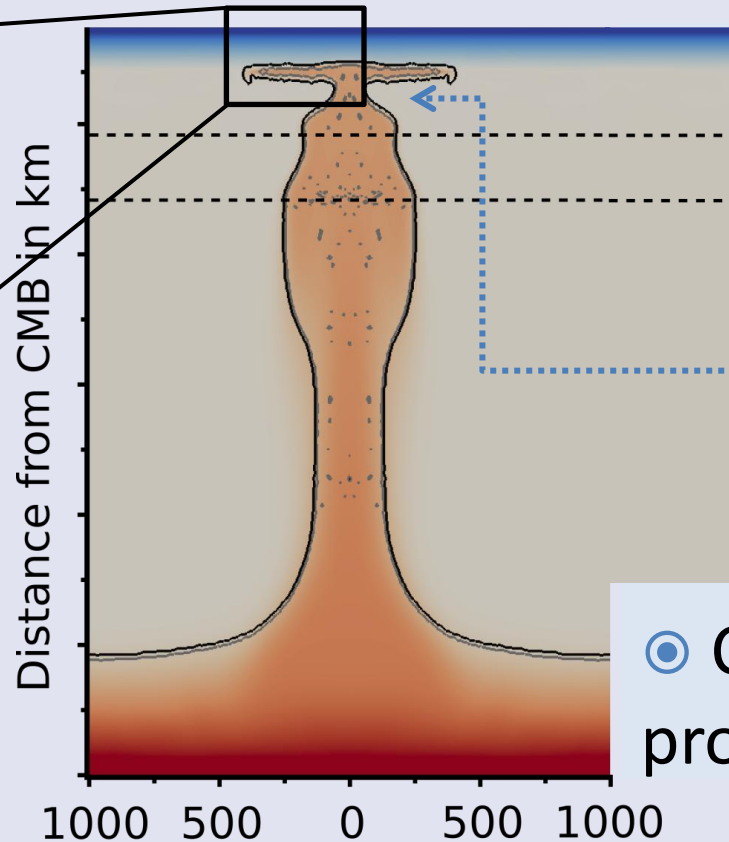
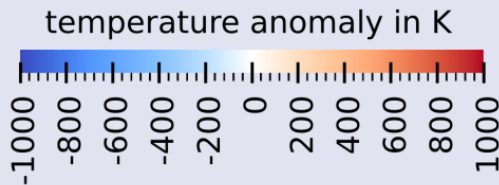


- Geometry: Quarter of a spherical shell
- Constant initial temperature with a perturbation to start the upwelling

Numerical Challenges



Different scales



⦿ High viscosity contrasts

⦿ Advection of steep thermal/compositional gradients

⦿ Complex material properties

⦿ Problems with large number of DOFs

Questions:

- How does the flow field change with varying the resolution?
- How does the runtime change with the adaptive refinement compared to global refinement?

Material model

```
set Adiabatic surface temperature = 1600

subsection Material model
  set Model name = simple
  subsection Simple model
    set Thermal expansion coefficient = 2e-5
    set Viscosity = 3e21
    set Thermal viscosity exponent = 3
    set Reference temperature = 1600
  end
end
```

These
should be
the same

Temperature-
dependent viscosity

```
subsection Geometry model
  set Model name = spherical shell

  subsection Spherical shell
    set Inner radius   = 3481000
    set Outer radius  = 6336000
    set Opening angle = 90
  end
end

subsection Gravity model
  set Model name = radial earth-like
end
```

The gravity model has to
be changed together with
the geometry

Initial conditions

```
set Adiabatic surface temperature = 1600
```

```
subsection Initial conditions  
  set Model name = adiabatic  
  
  subsection Adiabatic  
    set Amplitude = 10  
    set Radius = 500000  
  end  
end
```

This is the
temperature used
as initial condition

Boundary conditions

```
subsection Model settings
  set Zero velocity boundary indicators      = 0
  set Tangential velocity boundary indicators = 1, 2, 3

  set Prescribed velocity boundary indicators =
  set Fixed temperature boundary indicators  = 0, 1

  set Include shear heating                 = false
  set Include adiabatic heating             = false
end
```

Exactly the same as:

```
subsection Model settings
  set Zero velocity boundary indicators      = inner
  set Tangential velocity boundary indicators =
outer, left, right
  set Prescribed velocity boundary indicators =
  set Fixed temperature boundary indicators  = inner, outer

  set Include shear heating                 = false
  set Include adiabatic heating             = false
end
```

