Lecture 5. Rifting, Continental break-up, Transform faults

How to break a continent?

- Effect of magmas and Large Igneous Provinces
- Effect of oblique rifting
- Continental transform faults
  - > What caused Dead Sea transform?
  - San Andreas Fault System









### How to break continent?



# Effect of magma-filled dikes



#### Buck (2006)

## Effect of magma-filled dikes



It works if lithosphere is first thinned to about 75 km

Buck (2006)

# Lithospheric thinning above mantle plume



### Sobolev et al. Nature 2011

# Effect of oblique rifting



#### Brune, Popov, Sobolev JGR 2012

### Effect of oblique rifting



#### Brune, Popov, Sobolev JGR 2012

## Effect of oblique rifting





$$F_{strike-slip} = au_{yield}L_z$$

$$F_{extension} = \frac{r_{yield}L_z}{\sqrt{\frac{1}{3}(\nu^2 - \nu + 1)}}.$$

 $F_{extension} = 2\tau_{yield}L_z.$ 



#### Heine and Brune, Geology, 2014





Heine and Brune, Geology, 2014



Heine and Brune, Geology, 2014



# Conclusion

To break a continent are required:

(1) extensional deviatoric stresses (internal, from ridge push or subduction zones roll-back) and (2) lithospheric weakening

Large Igneous Provinces are optimal for lithospheric weakening, as they may both thin lithosphere and generate magma-filled dikes.

Intensive strike-slip deformation is also helpful

Continental transform faults (case Dead Sea Transform)

# **Continental Transform Faults**



### **Regional setting**

With the surface heat flow of 50-60 mW/m2, the DST is the coldest continental transform boundary



### Lithospheric thickness and magmatism

### Magmatism at 30-0 Ma





# Lithosphere-asthenosphere boundary (LAB) from seismic data



# Conclusion

Lithosphere around DST was thinned in the past and related high heat flow had not enough time to reach the surface

### **Model setup**





# Modeling technique LAPEX 3D combining FE and FD (Petrunin and Sobolev, Geology, 2006, PEPI, 2008)



### **Initial lithospheric structure:**





### **Model setup**



## Modeling results: role of the thermal erosion of the Applied force is 1.6e13N/m









## **Possible scenario**



Plumes at 25-35 Ma

# Lithospheric erosion 20-30 Ma

# Localization of the DST 15-17 Ma

# Lithospheric erosion has triggered the DST

#### Chang and Van der Lee, EPSL, 2011

# San Andreas Fault System

## San Andreas Fault System



#### **USGS** Professional Paper 1515



### 24 Ma: Shortly after Initiation of Strike-Slip



(animation by T. Atwater)





# **Questions addressed**

# Why the locus of deformation in SAFS migrates landwards with time?

How differently would evolve SAFS with "strong" and "weak" major faults? Why the locus of deformation in SAFS migrates landwards with time?

### **Extended 2D Model Setup (South view)**

















### **3D Model Setup** (view from the North)



Popov, Sobolev, Zoback, G3 2012

# Physical background

### **Balance equations**

Momentum: 
$$\frac{\partial \sigma_{ij}}{\partial x_j} + \Delta \rho g \ z_i = 0$$
  
Energy:  $\frac{DU}{Dt} = -\frac{\partial q_i}{\partial x_i} + r$ 



### **Deformation mechanisms**

 $\dot{\varepsilon}_{ij} = \dot{\varepsilon}_{ij}^{el} + \dot{\varepsilon}_{ij}^{vs} + \dot{\varepsilon}_{ij}^{pl}$ Elastic strain:  $\dot{\varepsilon}_{ij}^{el} = \frac{1}{2G} \hat{\tau}_{ij}$ Viscous strain:  $\dot{\varepsilon}_{ij}^{vs} = \frac{1}{2\eta_{eff}} \tau_{ij}$ Plastic strain:  $\dot{\varepsilon}_{ij}^{pl} = \dot{\gamma} \frac{\partial Q}{\partial \tau_{ij}}$ 





#### Popov and Sobolev (2008)

# Numerical background

#### Discretization by Finite Element Method

### Arbitrary Lagrangian-Eulerian kinematical formulation



Free surface effects (erosion, sedimentation)



Fast implicit time stepping + Newton-Raphson solver

 $u_{k+1} = u_k - K_k^{-1} r_k$ r - Residual Vector  $K = \frac{\partial r}{\partial \Delta u} - \text{Tangent Matrix}$ 

Remapping of entire fields by Particle-In-Cell technique



Popov and Sobolev (2008)

## "Strong" and "weak" faults models

"Strong faults" model: the friction coefficient decreases only slightly (from 0.6 to 0.3) with increasing plastic strain

"Weak faults" model: the friction coefficient decreases drastically (from 0.6 to 0.07) with increasing plastic strain

Popov, Sobolev, Zoback, G3 2012

# 3D Model (slab window cooling)



In 3D fault doesn't jump due to the slab window cooling. The reason is along-strike mechanical interaction (transpression) inhibiting fault jumping. Therefore new explanation is required

# 3D Model Setup with heterogeniety (at 12-15 MA)



Popov, Sobolev, Zoback, G3 2012

**250km** 





# Qualitative comparison of basic fault features







# Modeled surface heat flow



"Weak faults" versus "strong faults" model

# Weak-faults model





# Strong-faults model



## Major faults in SAFS must be weak!

## **Conclusions for SAFS**

Present day structure and landward motion of SAFS is controlled by kinematic boundary conditions and lithospheric heterogeneity, including captured Monterray microplate

Major faults at SAFS must be "week"