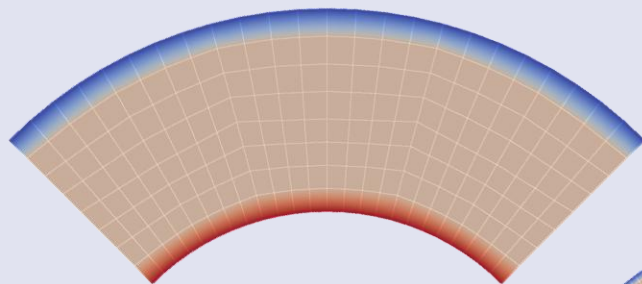
Mesh refinement

This is what needs to be changed:
Group 1: 3, Group 2: 4, Group 3: 5

```
subsection Mesh refinement
```

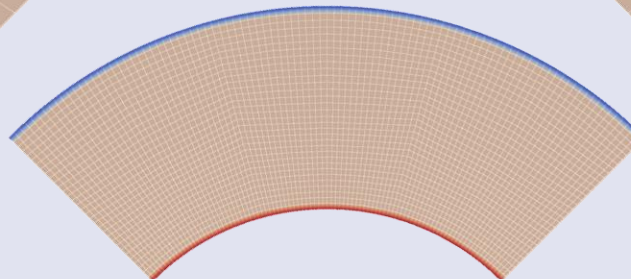
```
set Initial global refinement = 5  
set Initial adaptive refinement = 0  
set Strategy = temperature  
set Time steps between mesh refinement = 0  
set Coarsening fraction = 0.05  
set Refinement fraction = 0.3
```

```
end
```

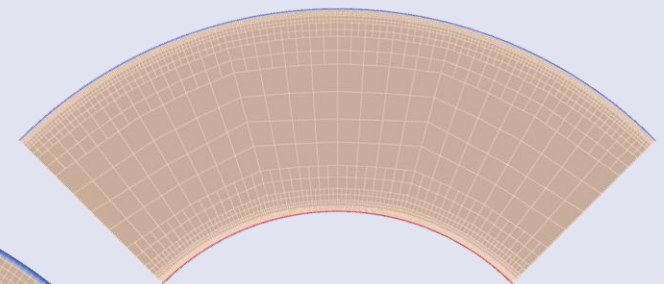


Global
refinement = 3

Global
refinement = 5



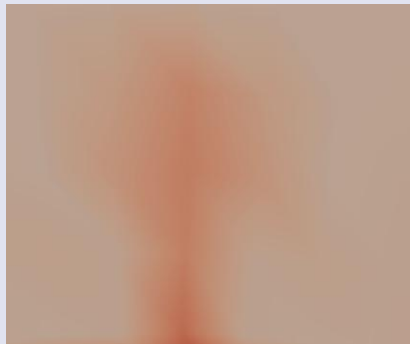
Global refinement = 4
Adaptive refinement = 2



1. Modify the `spherical_shell.prm` file to use your assigned refinement number
`gedit spherical_shell.prm`
2. Run the simulation
`aspect spherical_shell.prm` or in parallel
`mpirun -np 2 aspect spherical_shell.prm`
3. Visualize the results with Paraview
`ASPECT_TUTORIAL/models/spherical-shell/
ouput.pvd`

Just a hint: To stop the calculations, press **Ctrl + C**

Time snapshots of models with different resolution



Group 1: 3



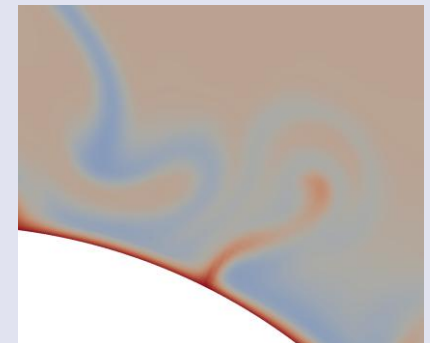
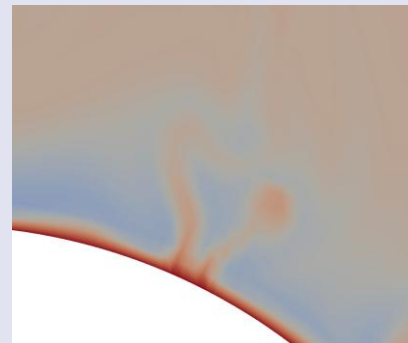
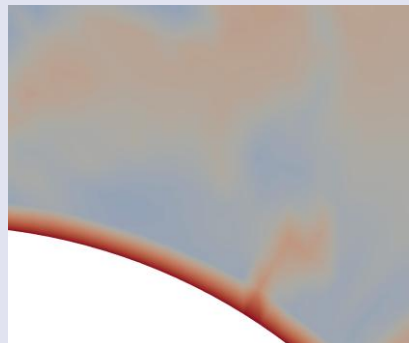
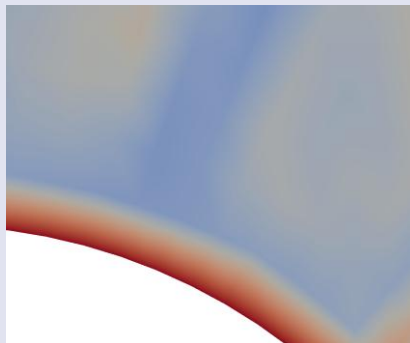
Group 2: 4



Group 3: 5



Group 4: 6

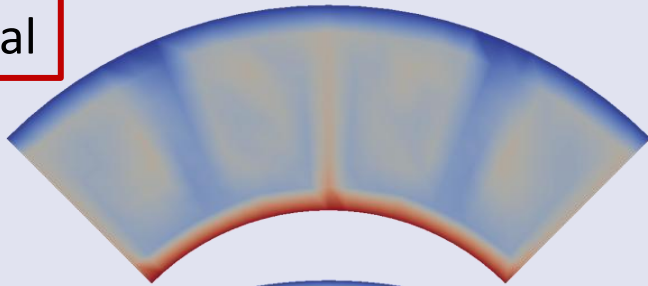


Results

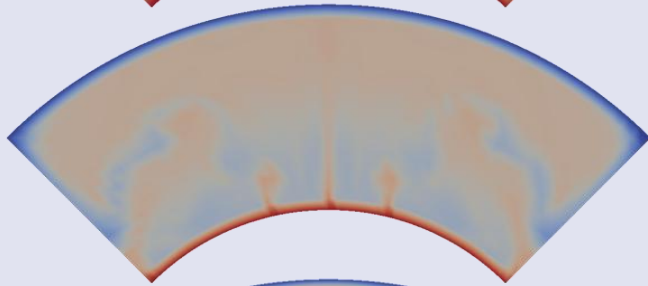
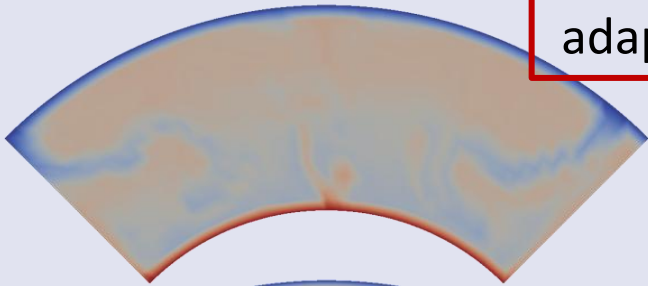
How does the flow field change with varying the resolution?

global

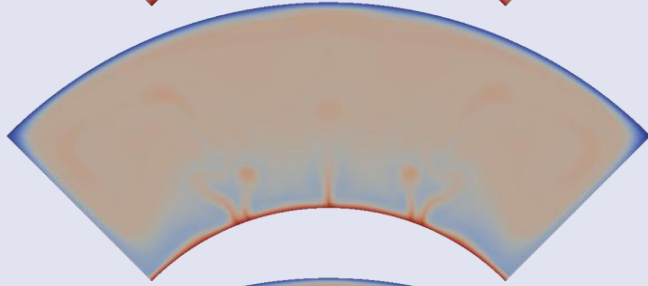
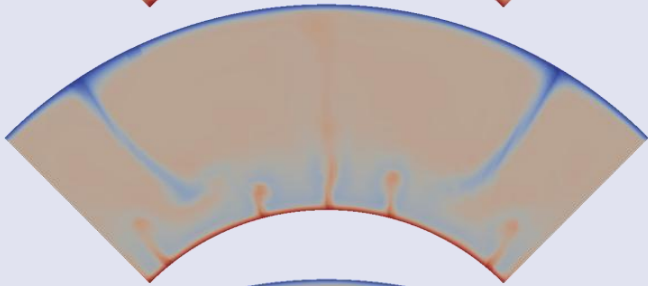
adaptive



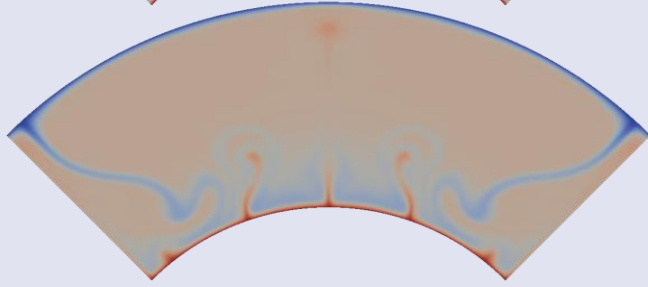
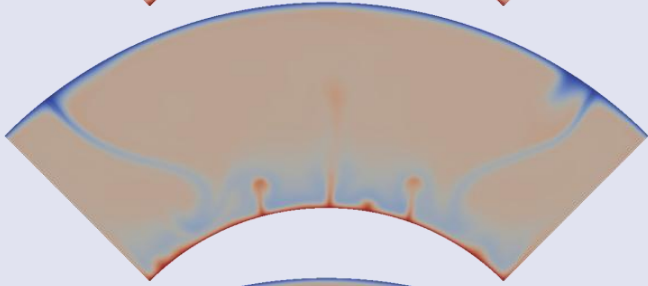
3 | 4



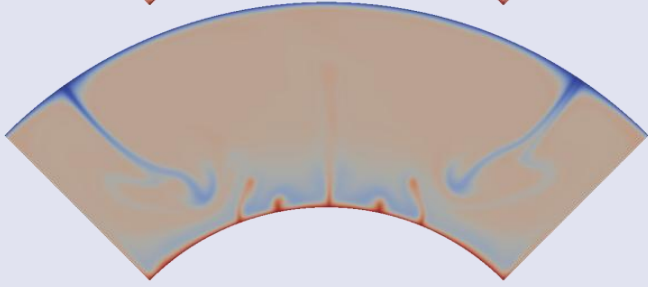
4 | 5



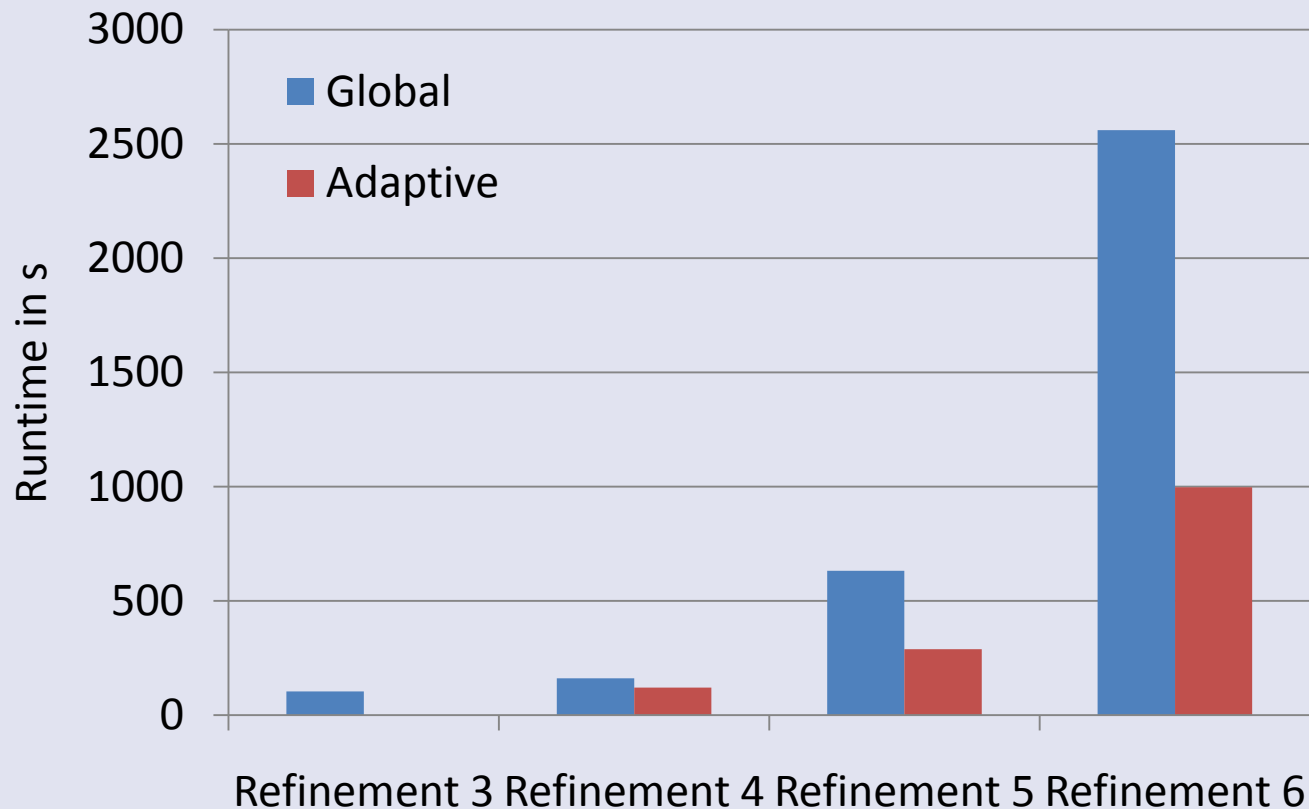
5 | 6



6 | 7



How does the runtime change with the adaptive refinement compared to global refinement?



[Movie:
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[Movie:
Thermochemical
convection
of a mantle plume](#)